NEXUS GAS TRANSMISSION PROJECT

RESOURCE REPORT 7
Soils

FERC Docket No. PF15-10-000

Pre-filing Draft
June 2015

NOTICE TO PUBLIC STAKEHOLDER REVIEWERS

This Draft Resource Report for the NEXUS Gas Transmission Project (“Project”) is being filed as part of the Federal Energy Regulatory Commission’s (“FERC’s”) pre-filing process. The pre-filing process allows interested stakeholders, FERC, and regulatory agency staff to engage in early dialogue to identify affected stakeholders, facilitate early issue identification and resolution, provide multiple opportunities for public meetings (e.g., open houses), and support the preparation of high-quality environmental Resource Reports and related documents that describe the Project, assess its potential impacts, identify measures to avoid and mitigate impacts, and analyze alternatives to the Project.

Since the initial filing of Draft Resource Report 1 (Project Description) and 10 (Alternatives) on January 23, 2015, NEXUS hosted eight Open Houses along the proposed pipeline route to inform stakeholders about the proposed Project and to answer questions. FERC staff also hosted six independent Public Scoping Meetings along the proposed route in April and May of 2015, as part of the National Environmental Policy Act (“NEPA”) compliance process. This Draft Resource Report may contain items that are highlighted in grey that will be filed when NEXUS files its NGA 7(c) Certificate Application with the Commission in November 2015.

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Filing Requirement	**Location in Environmental Report**
☒ Identify, describe, and group by milepost the soils affected by the proposed pipeline and aboveground facilities. *(§380.12 (i) (1))*	Section 7.2.2; Tables 7.2-1, 7.2-2, and 7.2-3
☒ For aboveground facilities that would occupy sites over 5 acres, determine the acreage of prime farmland soils that would be affected by construction and operation. *(§380.12 (i) (2))*	Section 7.4.1 and Table 7.2-2
☒ Describe, by milepost, potential impacts on soils. *(§§ 380.12 (i)(3) and (4))*	Sections 7.2 and 7.4; Tables 7.2-1, 7.2-2 and 7.2-3
☒ Identify proposed mitigation to minimize impact on soils, and compare with the staff's Upland Erosion Control, Revegetation, and Maintenance Plan. *(§380.12(i)(5))*	Section 7.5

ACRONYMS AND ABBREVIATIONS

BMPs	Best Management Practices
Certificate	Certificate of Public Convenience and Necessity
Dawn	Dawn Hub in Ontario, Canada
E&SCP	Erosion and Sediment Control Plan
FERC Plan	Upland Erosion Control, Revegetation and Maintenance Plan
FERC Procedures	Wetland and Waterbody Construction and Mitigation Procedures
FERC	Federal Energy Regulatory Commission
M&R	metering and regulating
MP	milepost
NRCS	Natural Resource Conservation Service
PARs	Permanent Access Roads
NEXUS	NEXUS Gas Transmission, LLC
NEXUS Project or Project	NEXUS Gas Transmission Project
ROW	right-of-way
NEXUS	NEXUS Gas Transmission, LLC
SSURGO	Soil Survey Geographic Database
TARs	Temporary Access Roads
U.S.	United States
USDA	U.S. Department of Agriculture
WEG	Wind Erodibility Group

7.0 RESOURCE REPORT 7 – SOILS

7.1 Introduction

NEXUS Gas Transmission, LLC ("NEXUS") is seeking a Certificate of Public Convenience and Necessity ("Certificate") from the Federal Energy Regulatory Commission ("FERC") pursuant to Section 7(c) of the Natural Gas Act authorizing the construction and operation of the NEXUS Gas Transmission Project ("NEXUS Project" or "Project"). NEXUS is owned by affiliates of Spectra Energy Partners, LP and DTE Energy Company. The NEXUS Project will utilize greenfield pipeline construction and capacity of third party pipelines to provide for the seamless transportation of 1.5 billion cubic feet per day of Appalachian Basin shale gas, including Utica and Marcellus shale gas production, directly to consuming markets in northern Ohio and southeastern Michigan, and to the Dawn Hub in Ontario, Canada ("Dawn"). Through interconnections with existing pipelines, shippers on the NEXUS Project will also be able to reach the Chicago Hub in Illinois and other Midwestern markets. The United States portion of the NEXUS Project will traverse Pennsylvania, West Virginia, Ohio and Michigan, terminating at the U.S./Canada international boundary between Michigan and Ontario. The Canadian portion of the Project will extend from the U.S./Canada international boundary to Dawn. A more detailed description of the Project is set forth in Draft Resource Report 1.

This Draft Resource Report 7 describes the soil resources of the NEXUS Project area for the pipeline facilities and the new aboveground facilities. Tables for this Resource Report are provided in the Tables section appended to this report.

Project drawings, maps, alignment sheets, and aerials are provided in Appendix 1A of Draft Resource Report 1.

7.2 Soils in the NEXUS Project Area

The descriptions and characteristics of soils discussed in this Draft Resource Report were compiled from a variety of data sources including soil surveys published by the U.S. Department of Agriculture ("USDA") – Natural Resource Conservation Service ("USDA-NRCS" or "NRCS") and website databases maintained by the USDA-NRCS. Soil surveys referenced in this Resource Report include those for Columbiana, Stark, Summit, Wayne, Medina, Lorrain, Erie, Sandusky, Wood, Lucas, Huron, Carroll, Henry and Fulton counties in Ohio; and Lenawee, Wayne, Monroe and Washtenaw counties in Michigan. Websites used include the USDA-NRCS "Official Series Description" website (USDA, 2010a) and the USDA-NRCS "Soil Data Mart" website (USDA, 2010b).

Soils within the Project area were mapped utilizing the USDA-NRCS digital Soil Survey Geographic Database ("SSURGO"), which includes geospatially referenced Geographic Information System soil map unit polygons at a 1:24,000 scale (USDA, 2010c). The SSURGO contains the most detailed level of soil mapping performed by the NRCS, and corresponds with or supersedes the original county soil survey mapping.

Descriptions of each of the soil series impacted by the Project pipeline facilities are provided in Appendix 7A. Descriptions of each of the soil series impacted by the Project above-ground facilities are provided below. A summary of soil types by county and state affected by the NEXUS Project pipeline facilities is listed by milepost in Table 7.2-1. Tabular summaries of relevant characteristics of these soils are provided in Tables 7.2-2 and 7.2.3. Specific soil characteristics listed in these tables include: wind and water erosion potential, USDA farmland designation, hydric soil status, drought potential, compaction potential, low re-vegetation potential, stony rocky soil, and depth to bedrock.

7.2.1 Soil Series Descriptions

This section describes each soil type crossed by the Project in each state. These soil types have developed in direct relation with the local surficial geology, landforms, and relief. For more detailed geology information, refer to Draft Resource Report 6.

Ohio

The physiography of the NEXUS Project along the Ohio route is typified by several different regions which include the Glaciated Allegheny Plateaus (Appalachian Highlands), Heron-Erie Lake Plains (Interior Plains), and the Till Plains Region (Interior Plains). Within the Glaciated Allegheny Plateaus Region, the Project falls within three physiographic sub-districts that include Killbuck-Glaciated Pittsburgh Plateau, Akron-Canton Interlobate Plateau and the Illinoian Glaciated Allegheny Plateau (ODNR 1998).

The Killbuck-Glaciated Pittsburgh Plateau sub-district is described as having ridges and flat uplands typically above 1,200 feet in elevation with moderate relief. These areas are covered with thin drift and dissected by steep valleys which alternate between broad drift-filled and narrow rock-walled reaches. Elevations throughout the sub-district varies between 600 feet and 1,505 feet. The geology associated with these areas consist of thin to thick Wisconsinan-age clay to loam till over Mississippian and Pennsylvanian-age shales, sandstones, conglomerates and coals.

The Akron-Canton Interlobate Plateau sub-district is described as being hummocky between two converging glacial lobes with moderate relief. These areas are dominated by Kames, Kame terraces, eskers, kettles, kettle lakes, and bogs/fens. Elevation throughout the sub-district varies between 900 feet and 1,200 feet.

The Illinoian Glaciated Allegheny Plateau sub-district is described as having rugged hills with loess and older drift on ridgetops except where bedrock is present on slopes. Dissection is similar to unglaciated regions of the Allegheny Plateau with elevations between 600 feet to 1,400 feet.

Within the Huron-Erie Lake Plains Region, the Project falls within five physiographic sub-districts that include Erie Lake Plain, Bellevue-Castalia Karst Plain, Woodville Lake-Plain Reefs, Maumee Sand Plains and the Maumee Lake Plains.

The Erie Lake Plain is described as being at the edge of an ice-age basin which is separated from modern Lake Erie by shoreline cliffs. This area also contains major streams in deep gorges with elevation ranges from 570 feet to 800 feet.

The Bellevue-Castalia Karst Plain (6a) is characterized as being a hummocky plain of rock knobs with numerous sinkholes, large solution features, caves, and springs that are thinly mantled by drift. This region straddles both the Lake Plain and the Till Plain and contains the greatest relief of any of the Lake Plain regions. Elevations throughout this sub-district range from 570 feet to 825 feet.

The Woodsville Lake-Plain Reefs are considered to have very low relief and are associated with a lacustrine plain that contains low dunes and lake-margin features that are punctuated by more than 75 ancient bedrock reefs rising 10 feet to 40 feet above the level of the plain. The oblong reefs are thinly draped with drift and can range from 0.1 to 3.0 square miles in area. Typical elevations can range from 600 feet to 775 feet.

The Maumee Sand Plains are a Lacustrine plain that is mantled by sand. This area also includes low dunes, inter-dunal pans, beach ridges, and sand sheets of glacial lakeshores. There is very low relief in this area and elevations range from 600 feet to 800 feet.

The Maumee Lake Plains consists of a flat lying ice-age lake basin with beach ridges, bars, dunes, deltas, and clay flats that were formerly a black swamp. This area is slightly dissected by modern streams and has elevations between 570 feet and 800 feet.

Within the Till Plain Region, the Project falls within two sub-districts that include the Galion Glaciated Low Plateau and the Berea Headlands of the Till Plain.

The Galion Glaciated Low Plateau Consists of rolling uplands that are transitional between the gently rolling Till Plain and the hilly Glaciated Allegheny Plateau. This area is mantled with thin to thick drift with elevations that range from 800 feet to 1,400 feet.

The Berea Headlands of the Till Plain is described as having gently rolling to flat terrain of thin drift that descends to Lake Erie. This area is also punctuated by more than 20 streamlined "whalebacks" of Berea Sandstone. These areas extend between 0.5 to 2.5 miles and have heights that range from 30 feet to 60 feet. Typical elevations range from 800 feet to 1,000 feet.

Michigan

The physiography of the NEXUS Project along the Michigan route is typified by two different major regions, the Maumee Lowlands Region and the Southern Lower Peninsula Hills and Plains Region. The Maumee Lowlands Region is characterized as a wet plain associated with Glacial Lake Maumee. Soils in the region range from sandy (on beach ridges and deltas) to clayey (deep water lake beds). There are also a few areas within the region that contain loamy surface textures. The hydrology within the regions broad wet plain has been artificially drained for agricultural purposes (MSU 2013).

The Southern Lower Peninsula Hills and Plains Region can be described as containing ground moraines of moderate to high relief which have been formed on loam and clay loam tills. There are several large meltwater channels that dissect this region as well. Soils in the region consist of well and moderately-well drained loamy and silty soils on upland areas. In the lowlands of the region, many swamps will contain histosols.

7.2.2 Soils Crossed by the NEXUS Project Pipeline Facilities

Pipeline Facilities

Approximately 487 soil types are crossed by the NEXUS pipeline facilities. Of that amount, 432 are crossed in Ohio and 55 are crossed in Michigan.

Soil map unit descriptions and their associated map unit symbols (shown in parentheses) are provided in Appendix 7A. These soil map units are also included in Tables 7.2-2 and 7.2-3, which identifies specific characteristics of each soil type by state and county. In addition, maps showing the soils crossed by the NEXUS Project pipeline facilities are provided in Appendix 7B.

Soils Located at the Aboveground Facilities

Soil map unit descriptions and their associated map unit symbols at the proposed compressor stations are provided below. Descriptions of these soil types and their associated characteristics are provided in Table 7.2-2 and 7.2-3 and maps showing the soils affected by the NEXUS Project Compressor Stations are provided in Appendix 7C.

Hanoverton Compressor Station – Columbiana County, Ohio

Berks channery silt loam (BkE)

The Berks channery silt loam consists of moderately deep, well drained soils. Parent material consists of residuum weathered from interbedded sedimentary rock. Depth to bedrock is 20 to 40 inches. Permeability is moderate or moderately rapid above the bedrock. The potential for surface runoff is high. Depth to the seasonal high water table is greater than 1.9 feet. These soils are not classified as hydric.

Fairpoint silty clay loam (FcD)

The Fairpoint series consists of very deep, well drained soils originating from coal extraction mine spoil derived from nonacid regolith of weathered fine- earth and fragments of neutral to calcareous shale, sandstone and siltstone. Depth to bedrock is about 60 inches. These soils are located on hill slopes, summits, shoulders, back slopes, foot slopes, surface mines, spoil piles, and reclaimed lands. Rock fragment content in the A or Ap horizon ranges from 15 to 60 percent, by volume; the C horizon ranges from 35 to 60 percent, by volume, averaging 45 percent. Rock fragment size ranges from 2 mm to 25 cm, but can include stones and boulders. These soils are not classified as hydric.

Fredericktown silt loam (FoB)

The Fredericktown series consists of very deep, well drained soils formed in early Wisconsinan or Illinoian age outwash, with or without a thin loess mantle, on stream terraces and kame terraces. Slopes range from 2 to 25 percent. Permeability is moderate in the surface, moderately rapid or rapid in the subsoil and rapid in the substratum. The potential for surface runoff is medium to negligible. Depth to bedrock is greater than 80 inches. These soils are not characterized as hydric.

Gilpin silt loam (GnC, GnD)

The Gilpin series consists of moderately deep, well drained soils formed in residuum of nearly horizontal interbedded shale, siltstone, and some sandstone of the Allegheny Plateau. Fractured, bedded and rippable bedrock is at depths of 20 to 40 inches. Rock fragments are mostly angular to subangular channers of shale, siltstone and sandstone and comprise 5 to 40 percent of individual horizons of the solum and 30 to 90 percent of the C horizon. Gilpin soils are on nearly level to very steep, convex, dissected uplands with slopes of 0 to 70 percent. These soils are not classified as hydric.

Kensington silt loam (KnC, KnD)

The Kensington series consists of deep, moderately well drained soils formed in loess, Illinoian age or early Wisconsinan age till, and residuum weathered from the underlying Pennsylvanian age shale, fine grained sandstone or siltstone on till plains. Slopes range from 2 to 25 percent. Permeability is moderate in the till and moderate or moderately rapid in the underlying material above the bedrock. The potential for surface runoff is medium or high. In undisturbed areas the depth to a perched seasonal high water table is at a depth of 1.5 to 3.5 feet during November to April. Bedrock is located around 71 inches and consists of siltstone. These soils are not classified as hydric.

Teegarden silt loam (TeC, TeC2)

The Teegarden series consists of very deep, moderately well drained soils formed in loess, Illinoian or early Wisconsinan age till, and material weathered from the underlying Pennsylvanian age shale, fine-grained sandstone, or siltstone. The depth to the top of the fragipan ranges from 18 to 30 inches. The depth to paralithic contact is greater than 60 inches. Teegarden soils are located on till plains. Slopes range from 2 to 15 percent. Permeability is moderate above the fragipan, slow in the fragipan and moderate to slow below the fragipan, above bedrock. Rock fragments are dominantly sandstone, but include shale, siltstone, and some crystalline rocks. These soils are not classified as hydric.

Wadsworth Compressor Station – Medina County, Ohio

Ritmand silt loam (RsB, RsC2)

The Rittman series consist of very deep, moderately well drained soils formed in Wisconsinan age low lime till. Rittman soils are found on till plains. A large proportion of Rittman soils is either cultivated or in pasture. Slopes range from 2 to 70 percent. Depth to fragipan ranges from 18 to 36 inches. Rock fragments range from 0 to 10 percent above the fragipan and from 2 to 15 percent in the fragipan and substratum. In undisturbed areas the top of an intermittent perched seasonal high water table ranges from 10 to 27 inches from November to April in normal years. These soils are not classified as hydric.

Udorthents, loam (Ud)

The Udorthents series ranges in depth and drainage. This series is usually comprised of three components; rock fragments with silty clay loam, silt loam, and fine earth material. Based on the collection of these components determines the depth to bedrock and drainage. Udorthents loam series is usually located in areas that have been cut and the remaining soil material is similar to the subsoil and substratum of surrounding soils. Due to site specific reviews required, this soils series is not classified as hydric or not hydric.

Wadsworth silt loam (WaA, WaB)

The Wadsworth series consists of very deep, somewhat poorly drained soils formed in Wisconsinan age till that was strongly influenced by sandstone and clay shale. Some pedons have a thin mantle of loess or other silty material. The depth to bedrock is typically greater than 60 inches and depth to fragipan ranges from 18 to 30 inches. Wadsworth soils are found on interfluves, side slopes and base slopes on till plains. Slopes range from 0 to 12 percent. Rock fragment content ranges from 0 to 4 percent in the A, BE, and Bt horizons and from 2 to 15 percent in the Btx, BC, and C horizons. These soils are not classified as hydric.

Clyde Compressor Station– Sandusky County, Ohio

Belmore loam (BaB)

The belmore series consists of deep, well drained soils formed in loamy and gravelly outwash and are underlain by gravelly, sandy and loamy outwash deposits. They are on terraces, outwash plains and glacial drainage channels. Slopes range from 0 to 50 percent. The potential for surface runoff is negligible to medium. Permeability is moderately rapid in the solum and rapid in the underlying material. Most areas of Belmore soils are cultivated with principle crops being corn, soybeans, wheat, oats and hay. This soil is not classified as hydric.

Haskins sandy loam (HaB)

The Haslins series consists of very deep, somewhat poorly drained soils that are moderately deep or deep to dense till. These soils formed in loamy water-sorted or glaciolucstrine material and in the underlying till. These soils are located on lake plains and till plains. Slopes range from 0 to 6 percent. Depth to the top of the intermittent perched high water table ranges from .5 to 1.5 feet. Bedrock is located greater than 80 inches between November and April. The potential for surface runoff is low to high. Permeability is moderate in the loamy material and slow or very slow in the underlying till. This soil is not classified as hydric.

Kibbie fine sandy loam (KbA)

The Kibbie series soils consists of very deep, somewhat poorly drained soils on lake plains, ground moraines, outwash plains, and deltas. These soils formed in stratified loamy and silty glaciofluvial or galciolucustrine deposits. Slopes range from 0 to 6 percent. The depth to the water table ranges from 1 to 2 feet below the surface from November to May in normal years. Potential for surface runoff is negligible to medium. Permeability is moderate. Depth to bedrock is greater than 60 inches. This soil is not classified as hydric.

Lenawee silty clay loam (Le)

The Lenawee series soils consist of very deep, poorly drained and very poorly drained soils formed in lacustrine deposits. These soils can be found on lake plains and in depressional areas on moraines, outwash plains, and glacial drainageways. Slopes range from 0 to 2 percent. Potential for surface runoff is negligible. Permeability is moderately slow or slow. Depth to bedrock is greater than 60 inches. This soil can be ponded by runoff from higher lying adjacent soils. The seasonal high water table is near or above the surface during extended wet periods. Most of these soils are drained for farming. This soil is classified as hydric.

<u>Waterville Compressor Station – Lucas County, Ohio</u>

<u>Mermill loam (Mf)</u>

The Mermill series consists of deep, very poorly drained soils on outwash plains, terraces, and beach ridges. Mermill soils formed in loamy material 20 to 40 inches thick over fine-textured till or lacustrine material. Slopes range from 0 to 2 percent. Permeability is moderate in the loamy material and slow or very slow in the clayey material. The depth to the seasonal high water table ranges from 1 foot above the surface to 1 foot below the surface between December and May. Depth to bedrock is greater than 80 inches. These soils are classified as hydric.

<u>Metamora sandy loam (MmA)</u>

The Metamora series consists of very deep, somewhat poorly drained soils formed in loamy glaciofluvial or lacustrine deposits and the underlying loamy till on lake plains, near shore zones (relict), till plains and low moraines. Slopes range from 0 to 6 percent. Depth to the top of an apparent seasonal high water table ranges from 6 to 18 inches between March and May and in October and November in normal years. Potential for surface runoff is very low to medium. Permeability is moderately rapid in the A and Bg horizons and moderate or moderately slow in the 2Bt and 2C horizons. Depth to bedrock is greater than 60 inches. These soils are not classified as hydric.

<u>Rimer loamy fine sand (RnA)</u>

The Rimer series consists of very deep, somewhat poorly drained soils that are deep or moderately deep to dense till. These soils formed in glaciolacustrine deposits in the underlying till. They are found on convex surfaces of lake plains, wave-worked till plains, till-floored lake plains, and till plains. Slopes range from 0 to 4 percent. The depth to the top of an intermittent perched high water table ranges from 0.5 to 1.5 feet between January and April in normal years. These soils are not classified as hydric.

<u>Metering & Regulating Stations</u>

Soil types located at the proposed metering and regulating ("M&R") Stations associated with the Project have been identified and are listed below. A breakdown of permanent and temporary impacts to occur within each station can be found in Table 7.2-2.

<u>NEXUS/Kensington M&R Station</u> *(Located at the Kensington Processing Plant in Columbiana County, Ohio)*

<u>Berks Channery silt loam (BkC, BkD)</u>

The Berks channery silt loam consists of moderately deep, well drained soils. Parent material consists of residuum weathered from interbedded sedimentary rock. Depth to bedrock is 20 to 40 inches. Permeability is moderate or moderately rapid above the bedrock. The potential for surface runoff is high. Depth to the seasonal high water table is greater than 1.9 feet. These soils are not classified as hydric.

<u>Coshocton silt loam (CoC)</u>

The Coshocton series consists of deep to very deep, moderately well drained soils that formed in residuum weathered from interbedded shale, siltstone, sandstone, and occasional thin strata of coal, coal underclay, and limestone. Depth to bedrock is 40 to 84 inches. Coshocton soils are located on hill slopes, summits, shoulders and back slopes. The rock fragment ranges from 2 to 20 percent within Coshocton series'. These soils are not classified as hydric.

Orrville silt loam (Or)
The Orrville series consists of very deep, somewhat poorly drained soils formed in alluvium from upland areas of low-lime drift, and from areas of sandstone, siltstone, shale, and limestone. Depth to bedrock is greater than 60 inches. These soils are found on floodplains and floodplain steps. Slopes range from 0 to 2 percent. Average clay content ranges from 18 to 30 percent and average sand content coarser than very fine sand ranges from 15 to 40 percent in the particle-size control section. The depth to the top of an intermittent apparent seasonal high water table ranges from 0.5 to 1.0 foot from November to May in normal years. Orrville soils are subject to occasional or frequent flooding. These soils are not classified as hydric.

NEXUS/Texas Eastern M&R Station *(Located at the tie-in with the interconnecting pipeline with the Texas Eastern mainline extension in Columbiana County, Ohio)*

Berks channery silt loam (BkC, BkB)
The Berks channery silt loam consists of moderately deep, well drained soils. Parent material consists of residuum weathered from interbedded sedimentary rock. Depth to bedrock is 20 to 40 inches. Permeability is moderate or moderately rapid above the bedrock. The potential for surface runoff is high. Depth to the seasonal high water table is greater than 1.9 feet. These soils are not classified as hydric.

Coshocton silt loam (CoC)
The Coshocton series consists of deep to very deep; moderately well drained soils that formed in residuum weathered from interbedded shale, siltstone, sandstone, and occasional thin strata of coal, coal underclay, and limestone. Depth to bedrock is 40 to 84 inches. Coshocton soils are located on hill slopes, summits, shoulders and back slopes. The rock fragment ranges from 2 to 20 percent within Coshocton series'. These soils are not classified as hydric.

NEXUS/TGP M&R Station *(Located at the tie-in with the interconnecting pipeline with the TGP mainline in Columbiana County, Ohio)*

Berks Channery silt loam (BkB, BkD)
The Berks channery silt loam consists of moderately deep, well drained soils. Parent material consists of residuum weathered from interbedded sedimentary rock. Depth to bedrock is 20 to 40 inches. Permeability is moderate or moderately rapid above the bedrock. The potential for surface runoff is high. Depth to the seasonal high water table is greater than 1.9 feet. These soils are not classified as hydric.

Coshocton silt loam (CoC)
The Coshocton series consists of deep to very deep; moderately well drained soils that formed in residuum weathered from interbedded shale, siltstone, sandstone, and occasional thin strata of coal, coal underclay, and limestone. Depth to bedrock is 40 to 84 inches. Coshocton soils are located on hill slopes, summits, shoulders and back slopes. The rock fragment ranges from 2 to 20 percent within Coshocton series'. These soils are not classified as hydric.

NEXUS/Willow Run delivery M&R Station *(Located at the Project terminus in Washtenaw County, Michigan)*

Wasepi sandy loam (WaA)
The Wasepi sandy loam consists of very deep, somewhat poorly drained soils formed in loamy and sandy glaciofluvial deposits underlain by sand and gravel. Wasepi soils are located on outwash plains, deltas, valley trains, glacial drainageways, and lake plains. Slopes range from 0 to 6 percent. Depth to bedrock is greater than 60 inches. Potential for surface runoff is negligible to low. Permeability is moderately rapid in the solum and rapid in underlying sand and gravel. These soils are not classified as hydric.

7.2.3 Soils Crossed by Access Roads

To the extent feasible, existing public and private road crossings along the proposed pipeline facilities will be used as the primary means of accessing the right-of-way ("ROW"). In addition, the proposed NEXUS Project pipeline facilities have been sited along existing utility ROWs and will use existing access roads where available during construction of the pipeline. A list of soils affected by both the temporary and permanent access roads is located in Table 7.2-3. NEXUS will utilize the existing access roads during construction of the pipeline facilities to the degree practicable; soil disturbance related to pipeline facility access roads will be minimal. Some minor upgrades to existing roads (tree trimming, backblading, *etc*.) may be required to improve the existing condition of degraded access roads.

7.2.4 Pipe Yards and Contractor Ware Yards

Land requirements for the proposed pipe/contractor ware yards are provided in Table 1.6-4 of Draft Resource Report 1. In Ohio, 244.7 acres will be affected by four pipe yards and contractor ware yards. In Michigan, 67.8 acres will be affected by three pipe yards and contractor ware yards. Any soil disturbance related to these proposed facilities will be minimized and mitigated through the implementation of measures described in the Project Erosion and Sediment Control Plan ("E&SCP").

7.2.5 Other Aboveground Facilities

Soil disturbance will also occur at new, small aboveground facilities that will be located along the Project route. Any soil disturbance related to these proposed facilities located within the pipeline permanent easement will be minimized and mitigated through the implementation of measures described in the Project E&SCP, as further discussed in Section 7.5 below. Therefore, new areas of soil disturbance related to these facilities have already been addressed for the Project pipeline facilities.

7.3 Temporary Easements and Workspaces

A limited amount of grading and vegetation clearing may be needed in certain temporary easements and work spaces as needed to facilitate pipeline construction. The temporary easements and work spaces will be restored upon completion of the Project. Disturbance associated with construction activities will be minimized and mitigated through the application of the Project E&SCP. Effects to soil types within the temporary easements and work spaces during construction are included in the calculations of total area effects on soils in Table 7.2-2 and 7.2-3.

7.4 Construction and Operation Effects

Land clearing and grading, aboveground facility construction, and installation of the pipeline will affect soils within the NEXUS Project area. Soil disturbance related to these activities will be minimized and mitigated through the implementation of the provisions of the Project E&SCP, as further discussed below. The following sections discuss potential soil effects associated with Project activities including: prime farmland and farmland of unique importance, soil erosion, hydric soils, droughty soils, soil structure and compaction, stony/rock soils, introduction of rock into topsoil, and contaminated soil. Refer to Appendix 7A for a listing of soil properties pertinent to potential soil effects for each soil map unit crossed by the Project pipeline facilities and Section 7.2.2 above for the Project aboveground facilities.

7.4.1 Prime Farmland, Farmland of State Importance and Farmland of Unique Importance

Prime farmland soils are defined by USDA as having the best combination of physical and chemical characteristics for producing food, feed, forage, fiber, and oilseed crops and are available for these uses. Prime farmland has the combination of soil properties, growing season, and moisture supply needed to produce sustained high yields of crops in an economic manner if it is treated and managed according to acceptable farming methods (USDA, 2013d). Prime farmland crossed within the Project pipeline facility and Project aboveground facilities is listed in Table 7.2-2 and 7.2-3.

The USDA also identifies unique farmland, farmland of statewide agricultural importance and farmland of local importance. Unique farmland areas are identified as soils that support specific high-valued foods, but these soils require proper management. Farmland of statewide importance soils are valuable for crop production, but typically require more management and have lower yields than prime farmland soils (USDA, 2013c).

The soil classifications along the Project pipeline that are within prime farmland, farmland of state importance or farmland of unique importance are listed in Tables 7.2-2, and 7.2-3. The soil classifications associated with Project aboveground facilities that are prime farmland, farmland of state importance or farmland of unique importance are listed in Table 7.2-2.

Soil disturbance associated with construction activities will be minimized and mitigated through the application of best management practices ("BMPs") ("f"), as provided in the Project E&SCP (Appendix 1B1 of Draft Resource Report 1). Measures to be implemented to minimize and mitigate soil erosion and sedimentation are discussed below.

Pipeline Facilities

The pipeline crosses approximately 35.91 miles of soil designated as prime farmland soil, approximately 150.33 miles of prime farmland if drained and approximately 20.19 miles of soils designated as farmland of local importance. There were no soils designated as unique or of statewide importance. Impacts to prime farmland soils will be temporary and limited to the construction period.

Compressor Station Sites

Hanoverton Compressor Station, Columbiana County, Ohio
Approximately 9.5 acres of the total 28.6 acres within the permanent easement for the Hanoverton Compressor Station is designated as prime farmland soil. The area inside the fence at this location will be permanently converted from farming by operations of the proposed compressor station.

Wadsworth Compressor Station, Medina County, Ohio
Of the 19.9 acres associated with the Wadsworth Compressor Station, approximately 15.1 acres is designated as prime farmland soil and 4.8 acres have been designated as prime farmland soil if drained. These areas will be permanently impacted by the construction of the compressor station.

Clyde Compressor Station, Sandusky County, Ohio
Of the 48.6 acres associated with the Clyde Compressor Station, approximately 0.02 acres is designated as prime farmland, and 48.4 acres has been designated as prime farmland if drained. These area will be permanently impacted by the construction of the compressor station.

Waterville Compressor Station, Lucas County, Ohio
The 35 acre Waterville Compressor Station is located in soils that are designated as prime farmland if drained. This area will be permanently impacted by the construction of the compressor station.

M&R Station Sites

NEXUS/Kensington M&R Station (Located at the Kensington Processing Plant in Columbiana County, Ohio)
Of the 4.5 acres associated with the Kensington M&R Station, approximately 0.7 acres is designated as prime farmland. This area will be permanently impacted by construction of the station.

<u>*NEXUS/TGP M&R Station*</u> *(Located at the tie-in with the interconnecting pipeline with the TGP mainline in Columbiana County, Ohio)*
Of the 2.1 acres associated with the TGP M&R Station, .7 acres is designated as prime farmland. This area will be permanently impacted by the construction of the station.

<u>*NEXUS/Willow Run M&R Station*</u> *(Located at the Project terminus in Washtenaw County, Michigan).*
All of the 2.1 acres associated with the Willow Run M&R Station is designated as farmland of local importance although it currently under industrial use. This area will occupied by construction of the station.

<u>Permanent Access Roads</u>

Approximately 0.52 miles of permanent access roads will cross soils designated as prime farmland, 0.69 miles designated as prime farmland soil if drained, and 0.25 miles designated as prime farmland of local importance. These areas will be permanently impacted by the construction of the access roads.

<u>Temporary Access Roads</u>

Approximately 2.35 miles of temporary access roads will cross soils designated as prime farmland, 14.07 miles of soils designated as prime farmland if drained, and 2.39 miles of soils designated as farmland of local importance.

7.4.2 Soil Erosion

The soils affected by the NEXUS Project have a potential to be eroded by water and wind processes. These soils have the potential to erode during rain events, periods of surface water runoff, and wind transport (USDA, 2007b). Tables 7.2-2 and 7.2-3 indicate the erodibility potentials of the affected soils. The erosion potential for soils affected by water processes was determined by each soil type's K factor. In addition, the soil erosion potential for soils affected by wind transport were determined by each soil type's designated Wind Erodibility Group ("WEG"). K factors and WEG values were provided by the NRCS online Soil Data Mart. The soil information provided by the NRCS can be state specific; some soil types that are crossed by the pipeline facilities may have different K factors and WEG values.

Erosion potential in areas affected by construction will increase due to clearing, grading, trenching, and backfilling. The NEXUS Project E&SCP, which details construction and restoration measures for the upland and adjacent waterbody and wetland areas, will be utilized to minimize potential effects to soil resources.

Temporary erosion controls will be installed after initial disturbance of the soils where necessary to minimize erosion and will be maintained throughout construction. All temporary erosion and sediment controls will be installed in accordance with the Project E&SCP.

7.4.2.1 Water Erodibility

The potential for soils in the Project area to be eroded by water was determined by averaging K factor values for all soil horizons for each soil type. K factors were obtained from the USDA-NRCS Soil Data Mart (USDA, 2010c). Based on the average K factor, each soil type was grouped into a water erosion class of "Low," "Moderate," and "High." Low values ranged from 0.10 - 0.20, moderate values ranged from 0.21 to 0.40, and high values ranged from 0.40 to 0.49. For map units comprised of a complex of different soil types, the soil type with the most limiting average K factor was used to categorize the map unit into a low, medium, or high class.

A summary of the water erosion classification of the soils affected by the Project can be found in Tables 7.2-2, and 7.2-3.

Pipeline Facilities

Approximately 48.42 miles of the pipeline will cross soils designated as having a high potential to be eroded by water processes.

Compressor Station Sites

Hanoverton Compressor Station, Columbiana County, Ohio

The Hanoverton Compressor Station will temporarily affect approximately 18.22 acres of soils designated as having a high potential to be eroded by water processes.

Wadsworth Compressor Station, Medina County, Ohio

The Wadsworth Compressor Station will temporarily affect approximately 63.44 acres of soils designated as having a high potential to be eroded by water processes.

Clyde Compressor Station, Sandusky County, Ohio

The Clyde Compressor Station will temporarily affect approximately 26.98 acres of soils designated as having a high potential to be eroded by water processes.

Waterville Compressor Station, Lucas County, Ohio

The Waterville Compressor Station will not affect soils designated as having a high potential to be eroded by water processes.

M&R Sites

NEXUS/Kensington M&R Station (Located at the Kensington Processing Plant in Columbiana County, Ohio)

The Kensington M&R Station will not affect any soils designated as having a high potential to be eroded by water processes.

NEXUS/TGP M&R Station (Located at the tie-in with the interconnecting pipeline with the TGP mainline in Columbiana County, Ohio)

The TGP M&R Station will not affect any soils designated as having a high potential to be eroded by water processes.

NEXUS/Willow Run M&R Station (Located at the Project terminus in Washtenaw County, Michigan)

The Willow Run M&R Station will not affect any soils designated as having a high potential to be eroded by water processes.

Permanent Access Roads

Approximately 0.65 miles of soils crossed by the Permanent Access Roads ("PARs") have a high potential to be eroded by water processes.

Temporary Access Roads

Approximately 5.30 miles of soils crossed by the Temporary Access Roads ("TARs") have a high potential to be eroded by water processes.

7.4.2.2 Wind Erodibility

The potential for soil erosion caused by wind transport for each particular soil type affected by the NEXUS Project was determined by each soil type's designated Wind Erodibility Group ("WEG"). WEGs for soil types within the Project area were obtained from the NRCS Soil Data Mart

(USDA, 2010c). WEGs are primarily based upon soil texture, clay content, and rock fragment content (USDA, 2010c). WEGs may range from 1 to 8, with one being the highest potential for wind erosion, and 8 the lowest (USDA, 2010c). These values are based upon Wind Erodibility Index. Soils with a value between 1 and 3 are considered to have a high potential for erosion.

A summary of the WEG values of the soils affected by the Project pipeline facilities can be found in Tables 7.2-2 and 7.2-3.

Pipeline Facilities

Approximately 48.42 miles of the Project facilities will cross soils designated as having a high potential to be eroded by wind according to the Wind Erodibility Index.

Compressor Station Sites

Hanoverton Compressor Station, Columbiana County, Ohio

The Hanoverton Compressor Station will not cross soils designated as having a high potential to be eroded by wind.

Wadsworth Compressor Station, Medina County, Ohio

The Wadsworth Compressor Station will not cross soils designated as having a high potential to be eroded by wind.

Clyde Compressor Station, Sandusky County, Ohio

Approximately 30.62 acres of the Clyde Compressor Station will cross soils designated as having a high potential to be eroded by wind according to the Wind Erodibility Index.

Waterville Compressor Station, Lucas County, Ohio

Approximately 17.13 acres of the Waterville Compressor Station contains soils designated as having a high potential to be eroded by wind according to the Wind Erodibility Index.

M&R Sites

NEXUS/Kensington M&R Station (Located at the Kensington Processing Plant in Columbiana County, Ohio)

The Kensington M&R Station will not cross soils designated as having a high potential to be eroded by wind.

NEXUS/TGP M&R Station (Located at the tie-in with the interconnecting pipeline with the TGP mainline in Columbiana County, Ohio)

The TGP M&R Station will not cross soils designated as having a high potential to be eroded by wind.

NEXUS/Willow Run M&R Station (Located at the Project terminus in Washtenaw County, Michigan)

Approximately 2.1 acres of the Willow Run M&R Station contains soils designated as having a high potential to be eroded by wind according to the Wind Erodibility Index.

Permanent Access Roads

Approximately 0.30 miles of soils crossed by the PARs have a high potential to be eroded by wind according to the Wind Erodibility index.

Temporary Access Roads

Approximately 4.48 miles of soils crossed by the TARs have a high potential to be eroded by wind according to the Wind Erodibility index.

7.4.3 Hydric Soils

Hydric soils include soils developed under sufficiently wet conditions to support the growth and regeneration of hydrophytic vegetation (USDA-NRCS, 2010c). Soils that are sufficiently wet because of artificial measures are included in hydric soils (USDA-NRCS, 2010c). Also, soils in which the hydrology has been artificially modified are hydric if the soil, in an unaltered state, was hydric (UDSA-NRCS, 2010c). Some series designated as hydric have phases that are not hydric depending on water table, flooding, and ponding characteristics (USDA-NRCS, 2010c). Generally, hydric soils are those soils that are classified as poorly and very poorly drained. Hydric soil data provided is summarized in Tables 7.2-2 and 7.2-3 and are discussed below.

Pipeline Facilities

The Project pipeline facilities will cross approximately 89.63 miles (approximately 1407.47 acres) of hydric soils. Of that amount, approximately 65.88 miles will be crossed in Ohio and 23.74 miles will be crossed in Michigan.

Compressor Station Sites

Hanoverton Compressor Station, Columbiana County, Ohio

The Hanoverton Compressor Station will affect approximately 0.04 acres of hydric soils as a result of the construction of the station.

Wadsworth Compressor Station, Medina County, Ohio

The Wadsworth Compressor Station will affect approximately 1.19 acres of hydric soils as a result of the construction of the station.

Clyde Compressor Station, Sandusky County, Ohio

The Clyde Compressor Station will affect approximately 29.81 acres of hydric soils as a result of the construction of the station.

Waterville Compressor Station, Lucas County, Ohio

The Waterville Compressor Station will affect approximately 20.35 acres of hydric soils as a result of the construction of the station.

M&R Station Sites

NEXUS/Kensington M&R Station (Located at the Kensington Processing Plant in Columbiana County, Ohio)

The Kensington M&R Station will not affect any hydric soils as a result of the construction of the station.

The Texas Eastern M&R Station will not affect any hydric soils as a result of the construction of the station.

NEXUS/TGP M&R Station (Located at the tie-in with the interconnecting pipeline with the TGP mainline in Columbiana County, Ohio)

The TGP M&R Station will not affect any hydric soils as a result of the construction of the station.

NEXUS/Willow Run M&R Station (Located at the Project terminus in Washtenaw County, Michigan)

The Willow Run M&R Station will not affect any hydric soils as a result of the construction of the station.

Permanent Access Roads

Approximately 0.30 miles of soils crossed by the PARs are hydric.

Temporary Access Roads

Approximately 5.70 miles of soils crossed by the TARs are hydric.

7.4.4 Soil Structure and Compaction

Compaction and associated damage to soil structure can inhibit infiltration of rainwater, increase runoff, and impede vegetation root establishment. Given the land use context of much of the area crossed by the Project, many soils along the Project pipeline route have probably been compacted to some extent due to proximity to existing roadways, utility corridors, poor farming practices and other disturbed areas that are currently paved. The potential for soils in the Project area to become compacted was evaluated based on soil drainage class. Soils that are poorly drained or very poorly drained were classified as having a high potential for compaction. Soils that are somewhat poorly drained to moderately well drained were classified as having a moderate potential for compaction, and soils that are well drained to excessively drained were classified as having a low potential for compaction.

The soil compaction potential for each soil type within the Project area is listed in Tables 7.2-2 and 7.2-3. Section 7.5.5 provides a description of the measures that will be taken to avoid and minimize damage to soil structure and prevent soil compaction in poorly drained and very poorly drained soils.

Based on the NRCS data, the Project pipeline facilities will cross approximately 89.63 miles of soil with a high potential for compaction. Approximately 50.16 acres of impact will occur with a high potential for compaction at the Project aboveground facility sites.

7.4.5 Introduction of Rock into the Topsoil

Rocky subsoils and soils with depth to bedrock shallower than the proposed pipeline facilities are located in the Project area. As a result, NEXUS anticipates that some rock excavation and/or rock blasting during construction activities will be required. Proposed blasting activities are discussed in detail in Draft Resource Report 1 (Section 1.7.1.8), Appendix 1B3 – NEXUS Project Blasting Plan, and in Draft Resource Report 6 (Section 6.3).

To prevent incorporation of rock fragments into the topsoil along agricultural land crossed by the NEXUS Project facilities, several measures will be implemented. These measures include segregation and protection of topsoil along the trenchline, rock backfill in agricultural lands only to the top of bedrock, and disposal of excess rock fragments in an approved manner so as to not incorporate rock fragments into topsoil layers or otherwise interfere with agricultural activities. Through adherence to these measures, no significant increase to the rock content of the topsoil is anticipated in agricultural land temporarily disturbed by Project construction.

A discussion of minimization and mitigation measures for rock material in the topsoil is provided in Section 7.5.6. The depth to bedrock for each soil type within the Project area is listed in Tables 7.2-2, 7.2-3. These soils included soils that are stony, channery, cobbley and boulder modifiers.

7.4.6 Contaminated Soil

Soil contamination along the Project pipeline may result from at least two sources: hazardous material or fuel spills during construction; and/or those occurring prior to construction in pre-existing contaminated areas that are encountered during construction. Contamination from spills or leaks of fuels, lubricants, and coolant from construction equipment could adversely affect soils. The effects of such contamination are typically minor because of the low frequency and volumes of spills and leaks. NEXUS has developed a Spill Prevention, Control and Countermeasure Plan, in compliance with Environmental Protection Agency regulations at 40 CFR. Part 112 that specifies cleanup procedures in the event of soil contamination from spills or leaks of fuel, lubricants, coolants, or solvents (*see* Appendix 1B2 in Draft Resource Report 1). NEXUS and its contractors will implement the Spill Prevention, Control and Countermeasure Plan to minimize the potential effects of accidental spills of materials that may contaminate soils, and to ensure that inadvertent spills of fuels, lubricants, or solvents are contained, cleaned up, and disposed of as quickly as possible and in an appropriate manner to minimize potentially adverse effects.

NEXUS conducted a corridor database search using Environmental Data Resources, Inc., ("EDR") to identify various facilities with potential and/or actual sources of contamination that may affect soil near and along the proposed pipeline and aboveground facilities. The search identified multiple facilities with potential sources of contamination that may impact nearby soil and aboveground facilities. Information in the EDR report includes a compilation of data from a variety of available federal, state, and local government databases detailed further in Draft Resource Report 8. The EDR report provides a detailed list of potentially contaminated sites within one mile of the pipeline centerline; however, only sites within 0.25 mile of the pipelines were reviewed for their potential to affect pipeline construction.

Information relevant to documented effected areas that the pipeline will transect, or that the pipeline will be in close proximity to, is provided in Section 8.4.2.3 of Draft Resource Report 8. See Table 8.4-4 for a listing of environmental sites listed by milepost that are located within 0.25 miles of the NEXUS Project. Of the 105 reported historic occurrences along the Project pipeline in the databases queried by EDR, approximately 42 sites are located less than 500 feet from the pipeline and two are less than 100 feet from the pipeline. The Willow Run M&R Station is the only aboveground facility that is located within 500 feet of a known site. There are no known sites located within the construction workspace areas of the Project.

7.5 Impact Minimization and Mitigation

7.5.1 Existing Conditions

It is a goal of NEXUS to minimize soil impacts by locating the Project facilities adjacent to existing utility ROW to the maximum extent feasible. Utilizing existing ROW will limit new soil disturbance by working within previously developed or disturbed soils and minimizing land use change. A substantial portion of the access roads that will be used during construction and operations of the pipeline facilities already exists. These paved, dirt, and gravel municipal and private roadways will not require substantial clearing, grading, or excavation. Some maintenance may be necessary to existing access roads in order to minimize potential safety and erosion issues. Techniques that will be used to mitigate potential Project effects are described in the Project E&SCP in Appendix 1B1 of Draft Resource Report 1, which will be used by NEXUS and it's contractors as guidance for minimizing soil disturbance and transportation of sediments off the ROW or into sensitive resources (wetlands, streams, and residential areas) during pipeline construction.

7.5.2 USDA Designated Farmland Soils

As determined from SSURGO soil survey mapping and as identified by NRCS soil data mart, Project facilities will cross prime farmland soils, prime farmland if drained, and soils designated as local importance (*see* Tables 7.2-2 and 7.2-3). To the extent possible, when located on these soil types, the Project will be primarily within or along existing utility ROW and will use access roads that have been previously disturbed or developed.

During construction, NEXUS construction crews will perform topsoil segregation (described in detail in the NEXUS Project E&SCP located in Appendix 1B1 in Draft Resource Report 1) in agricultural lands as needed, which include permanent or rotated croplands, hayfields, or improved pastures, and in other areas at the request of the resource agencies or landowners. NEXUS will stockpile topsoil separately from the subsoil and will replace these soil horizons in the proper order during backfilling and final grading operations. As a result, no significant effects to soils identified as prime farmlands, prime farmland if drained, or farmland of local importance, are anticipated.

7.5.3 Soil Erosion

NEXUS has developed a Project E&SCP that provides detailed descriptions and schematics of BMPs that will be used to control soil erosion caused by water and wind. This plan is in compliance with the FERC *Upland Erosion Control, Revegetation, and Maintenance Plan* ("FERC Plan", May 2013 version) and *Wetland and Waterbody Construction and Mitigation Procedures* ("FERC Procedures", May 2013 version) as well as the specific erosion and sediment control rules and regulations for each state. Specific BMPs and procedures are summarized below:

- An Environmental Inspector will monitor all phases of Project construction to ensure BMPs outlined in the Project E&SCP are followed;
- Personnel involved in Project construction will undergo environmental training in principles and techniques outlined in the Project E&SCP;
- ROW, temporary and permanent slope breakers will be constructed to reduce runoff velocities and direct water off of the ROW;
- Temporary and permanent trench plugs will be constructed to reduce runoff velocities in the trench during construction and reduce subsurface groundwater movement after the trench is backfilled;
- Erosion controls will be placed at dike and drainage swale outlets, on steep slopes, and adjacent to roads and waterbodies as necessary;
- Surface contours and drainage patterns will be returned as nearly as possible to original conditions, except at access roads that requires improvement, and at other aboveground facilities;
- All disturbed grounds (except wetlands) will be seeded and mulched to encourage revegetation;
- Temporary winter vegetation cover will be established if Project construction is completed too late in the growing season to facilitate permanent vegetation re-establishment;
- Wetland and waterbody crossing procedures designed to minimize direct stream channel disturbance, minimize hydric soil rutting and compaction, and contain temporary trench spoil piles will be followed; and
- Post-construction monitoring will identify areas in need of remedial soil stabilization and vegetation re-establishment.

Therefore, significant soil erosion is not expected during or after Project construction.

7.5.4 Hydric and Droughty Soils

Hydric soils occur primarily within wetlands and other wet areas along the Project route while droughty soils occur in dryer areas. The Project E&SCP has been adopted for use by NEXUS and its contractors as a guidance manual for minimizing soil disturbance and transportation of sediments off the right of way or into sensitive resources during construction. Adhering to the Project E&SCP will avoid and minimize significant impacts to hydric and droughty soils where they occur.

7.5.5 Soil Structure and Compaction

Construction of the Project could result in loss of soil productivity due to compaction, or damage to soil structure from the use of heavy equipment. Soil structural damage and compaction could also result from pipeline construction during exceptionally wet periods. To minimize potential impacts to soil resources, NEXUS will utilize the measures contained in the Project E&SCP, which provides detailed construction and restoration measures for uplands and adjacent waterbody and wetland areas that could be affected by the Project. These measures include the pre and post testing of soil compaction in agricultural areas or in areas that are excessively wet using a penetrometer or other appropriate device to determine if the use of a paraplow or other deep tillage implement would be necessary. In severely compacted soils where the topsoil has been segregated, it may be necessary to plow the subsoil before replacing the segregated topsoil.

The Project is sited parallel, as much as practical, to the existing linear facilities, roads, and highways, and crosses numerous active agricultural fields where soils have been previously impacted and this will limit the amount of new soil disturbance. Where the Project does not parallel linear facilities, roads, or highways, or crosses agricultural fields, the construction of these segments will result in greater soil disturbance. The construction through agricultural land will involve special procedures such as topsoil stripping and segregation prior to construction, and de-compaction and removal of rock following installation of the pipeline during restoration.

Upon completion of pipeline installation, route surveillance as required by 49 CFR Part 192.613 will be used to monitor the pipeline rights of way. NEXUS will ensure that personnel are trained to identify signs of soil movement or subsidence. Should subsidence occur, the affected area of the pipeline will be exposed, repositioned or replaced to a stress-free state, and then properly bedded and backfilled.

7.5.6 Rock Material in the Topsoil

As previously discussed, soils with shallow bedrock may be encountered along the Project route. As a result, NEXUS anticipates that some rock excavation and/or rock blasting during construction activities will be required. These blasting activities are discussed in detail in Draft Resource Report 1 (Section 1.7.1.8 and in Appendix 1B3).

To prevent incorporation of rock fragments into the topsoil along agricultural land crossed by the NEXUS Project facilities, several measures will be implemented. These measures include segregation and protection of the topsoil along the trenchline, rock backfill in agricultural lands only to the top of the bedrock, and disposal of excess rock fragments in an approved manner so as to not incorporate rock fragments into the topsoil layers or otherwise which would impede agricultural activities. Through adherence to these measures, no significant increase to the rock content of the topsoil is anticipated.

7.5.7 Contaminated Soil

NEXUS has extensive experience managing contaminated soils and groundwater during construction activities. All soils excavated during construction will be managed in accordance with the Project E&SCP. NEXUS continues to evaluate the EDR database results and federal and state files to determine if field sampling will be required prior to construction along any of the Project areas. Although the Project route does not cross any known contaminated sites, if previously unknown/undocumented contaminated soils are encountered during construction, measures will be implemented to transport and manage excavated soil in designated soil staging areas, to characterize the soils for waste disposal, and to ensure that all soils are managed in accordance with state and federal regulations.

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TABLES

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
Ohio						
Interconnecting Pipeline to TGP						
	COLUMBIANA	Berks channery silt loam, 2 to 6 percent slopes	BkB	0.00	0.04	209
	COLUMBIANA	Berks channery silt loam, 15 to 25 percent slopes	BkD	0.04	0.11	394
	COLUMBIANA	Berks channery silt loam, 6 to 15 percent slopes	BkC	0.11	0.18	330
	COLUMBIANA	Berks channery silt loam, 15 to 25 percent slopes	BkD	0.18	0.21	153
	COLUMBIANA	Coshocton silt loam, 6 to 15 percent slopes	CoC	0.21	0.24	196
	COLUMBIANA	Berks channery silt loam, 15 to 25 percent slopes	BkD	0.24	0.33	474
	COLUMBIANA	Berks channery silt loam, 2 to 6 percent slopes	BkB	0.33	0.40	353
	COLUMBIANA	Berks channery silt loam, 6 to 15 percent slopes	BkC	0.40	0.54	763
	COLUMBIANA	Gilpin silt loam, 2 to 6 percent slopes	GnB	0.54	0.56	99
	COLUMBIANA	Berks channery silt loam, 6 to 15 percent slopes	BkC	0.56	0.58	77
	COLUMBIANA	Berks channery silt loam, 15 to 25 percent slopes	BkD	0.58	0.66	415
	COLUMBIANA	Coshocton silt loam, 6 to 15 percent slopes	CoC	0.66	0.68	136
	COLUMBIANA	Orrville silt loam, 0 to 2 percent slopes, occasionally flooded	OrA	0.68	0.75	336
	COLUMBIANA	Coshocton silt loam, 6 to 15 percent slopes	CoC	0.75	0.87	661
	COLUMBIANA	Berks channery silt loam, 15 to 25 percent slopes	BkD	0.87	0.89	114
Mainline						
	COLUMBIANA	Coshocton silt loam, 6 to 15 percent slopes	CoC	0.00	0.12	639
	COLUMBIANA	Berks channery silt loam, 15 to 25 percent slopes	BkD	0.12	0.16	188
	COLUMBIANA	Berks channery silt loam, 6 to 15 percent slopes	BkC	0.16	0.24	427

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	COLUMBIANA	Mechanicsburg silt loam, 2 to 6 percent slopes	McB	0.24	0.51	1457
	COLUMBIANA	Berks channery silt loam, 15 to 25 percent slopes	BkD	0.51	0.58	367
	COLUMBIANA	Teegarden silt loam, 6 to 15 percent slopes, eroded	TeC2	0.58	0.64	306
	COLUMBIANA	Zepernick silt loam, 0 to 2 percent slopes, occasionally flooded	ZeA	0.64	0.67	167
	COLUMBIANA	Teegarden silt loam, 6 to 15 percent slopes, eroded	TeC2	0.67	0.71	207
	COLUMBIANA	Berks channery silt loam, 15 to 25 percent slopes	BkD	0.71	0.80	477
	COLUMBIANA	Mechanicsburg silt loam, 6 to 15 percent slopes	McC	0.80	0.82	118
	COLUMBIANA	Berks channery silt loam, 15 to 25 percent slopes	BkD	0.82	0.87	261
	COLUMBIANA	Teegarden silt loam, 6 to 15 percent slopes, eroded	TeC2	0.87	1.00	680
	COLUMBIANA	Kensington silt loam, 15 to 25 percent slopes	KnD	1.00	1.05	269
	COLUMBIANA	Kensington silt loam, 6 to 15 percent slopes	KnC	1.05	1.11	287
	COLUMBIANA	Kensington silt loam, 15 to 25 percent slopes	KnD	1.11	1.13	140
	COLUMBIANA	Gilpin silt loam, 15 to 25 percent slopes	GnD	1.13	1.16	149
	COLUMBIANA	Teegarden silt loam, 6 to 15 percent slopes	TeC	1.16	1.23	351
	COLUMBIANA	Gilpin silt loam, 15 to 25 percent slopes	GnD	1.23	1.25	129
	COLUMBIANA	Gilpin silt loam, 6 to 15 percent slopes	GnC	1.25	1.31	287
	COLUMBIANA	Kensington silt loam, 6 to 15 percent slopes	KnC	1.31	1.35	215
	COLUMBIANA	Kensington silt loam, 15 to 25 percent slopes	KnD	1.35	1.38	179
	COLUMBIANA	Gilpin silt loam, 6 to 15 percent slopes	GnC	1.38	1.41	165
	COLUMBIANA	Fairpoint silty clay loam, 8 to 25 percent slopes	FcD	1.41	1.53	609

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	COLUMBIANA	Teegarden silt loam, 6 to 15 percent slopes, eroded	TeC2	1.53	1.59	340
	COLUMBIANA	Kensington silt loam, 15 to 25 percent slopes	KnD	1.59	1.62	133
	COLUMBIANA	Mechanicsburg silt loam, 6 to 15 percent slopes	McC	1.62	1.67	268
	COLUMBIANA	Berks channery silt loam, 25 to 40 percent slopes	BkE	1.67	1.70	149
	COLUMBIANA	Fredericktown gravelly loam, 6 to 15 percent slopes, eroded	FnC2	1.70	1.75	262
	COLUMBIANA	Fitchville silt loam, 0 to 2 percent slopes	FdA	1.75	1.83	429
	COLUMBIANA	Fredericktown silt loam, 2 to 6 percent slopes	FoB	1.83	1.85	100
	COLUMBIANA	Wick silt loam, 0 to 2 percent slopes, frequently flooded	WoA	1.85	1.87	116
	COLUMBIANA	Udorthents, refuse substratum, 2 to 25 percent slopes	Ub	1.87	1.89	133
	COLUMBIANA	Wick silt loam, 0 to 2 percent slopes, frequently flooded	WoA	1.89	2.16	1403
	COLUMBIANA	Glenford silt loam, 6 to 12 percent slopes	GrC	2.16	2.25	500
	COLUMBIANA	Gilpin silt loam, 15 to 25 percent slopes	GnD	2.25	2.28	127
	COLUMBIANA	Glenford silt loam, 6 to 12 percent slopes	GrC	2.28	2.32	227
	COLUMBIANA	Gilpin silt loam, 15 to 25 percent slopes	GnD	2.32	2.39	387
	COLUMBIANA	Hazleton channery loam, 6 to 15 percent slopes	HeC	2.39	2.46	337
	COLUMBIANA	Gilpin silt loam, 15 to 25 percent slopes	GnD	2.46	2.47	71
	COLUMBIANA	Hazleton channery loam, 6 to 15 percent slopes	HeC	2.47	2.55	409
	COLUMBIANA	Gilpin silt loam, 15 to 25 percent slopes	GnD	2.55	2.67	654
	COLUMBIANA	Hazleton channery loam, 6 to 15 percent slopes	HeC	2.67	2.78	539
	COLUMBIANA	Mechanicsburg silt loam, 2 to 6 percent slopes	McB	2.78	2.78	9

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	COLUMBIANA	Gilpin silt loam, 6 to 15 percent slopes	GnC	2.78	2.85	387
	COLUMBIANA	Mechanicsburg silt loam, 2 to 6 percent slopes	McB	2.85	2.92	340
	COLUMBIANA	Gilpin silt loam, 6 to 15 percent slopes	GnC	2.92	3.17	1356
	COLUMBIANA	Mechanicsburg silt loam, 2 to 6 percent slopes	McB	3.17	3.19	121
	COLUMBIANA	Kensington silt loam, 6 to 15 percent slopes	KnC	3.19	3.27	401
	COLUMBIANA	Gilpin silt loam, 15 to 25 percent slopes	GnD	3.27	3.30	175
	COLUMBIANA	Teegarden silt loam, 6 to 15 percent slopes	TeC	3.30	3.33	161
	COLUMBIANA	Berks channery silt loam, 25 to 40 percent slopes	BkE	3.33	3.39	302
	COLUMBIANA	Kensington silt loam, 15 to 25 percent slopes	KnD	3.39	3.41	74
	COLUMBIANA	Teegarden silt loam, 6 to 15 percent slopes	TeC	3.41	3.52	584
	COLUMBIANA	Kensington silt loam, 15 to 25 percent slopes	KnD	3.52	3.54	142
	COLUMBIANA	Kensington silt loam, 6 to 15 percent slopes	KnC	3.54	3.69	798
	COLUMBIANA	Kensington silt loam, 15 to 25 percent slopes	KnD	3.69	3.73	209
	COLUMBIANA	Gilpin silt loam, 15 to 25 percent slopes	GnD	3.73	3.84	569
	COLUMBIANA	Kensington silt loam, 6 to 15 percent slopes	KnC	3.84	3.88	192
	COLUMBIANA	Gilpin silt loam, 6 to 15 percent slopes	GnC	3.88	3.91	173
	COLUMBIANA	Gilpin silt loam, 15 to 25 percent slopes	GnD	3.91	4.07	821
	COLUMBIANA	Kensington silt loam, 15 to 25 percent slopes	KnD	4.07	4.09	109
	COLUMBIANA	Gilpin silt loam, 15 to 25 percent slopes	GnD	4.09	4.13	231
	COLUMBIANA	Kensington silt loam, 15 to 25 percent slopes	KnD	4.13	4.23	525

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	COLUMBIANA	Kensington silt loam, 6 to 15 percent slopes	KnC	4.23	4.28	241
	COLUMBIANA	Kensington silt loam, 15 to 25 percent slopes	KnD	4.28	4.35	418
	COLUMBIANA	Kensington silt loam, 6 to 15 percent slopes	KnC	4.35	4.46	568
	COLUMBIANA	Gilpin silt loam, 6 to 15 percent slopes	GnC	4.46	4.59	673
	COLUMBIANA	Gilpin silt loam, 15 to 25 percent slopes	GnD	4.59	4.66	386
	COLUMBIANA	Fredericktown gravelly loam, 6 to 15 percent slopes, eroded	FnC2	4.66	4.71	229
	COLUMBIANA	Jimtown silt loam, 2 to 6 percent slopes	JwB	4.71	4.75	229
	COLUMBIANA	Fredericktown gravelly loam, 6 to 15 percent slopes, eroded	FnC2	4.75	4.78	180
	COLUMBIANA	Wick silt loam, 0 to 2 percent slopes, frequently flooded	WoA	4.78	4.79	14
	COLUMBIANA	Zepernick silt loam, 0 to 2 percent slopes, occasionally flooded	ZeA	4.79	4.91	672
	COLUMBIANA	Fredericktown gravelly loam, 6 to 15 percent slopes, eroded	FnC2	4.91	5.01	484
	COLUMBIANA	Berks channery silt loam, 25 to 40 percent slopes	BkE	5.01	5.09	462
	COLUMBIANA	Teegarden silt loam, 6 to 15 percent slopes	TeC	5.09	5.14	241
	COLUMBIANA	Zepernick silt loam, 0 to 2 percent slopes, occasionally flooded	ZeA	5.14	5.17	168
	COLUMBIANA	Teegarden silt loam, 6 to 15 percent slopes	TeC	5.17	5.23	290
	COLUMBIANA	Kensington silt loam, 15 to 25 percent slopes	KnD	5.23	5.28	277
	COLUMBIANA	Kensington silt loam, 6 to 15 percent slopes	KnC	5.28	5.36	422
	COLUMBIANA	Kensington silt loam, 15 to 25 percent slopes	KnD	5.36	5.42	336
	COLUMBIANA	Teegarden silt loam, 6 to 15 percent slopes	TeC	5.42	5.47	248

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	COLUMBIANA	Zepernick silt loam, 0 to 2 percent slopes, occasionally flooded	ZeA	5.47	5.52	259
	COLUMBIANA	Fredericktown gravelly loam, 6 to 15 percent slopes, eroded	FnC2	5.52	5.54	93
	COLUMBIANA	Zepernick silt loam, 0 to 2 percent slopes, occasionally flooded	ZeA	5.54	5.59	264
	COLUMBIANA	Fredericktown gravelly loam, 6 to 15 percent slopes, eroded	FnC2	5.59	5.62	202
	COLUMBIANA	Kensington silt loam, 15 to 25 percent slopes	KnD	5.62	5.92	1580
	COLUMBIANA	Canfield silt loam, 6 to 12 percent slopes	CcC	5.92	5.96	180
	COLUMBIANA	Canfield silt loam, 2 to 6 percent slopes	CcB	5.96	6.11	791
	COLUMBIANA	Canfield silt loam, 6 to 12 percent slopes	CcC	6.11	6.19	443
	COLUMBIANA	Canfield silt loam, 2 to 6 percent slopes	CcB	6.19	6.28	495
	COLUMBIANA	Wick silt loam, 0 to 2 percent slopes, frequently flooded	WoA	6.28	6.32	196
	COLUMBIANA	Canfield silt loam, 12 to 20 percent slopes	CcD	6.32	6.39	383
	COLUMBIANA	Canfield silt loam, 6 to 12 percent slopes	CcC	6.39	6.46	374
	COLUMBIANA	Canfield silt loam, 2 to 6 percent slopes	CcB	6.46	6.52	266
	COLUMBIANA	Canfield silt loam, 6 to 12 percent slopes	CcC	6.52	6.69	950
	COLUMBIANA	Ravenna silt loam, 2 to 6 percent slopes	ReB	6.69	6.74	229
	COLUMBIANA	Canfield silt loam, 6 to 12 percent slopes	CcC	6.74	6.85	601
	COLUMBIANA	Canfield silt loam, 2 to 6 percent slopes	CcB	6.85	6.89	174
	COLUMBIANA	Canfield silt loam, 6 to 12 percent slopes	CcC	6.89	7.02	726
	COLUMBIANA	Amanda loam, 35 to 70 percent slopes	AmF	7.02	7.10	413
	COLUMBIANA	Canfield silt loam, 6 to 12 percent slopes	CcC	7.10	7.17	381

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	COLUMBIANA	Canfield silt loam, 2 to 6 percent slopes	CcB	7.17	7.29	633
	COLUMBIANA	Canfield silt loam, 6 to 12 percent slopes	CcC	7.29	7.39	516
	COLUMBIANA	Hazleton channery loam, 25 to 40 percent slopes	HeE	7.39	7.49	550
	COLUMBIANA	Kensington silt loam, 15 to 25 percent slopes	KnD	7.49	7.59	513
	COLUMBIANA	Hazleton channery loam, 25 to 40 percent slopes	HeE	7.59	7.63	192
	COLUMBIANA	Kensington silt loam, 15 to 25 percent slopes	KnD	7.63	7.67	221
	COLUMBIANA	Fitchville silt loam, 0 to 2 percent slopes	FdA	7.67	7.70	177
	COLUMBIANA	Fluvaquents, silty, 0 to 1 percent slopes, frequently flooded	FeA	7.70	7.74	170
	COLUMBIANA	Bethesda and Fairpoint channery silt loams, 25 to 70 percent slopes	BtF4F1	7.74	7.82	433
	COLUMBIANA	Fitchville silt loam, 2 to 6 percent slopes	FdB	7.82	7.90	448
	COLUMBIANA	Chili silt loam, 6 to 12 percent slopes	ChC	7.90	7.91	37
	COLUMBIANA	Kensington silt loam, 15 to 25 percent slopes	KnD	7.91	7.96	287
	COLUMBIANA	Canfield silt loam, 12 to 20 percent slopes	CcD	7.96	8.07	565
	COLUMBIANA	Canfield silt loam, 6 to 12 percent slopes	CcC	8.07	8.34	1404
	COLUMBIANA	Canfield silt loam, 2 to 6 percent slopes	CcB	8.34	8.89	2906
	COLUMBIANA	Canfield silt loam, 20 to 35 percent slopes	CcE	8.89	8.90	74
	COLUMBIANA	Canfield silt loam, 6 to 12 percent slopes	CcC	8.90	8.94	211
	COLUMBIANA	Canfield silt loam, 2 to 6 percent slopes	CcB	8.94	8.99	250
	COLUMBIANA	Canfield silt loam, 6 to 12 percent slopes	CcC	8.99	9.02	157
	COLUMBIANA	Canfield silt loam, 20 to 35 percent slopes	CcE	9.02	9.20	957

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	COLUMBIANA	Canfield silt loam, 6 to 12 percent slopes	CcC	9.20	9.24	218
	COLUMBIANA	Canfield silt loam, 20 to 35 percent slopes	CcE	9.24	9.27	155
	COLUMBIANA	Canfield silt loam, 6 to 12 percent slopes	CcC	9.27	9.37	548
	COLUMBIANA	Canfield silt loam, 20 to 35 percent slopes	CcE	9.37	9.47	530
	COLUMBIANA	Fitchville silt loam, 0 to 2 percent slopes	FdA	9.47	9.65	905
	COLUMBIANA	Rittman silt loam, 12 to 20 percent slopes, eroded	RsD2	9.65	9.68	196
	COLUMBIANA	Rittman silt loam, 6 to 12 percent slopes	RsC	9.68	9.72	222
	COLUMBIANA	Rittman silt loam, 2 to 6 percent slopes	RsB	9.72	9.83	565
	COLUMBIANA	Rittman silt loam, 6 to 12 percent slopes	RsC	9.83	9.89	291
	COLUMBIANA	Wadsworth silt loam, 2 to 6 percent slopes	WaB	9.89	9.92	159
	COLUMBIANA	Rittman silt loam, 6 to 12 percent slopes	RsC	9.92	9.94	113
	COLUMBIANA	Rittman silt loam, 2 to 6 percent slopes	RsB	9.94	10.03	483
	COLUMBIANA	Rittman silt loam, 6 to 12 percent slopes	RsC	10.03	10.07	203
	COLUMBIANA	Canfield silt loam, 20 to 35 percent slopes	CcE	10.07	10.12	254
	COLUMBIANA	Rittman silt loam, 6 to 12 percent slopes	RsC	10.12	10.17	302
	COLUMBIANA	Canfield silt loam, 20 to 35 percent slopes	CcE	10.17	10.23	309
	COLUMBIANA	Rittman silt loam, 6 to 12 percent slopes	RsC	10.23	10.24	60
	COLUMBIANA	Canfield silt loam, 20 to 35 percent slopes	CcE	10.24	10.28	177
	COLUMBIANA	Rittman silt loam, 6 to 12 percent slopes	RsC	10.28	10.34	357
	COLUMBIANA	Canfield silt loam, 20 to 35 percent slopes	CcE	10.34	10.42	380

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	COLUMBIANA	Rittman silt loam, 6 to 12 percent slopes	RsC	10.42	10.49	389
	COLUMBIANA	Rittman silt loam, 2 to 6 percent slopes	RsB	10.49	10.63	716
	COLUMBIANA	Canfield silt loam, 20 to 35 percent slopes	CcE	10.63	10.70	399
	COLUMBIANA	Rittman silt loam, 12 to 20 percent slopes, eroded	RsD2	10.70	10.74	215
	COLUMBIANA	Zepernick silt loam, 0 to 2 percent slopes, occasionally flooded	ZeA	10.74	10.80	313
	COLUMBIANA	Canfield silt loam, 12 to 20 percent slopes	CcD	10.80	10.86	287
	COLUMBIANA	Jimtown silt loam, 2 to 6 percent slopes	JwB	10.86	10.93	368
	COLUMBIANA	Canfield silt loam, 6 to 12 percent slopes	CcC	10.93	11.09	851
	COLUMBIANA	Canfield silt loam, 20 to 35 percent slopes	CcE	11.09	11.22	723
	COLUMBIANA	Zepernick silt loam, 0 to 2 percent slopes, occasionally flooded	ZeA	11.22	11.33	566
	COLUMBIANA	Canfield silt loam, 20 to 35 percent slopes	CcE	11.33	11.36	150
	COLUMBIANA	Canfield silt loam, 6 to 12 percent slopes	CcC	11.36	11.42	323
	COLUMBIANA	Canfield silt loam, 2 to 6 percent slopes	CcB	11.42	11.44	105
	COLUMBIANA	Canfield silt loam, 6 to 12 percent slopes	CcC	11.44	11.58	754
	COLUMBIANA	Canfield silt loam, 2 to 6 percent slopes	CcB	11.58	11.62	197
	COLUMBIANA	Canfield silt loam, 6 to 12 percent slopes	CcC	11.62	11.65	155
	COLUMBIANA	Canfield silt loam, 2 to 6 percent slopes	CcB	11.65	11.73	401
	COLUMBIANA	Canfield silt loam, 6 to 12 percent slopes	CcC	11.73	11.87	780
	COLUMBIANA	Canfield silt loam, 12 to 20 percent slopes	CcD	11.87	11.91	175
	COLUMBIANA	Canfield silt loam, 20 to 35 percent slopes	CcE	11.91	11.92	92

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	COLUMBIANA	Zepernick silt loam, 0 to 2 percent slopes, occasionally flooded	ZeA	11.92	12.00	402
	COLUMBIANA	Canfield silt loam, 12 to 20 percent slopes	CcD	12.00	12.01	50
	COLUMBIANA	Bogart silt loam, 2 to 6 percent slopes	BtB	12.01	12.08	362
	COLUMBIANA	Canfield silt loam, 6 to 12 percent slopes	CcC	12.08	12.20	620
	COLUMBIANA	Ravenna silt loam, 2 to 6 percent slopes	ReB	12.20	12.26	327
	COLUMBIANA	Ravenna silt loam, 2 to 6 percent slopes	ReB	12.26	12.27	54
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	12.27	12.39	643
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	12.39	12.48	467
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	12.48	12.52	212
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	12.52	12.65	693
	STARK	Canfield silt loam, 6 to 12 percent slopes, moderately eroded	CdC2	12.65	12.66	45
	STARK	Shoals silt loam	Sh	12.66	12.71	277
	STARK	Canfield silt loam, 6 to 12 percent slopes, moderately eroded	CdC2	12.71	12.72	61
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	12.72	12.79	367
	STARK	Canfield silt loam, 6 to 12 percent slopes, moderately eroded	CdC2	12.79	12.89	501
	STARK	Shoals silt loam	Sh	12.89	12.94	278
	STARK	Canfield silt loam, 6 to 12 percent slopes	CdC	12.94	13.06	637
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	13.06	13.13	391
	STARK	Canfield silt loam, 6 to 12 percent slopes, moderately eroded	CdC2	13.13	13.24	561

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State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	13.24	13.32	437
	STARK	Canfield silt loam, 6 to 12 percent slopes, moderately eroded	CdC2	13.32	13.36	178
	STARK	Canfield silt loam, 12 to 18 percent slopes, moderately eroded	CdD2	13.36	13.48	635
	STARK	Fitchville silt loam, 0 to 2 percent slopes	FcA	13.48	13.56	419
	STARK	Canfield silt loam, 6 to 12 percent slopes, moderately eroded	CdC2	13.56	13.78	1198
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	13.78	13.91	684
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	13.91	13.93	80
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	13.93	14.02	490
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	14.02	14.04	111
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	14.04	14.10	298
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	14.10	14.13	191
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	14.13	14.22	460
	STARK	Fitchville silt loam, 0 to 2 percent slopes	FcA	14.22	14.33	556
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	14.33	14.41	440
	STARK	Canfield silt loam, 6 to 12 percent slopes	CdC	14.41	14.45	229
	STARK	Fitchville silt loam, 0 to 2 percent slopes	FcA	14.45	14.48	146
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	14.48	14.54	314
	STARK	Luray silt loam	Ly	14.54	14.54	22
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	14.54	14.63	461
	STARK	Canfield silt loam, 6 to 12 percent slopes	CdC	14.63	14.68	278

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	14.68	14.75	351
	STARK	Canfield silt loam, 6 to 12 percent slopes	CdC	14.75	14.78	176
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	14.78	14.82	180
	STARK	Fitchville silt loam, 0 to 2 percent slopes	FcA	14.82	14.93	594
	STARK	Canfield silt loam, 6 to 12 percent slopes	CdC	14.93	14.97	179
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	14.97	15.02	281
	STARK	Canfield silt loam, 12 to 18 percent slopes, moderately eroded	CdD2	15.02	15.07	290
	STARK	Canfield silt loam, 6 to 12 percent slopes	CdC	15.07	15.08	22
	STARK	Canfield silt loam, 12 to 18 percent slopes, moderately eroded	CdD2	15.08	15.14	308
	STARK	Canfield silt loam, 6 to 12 percent slopes	CdC	15.14	15.18	229
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	15.18	15.41	1193
	STARK	Canfield silt loam, 6 to 12 percent slopes	CdC	15.41	15.48	383
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	15.48	15.63	828
	STARK	Canfield silt loam, 6 to 12 percent slopes, moderately eroded	CdC2	15.63	15.65	96
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	15.65	15.74	441
	STARK	Canfield silt loam, 6 to 12 percent slopes, moderately eroded	CdC2	15.74	15.77	187
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	15.77	15.78	23
	STARK	Canfield silt loam, 6 to 12 percent slopes, moderately eroded	CdC2	15.78	15.80	119

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	15.80	15.83	189
	STARK	Ravenna silt loam, 0 to 2 percent slopes	ReA	15.83	15.88	226
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	15.88	15.90	141
	STARK	Canfield silt loam, 6 to 12 percent slopes, moderately eroded	CdC2	15.90	15.93	131
	STARK	Luray silt loam	Ly	15.93	16.00	383
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	16.00	16.07	376
	STARK	Chili silt loam, 6 to 12 percent slopes, moderately eroded	CpC2	16.07	16.15	434
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	16.15	16.22	340
	STARK	Glenford silt loam, 6 to 12 percent slopes	GfC	16.22	16.26	239
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	16.26	16.40	694
	STARK	Chili silt loam, 6 to 12 percent slopes, moderately eroded	CpC2	16.40	16.43	190
	STARK	Sebring silt loam	Sb	16.43	16.91	2543
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	16.91	16.99	385
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	16.99	17.05	331
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	17.05	17.11	348
	STARK	Ravenna silt loam, 0 to 2 percent slopes	ReA	17.11	17.17	268
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	17.17	17.18	86
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	17.18	17.21	124
	STARK	Fitchville silt loam, 0 to 2 percent slopes	FcA	17.21	17.24	170
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	17.24	17.29	269
	STARK	Ravenna silt loam, 0 to 2 percent slopes	ReA	17.29	17.42	694

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	17.42	17.47	264
	STARK	Ravenna silt loam, 0 to 2 percent slopes	ReA	17.47	17.49	88
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	17.49	17.53	206
	STARK	Canfield silt loam, 6 to 12 percent slopes	CdC	17.53	17.63	539
	STARK	Luray silt loam	Ly	17.63	17.65	98
	STARK	Canfield silt loam, 6 to 12 percent slopes	CdC	17.65	17.65	46
	STARK	Luray silt loam	Ly	17.65	17.68	136
	STARK	Shoals silt loam	Sh	17.68	17.69	48
	STARK	Canfield silt loam, 6 to 12 percent slopes	CdC	17.69	17.70	68
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	17.70	17.72	81
	STARK	Fitchville silt loam, 0 to 2 percent slopes	FcA	17.72	17.85	712
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	17.85	17.91	291
	STARK	Canfield silt loam, 6 to 12 percent slopes	CdC	17.91	17.93	101
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	17.93	17.96	150
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	17.96	18.05	502
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	18.05	18.07	109
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	18.07	18.10	160
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	18.10	18.12	82
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	18.12	18.21	507
	STARK	Canfield silt loam, 6 to 12 percent slopes, moderately eroded	CdC2	18.21	18.26	260
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	18.26	18.30	187

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	STARK	Canfield silt loam, 6 to 12 percent slopes, moderately eroded	CdC2	18.30	18.31	85
	STARK	Wooster silt loam, 12 to 18 percent slopes, moderately eroded	WuD2	18.31	18.33	85
	STARK	Shoals silt loam	Sh	18.33	18.34	78
	STARK	Canfield silt loam, 6 to 12 percent slopes, moderately eroded	CdC2	18.34	18.46	609
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	18.46	18.48	120
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	18.48	18.52	197
	STARK	Canfield silt loam, 6 to 12 percent slopes, moderately eroded	CdC2	18.52	18.54	117
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	18.54	18.56	79
	STARK	Canfield silt loam, 6 to 12 percent slopes, moderately eroded	CdC2	18.56	18.57	94
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	18.57	18.59	73
	STARK	Canfield silt loam, 6 to 12 percent slopes, moderately eroded	CdC2	18.59	18.61	95
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	18.61	18.71	558
	STARK	Ravenna silt loam, 0 to 2 percent slopes	ReA	18.71	18.73	110
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	18.73	18.77	185
	STARK	Ravenna silt loam, 0 to 2 percent slopes	ReA	18.77	18.83	337
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	18.83	18.88	257
	STARK	Shoals silt loam	Sh	18.88	18.91	172
	STARK	Fitchville silt loam, 2 to 6 percent slopes	FcB	18.91	18.95	191
	STARK	Shoals silt loam	Sh	18.95	18.99	187

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	STARK	Canfield silt loam, 6 to 12 percent slopes	CdC	18.99	19.01	154
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	19.01	19.05	201
	STARK	Canfield silt loam, 6 to 12 percent slopes	CdC	19.05	19.07	102
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	19.07	19.10	171
	STARK	Ravenna silt loam, 0 to 2 percent slopes	ReA	19.10	19.13	129
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	19.13	19.25	668
	STARK	Ravenna silt loam, 0 to 2 percent slopes	ReA	19.25	19.29	200
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	19.29	19.31	114
	STARK	Sebring silt loam	Sb	19.31	19.34	149
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	19.34	19.36	101
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	19.36	19.37	57
	STARK	Fitchville silt loam, 0 to 2 percent slopes	FcA	19.37	19.39	113
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	19.39	19.41	84
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	19.41	19.48	363
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	19.48	19.50	103
	STARK	Fitchville silt loam, 0 to 2 percent slopes	FcA	19.50	19.64	764
	STARK	Wadsworth silt loam, 6 to 12 percent slopes	WaC	19.64	19.68	172
	STARK	Wadsworth silt loam, 2 to 6 percent slopes	WaB	19.68	19.78	569
	STARK	Rittman silt loam, 6 to 12 percent slopes, moderately eroded	RsC2	19.78	19.86	384
	STARK	Wadsworth silt loam, 2 to 6 percent slopes	WaB	19.86	20.03	940
	STARK	Shoals silt loam	Sh	20.03	20.11	402

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	STARK	Rittman silt loam, 2 to 6 percent slopes	RsB	20.11	20.27	842
	STARK	Rittman silt loam, 6 to 12 percent slopes, moderately eroded	RsC2	20.27	20.33	321
	STARK	Wadsworth silt loam, 2 to 6 percent slopes	WaB	20.33	20.38	275
	STARK	Rittman silt loam, 6 to 12 percent slopes, moderately eroded	RsC2	20.38	20.45	369
	STARK	Wadsworth silt loam, 2 to 6 percent slopes	WaB	20.45	20.52	355
	STARK	Rittman silt loam, 6 to 12 percent slopes, moderately eroded	RsC2	20.52	20.53	71
	STARK	Wadsworth silt loam, 2 to 6 percent slopes	WaB	20.53	20.60	356
	STARK	Sebring silt loam, till substratum	Se	20.60	20.63	155
	STARK	Conotton gravelly loam, 2 to 6 percent slopes	CyB	20.63	20.78	773
	STARK	Ravenna silt loam, 0 to 2 percent slopes	ReA	20.78	20.81	197
	STARK	Sebring silt loam, till substratum	Se	20.81	20.84	162
	STARK	Wadsworth silt loam, 0 to 2 percent slopes	WaA	20.84	20.98	702
	STARK	Rittman silt loam, 2 to 6 percent slopes	RsB	20.98	21.00	108
	STARK	Wadsworth silt loam, 0 to 2 percent slopes	WaA	21.00	21.10	552
	STARK	Wadsworth silt loam, 2 to 6 percent slopes	WaB	21.10	21.12	112
	STARK	Wadsworth silt loam, 0 to 2 percent slopes	WaA	21.12	21.16	191
	STARK	Wadsworth silt loam, 2 to 6 percent slopes	WaB	21.16	21.25	466
	STARK	Wadsworth silt loam, 6 to 12 percent slopes	WaC	21.25	21.29	238
	STARK	Weinbach silt loam, 0 to 2 percent slopes	WhA	21.29	21.33	175
	STARK	Weinbach silt loam, 2 to 6 percent slopes	WhB	21.33	21.42	501

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	STARK	Wadsworth silt loam, 0 to 2 percent slopes	WaA	21.42	21.59	910
	STARK	Wadsworth silt loam, 2 to 6 percent slopes	WaB	21.59	21.79	1047
	STARK	Wadsworth silt loam, 0 to 2 percent slopes	WaA	21.79	21.86	385
	STARK	Wadsworth silt loam, 2 to 6 percent slopes	WaB	21.86	21.98	596
	STARK	Wadsworth silt loam, 6 to 12 percent slopes, moderately eroded	WaC2	21.98	22.01	177
	STARK	Rittman silt loam, 12 to 18 percent slopes, moderately eroded	RsD2	22.01	22.03	123
	STARK	Wadsworth silt loam, 2 to 6 percent slopes	WaB	22.03	22.06	151
	STARK	Rittman silt loam, 12 to 18 percent slopes, moderately eroded	RsD2	22.06	22.07	14
	STARK	Rittman silt loam, 6 to 12 percent slopes, moderately eroded	RsC2	22.07	22.13	352
	STARK	Wadsworth silt loam, 2 to 6 percent slopes	WaB	22.13	22.24	566
	STARK	Wadsworth silt loam, 6 to 12 percent slopes, moderately eroded	WaC2	22.24	22.27	161
	STARK	Shoals silt loam	Sh	22.27	22.30	137
	STARK	Wadsworth silt loam, 2 to 6 percent slopes	WaB	22.30	22.33	155
	STARK	Rittman silt loam, 6 to 12 percent slopes, moderately eroded	RsC2	22.33	22.43	546
	STARK	Wadsworth silt loam, 6 to 12 percent slopes, moderately eroded	WaC2	22.43	22.48	286
	STARK	Sebring silt loam, till substratum	Se	22.48	22.50	107
	STARK	Wadsworth silt loam, 6 to 12 percent slopes, moderately eroded	WaC2	22.50	22.53	141
	STARK	Wadsworth silt loam, 2 to 6 percent slopes	WaB	22.53	22.62	482

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	STARK	Wadsworth silt loam, 6 to 12 percent slopes, moderately eroded	WaC2	22.62	22.71	447
	STARK	Wadsworth silt loam, 2 to 6 percent slopes	WaB	22.71	22.80	489
	STARK	Wadsworth silt loam, 6 to 12 percent slopes, moderately eroded	WaC2	22.80	22.85	281
	STARK	Wadsworth silt loam, 2 to 6 percent slopes	WaB	22.85	23.29	2319
	STARK	Sebring silt loam, till substratum	Se	23.29	23.36	339
	STARK	Wadsworth silt loam, 2 to 6 percent slopes	WaB	23.36	23.39	162
	STARK	Sebring silt loam, till substratum	Se	23.39	23.41	120
	STARK	Wadsworth silt loam, 2 to 6 percent slopes	WaB	23.41	23.63	1163
	STARK	Wadsworth silt loam, 0 to 2 percent slopes	WaA	23.63	23.77	729
	STARK	Wadsworth silt loam, 2 to 6 percent slopes	WaB	23.77	23.80	178
	STARK	Weinbach silt loam, 0 to 2 percent slopes	WhA	23.80	23.83	177
	STARK	Sloan silt loam	Sl	23.83	23.91	381
	STARK	Ravenna silt loam, 0 to 2 percent slopes	ReA	23.91	24.08	923
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	24.08	24.16	427
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	24.16	24.29	694
	STARK	Wooster silt loam, 6 to 12 percent slopes, moderately eroded	WuC2	24.29	24.41	637
	STARK	Luray silt loam	Ly	24.41	24.43	79
	STARK	Wooster silt loam, 6 to 12 percent slopes, moderately eroded	WuC2	24.43	24.50	362
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	24.50	24.51	87
	STARK	Wooster silt loam, 6 to 12 percent slopes, moderately eroded	WuC2	24.51	24.61	510

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	STARK	Canfield silt loam, 6 to 12 percent slopes, moderately eroded	CdC2	24.61	24.63	82
	STARK	Wooster silt loam, 6 to 12 percent slopes, moderately eroded	WuC2	24.63	24.67	209
	STARK	Wooster silt loam, 12 to 18 percent slopes, moderately eroded	WuD2	24.67	24.71	231
	STARK	Wooster silt loam, 6 to 12 percent slopes, moderately eroded	WuC2	24.71	24.73	100
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	24.73	24.86	697
	STARK	Luray silt loam	Ly	24.86	24.90	221
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	24.90	24.91	62
	STARK	Wooster silt loam, 6 to 12 percent slopes, moderately eroded	WuC2	24.91	24.93	71
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	24.93	24.97	200
	STARK	Luray silt loam	Ly	24.97	24.99	114
	STARK	Weinbach silt loam, 0 to 2 percent slopes	WhA	24.99	25.07	450
	STARK	Fitchville silt loam, 0 to 2 percent slopes	FcA	25.07	25.15	418
	STARK	Wooster silt loam, 6 to 12 percent slopes	WuC	25.15	25.22	354
	STARK	Chili gravelly loam, 6 to 12 percent slopes, moderately eroded	CoC2	25.22	25.24	139
	STARK	Chili loam, 2 to 6 percent slopes	CnB	25.24	25.29	240
	STARK	Chili gravelly loam, 6 to 12 percent slopes, moderately eroded	CoC2	25.29	25.37	416
	STARK	Chili loam, 2 to 6 percent slopes	CnB	25.37	25.57	1045
	STARK	Ravenna silt loam, 0 to 2 percent slopes	ReA	25.57	25.59	109
	STARK	Chili gravelly loam, 6 to 12 percent slopes	CoC	25.59	25.73	732

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	STARK	Bogart silt loam, 2 to 6 percent slopes	BoB	25.73	25.75	148
	STARK	Chili silt loam, 6 to 12 percent slopes, moderately eroded	CpC2	25.75	25.87	595
	STARK	Chili silt loam, 0 to 2 percent slopes	CpA	25.87	25.91	212
	STARK	Chili silt loam, 2 to 6 percent slopes	CpB	25.91	25.93	135
	STARK	Luray silt loam, gravelly subsoil variant	Lz	25.93	26.23	1578
	STARK	Chili silt loam, 6 to 12 percent slopes	CpC	26.23	26.39	837
	STARK	Weinbach silt loam, 0 to 2 percent slopes	WhA	26.39	26.49	523
	STARK	Luray silt loam	Ly	26.49	26.51	136
	STARK	Sloan silt loam	Sl	26.51	26.54	150
	STARK	Willette muck	Wt	26.54	26.59	257
	STARK	Fitchville silt loam, 0 to 2 percent slopes	FcA	26.59	26.64	274
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	26.64	26.67	165
	STARK	Wooster silt loam, 12 to 18 percent slopes, moderately eroded	WuD2	26.67	26.71	185
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	26.71	26.76	240
	STARK	Chili silt loam, 2 to 6 percent slopes	CpB	26.76	26.80	257
	STARK	Wooster silt loam, 6 to 12 percent slopes, moderately eroded	WuC2	26.80	26.86	275
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	26.86	26.93	381
	STARK	Carlisle muck	Ch	26.93	27.06	696
	STARK	Chili silt loam, 2 to 6 percent slopes	CpB	27.06	27.15	493
	STARK	Willette muck	Wt	27.15	27.25	489
	STARK	Fitchville silt loam, 0 to 2 percent slopes	FcA	27.25	27.25	7

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	STARK	Chili silt loam, 6 to 12 percent slopes, moderately eroded	CpC2	27.25	27.32	390
	STARK	Fitchville silt loam, 0 to 2 percent slopes	FcA	27.32	27.33	23
	STARK	Chili silt loam, 6 to 12 percent slopes, moderately eroded	CpC2	27.33	27.43	566
	STARK	Fitchville silt loam, 0 to 2 percent slopes	FcA	27.43	27.46	125
	STARK	Chili silt loam, 6 to 12 percent slopes, moderately eroded	CpC2	27.46	27.52	312
	STARK	Fitchville silt loam, 0 to 2 percent slopes	FcA	27.52	27.55	196
	STARK	Chili silt loam, 6 to 12 percent slopes, moderately eroded	CpC2	27.55	27.62	363
	STARK	Chili silt loam, 2 to 6 percent slopes	CpB	27.62	27.89	1419
	STARK	Fitchville silt loam, 0 to 2 percent slopes	FcA	27.89	27.93	232
	STARK	Bogart silt loam, 2 to 6 percent slopes	BoB	27.93	28.13	1051
	STARK	Fitchville silt loam, 0 to 2 percent slopes	FcA	28.13	28.24	559
	STARK	Chili silt loam, 2 to 6 percent slopes	CpB	28.24	28.39	821
	STARK	Chili silt loam, 6 to 12 percent slopes, moderately eroded	CpC2	28.39	28.42	140
	STARK	Chili silt loam, 2 to 6 percent slopes	CpB	28.42	28.48	329
	STARK	Weinbach silt loam, 0 to 2 percent slopes	WhA	28.48	28.50	62
	STARK	Sebring silt loam	Sb	28.50	28.55	294
	STARK	Luray silt loam	Ly	28.55	28.61	334
	STARK	Fitchville silt loam, 0 to 2 percent slopes	FcA	28.61	28.68	329
	STARK	Weinbach silt loam, 0 to 2 percent slopes	WhA	28.68	28.73	258
	STARK	Chili silt loam, 6 to 12 percent slopes	CpC	28.73	28.82	526
	STARK	Fitchville silt loam, 0 to 2 percent slopes	FcA	28.82	28.85	149

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	STARK	Willette muck	Wt	28.85	28.90	264
	STARK	Luray silt loam	Ly	28.90	28.93	158
	STARK	Weinbach silt loam, 0 to 2 percent slopes	WhA	28.93	28.94	39
	STARK	Weinbach silt loam, 2 to 6 percent slopes	WhB	28.94	28.99	278
	STARK	Weinbach silt loam, 0 to 2 percent slopes	WhA	28.99	28.99	10
	STARK	Carlisle muck	Ch	28.99	29.01	102
	STARK	Weinbach silt loam, 0 to 2 percent slopes	WhA	29.01	29.04	113
	STARK	Carlisle muck	Ch	29.04	29.05	91
	STARK	Luray silt loam	Ly	29.05	29.08	138
	STARK	Weinbach silt loam, 2 to 6 percent slopes	WhB	29.08	29.10	98
	STARK	Luray silt loam	Ly	29.10	29.13	159
	STARK	Fitchville silt loam, 2 to 6 percent slopes	FcB	29.13	29.14	87
	STARK	Chili gravelly loam, 12 to 18 percent slopes, moderately eroded	CoD2	29.14	29.16	103
	STARK	Chili silt loam, 6 to 12 percent slopes, moderately eroded	CpC2	29.16	29.21	230
	STARK	Carlisle muck	Ch	29.21	29.25	224
	STARK	Chili silt loam, 6 to 12 percent slopes, moderately eroded	CpC2	29.25	29.31	316
	STARK	Chili gravelly loam, 12 to 18 percent slopes, moderately eroded	CoD2	29.31	29.33	90
	STARK	Glenford silt loam, 2 to 6 percent slopes	GfB	29.33	29.36	167
	STARK	Luray silt loam	Ly	29.36	29.45	492
	STARK	Glenford silt loam, 2 to 6 percent slopes	GfB	29.45	29.48	151
	STARK	Wheeling silt loam, 2 to 6 percent slopes	WrB	29.48	29.53	280
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	12.27	12.39	643

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	12.39	12.48	467
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	12.48	12.52	212
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	12.52	12.65	693
	STARK	Canfield silt loam, 6 to 12 percent slopes, moderately eroded	CdC2	12.65	12.66	45
	STARK	Shoals silt loam	Sh	12.66	12.71	277
	STARK	Canfield silt loam, 6 to 12 percent slopes, moderately eroded	CdC2	12.71	12.72	61
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	12.72	12.79	367
	STARK	Canfield silt loam, 6 to 12 percent slopes, moderately eroded	CdC2	12.79	12.89	501
	STARK	Shoals silt loam	Sh	12.89	12.94	278
	STARK	Canfield silt loam, 6 to 12 percent slopes	CdC	12.94	13.06	637
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	13.06	13.13	391
	STARK	Canfield silt loam, 6 to 12 percent slopes, moderately eroded	CdC2	13.13	13.24	561
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	13.24	13.32	437
	STARK	Canfield silt loam, 6 to 12 percent slopes, moderately eroded	CdC2	13.32	13.36	178
	STARK	Canfield silt loam, 12 to 18 percent slopes, moderately eroded	CdD2	13.36	13.48	635
	STARK	Fitchville silt loam, 0 to 2 percent slopes	FcA	13.48	13.56	419
	STARK	Canfield silt loam, 6 to 12 percent slopes, moderately eroded	CdC2	13.56	13.78	1198
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	13.78	13.91	684

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	13.91	13.93	80
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	13.93	14.02	490
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	14.02	14.04	111
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	14.04	14.10	298
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	14.10	14.13	191
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	14.13	14.22	460
	STARK	Fitchville silt loam, 0 to 2 percent slopes	FcA	14.22	14.33	556
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	14.33	14.41	440
	STARK	Canfield silt loam, 6 to 12 percent slopes	CdC	14.41	14.45	229
	STARK	Fitchville silt loam, 0 to 2 percent slopes	FcA	14.45	14.48	146
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	14.48	14.54	314
	STARK	Luray silt loam	Ly	14.54	14.54	22
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	14.54	14.63	461
	STARK	Canfield silt loam, 6 to 12 percent slopes	CdC	14.63	14.68	278
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	14.68	14.75	351
	STARK	Canfield silt loam, 6 to 12 percent slopes	CdC	14.75	14.78	176
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	14.78	14.82	180
	STARK	Fitchville silt loam, 0 to 2 percent slopes	FcA	14.82	14.93	594
	STARK	Canfield silt loam, 6 to 12 percent slopes	CdC	14.93	14.97	179
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	14.97	15.02	281

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	STARK	Canfield silt loam, 12 to 18 percent slopes, moderately eroded	CdD2	15.02	15.07	290
	STARK	Canfield silt loam, 6 to 12 percent slopes	CdC	15.07	15.08	22
	STARK	Canfield silt loam, 12 to 18 percent slopes, moderately eroded	CdD2	15.08	15.14	308
	STARK	Canfield silt loam, 6 to 12 percent slopes	CdC	15.14	15.18	229
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	15.18	15.41	1193
	STARK	Canfield silt loam, 6 to 12 percent slopes	CdC	15.41	15.48	383
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	15.48	15.63	828
	STARK	Canfield silt loam, 6 to 12 percent slopes, moderately eroded	CdC2	15.63	15.65	96
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	15.65	15.74	441
	STARK	Canfield silt loam, 6 to 12 percent slopes, moderately eroded	CdC2	15.74	15.77	187
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	15.77	15.78	23
	STARK	Canfield silt loam, 6 to 12 percent slopes, moderately eroded	CdC2	15.78	15.80	119
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	15.80	15.83	189
	STARK	Ravenna silt loam, 0 to 2 percent slopes	ReA	15.83	15.88	226
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	15.88	15.90	141
	STARK	Canfield silt loam, 6 to 12 percent slopes, moderately eroded	CdC2	15.90	15.93	131
	STARK	Luray silt loam	Ly	15.93	16.00	383
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	16.00	16.07	376

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	STARK	Chili silt loam, 6 to 12 percent slopes, moderately eroded	CpC2	16.07	16.15	434
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	16.15	16.22	340
	STARK	Glenford silt loam, 6 to 12 percent slopes	GfC	16.22	16.26	239
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	16.26	16.40	694
	STARK	Chili silt loam, 6 to 12 percent slopes, moderately eroded	CpC2	16.40	16.43	190
	STARK	Sebring silt loam	Sb	16.43	16.91	2543
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	16.91	16.99	385
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	16.99	17.05	331
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	17.05	17.11	348
	STARK	Ravenna silt loam, 0 to 2 percent slopes	ReA	17.11	17.17	268
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	17.17	17.18	86
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	17.18	17.21	124
	STARK	Fitchville silt loam, 0 to 2 percent slopes	FcA	17.21	17.24	170
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	17.24	17.29	269
	STARK	Ravenna silt loam, 0 to 2 percent slopes	ReA	17.29	17.42	694
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	17.42	17.47	264
	STARK	Ravenna silt loam, 0 to 2 percent slopes	ReA	17.47	17.49	88
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	17.49	17.53	206
	STARK	Canfield silt loam, 6 to 12 percent slopes	CdC	17.53	17.63	539
	STARK	Luray silt loam	Ly	17.63	17.65	98
	STARK	Canfield silt loam, 6 to 12 percent slopes	CdC	17.65	17.65	46

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	STARK	Luray silt loam	Ly	17.65	17.68	136
	STARK	Shoals silt loam	Sh	17.68	17.69	48
	STARK	Canfield silt loam, 6 to 12 percent slopes	CdC	17.69	17.70	68
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	17.70	17.72	81
	STARK	Fitchville silt loam, 0 to 2 percent slopes	FcA	17.72	17.85	712
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	17.85	17.91	291
	STARK	Canfield silt loam, 6 to 12 percent slopes	CdC	17.91	17.93	101
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	17.93	17.96	150
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	17.96	18.05	502
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	18.05	18.07	109
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	18.07	18.10	160
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	18.10	18.12	82
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	18.12	18.21	507
	STARK	Canfield silt loam, 6 to 12 percent slopes, moderately eroded	CdC2	18.21	18.26	260
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	18.26	18.30	187
	STARK	Canfield silt loam, 6 to 12 percent slopes, moderately eroded	CdC2	18.30	18.31	85
	STARK	Wooster silt loam, 12 to 18 percent slopes, moderately eroded	WuD2	18.31	18.33	85
	STARK	Shoals silt loam	Sh	18.33	18.34	78
	STARK	Canfield silt loam, 6 to 12 percent slopes, moderately eroded	CdC2	18.34	18.46	609
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	18.46	18.48	120

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	18.48	18.52	197
	STARK	Canfield silt loam, 6 to 12 percent slopes, moderately eroded	CdC2	18.52	18.54	117
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	18.54	18.56	79
	STARK	Canfield silt loam, 6 to 12 percent slopes, moderately eroded	CdC2	18.56	18.57	94
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	18.57	18.59	73
	STARK	Canfield silt loam, 6 to 12 percent slopes, moderately eroded	CdC2	18.59	18.61	95
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	18.61	18.71	558
	STARK	Ravenna silt loam, 0 to 2 percent slopes	ReA	18.71	18.73	110
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	18.73	18.77	185
	STARK	Ravenna silt loam, 0 to 2 percent slopes	ReA	18.77	18.83	337
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	18.83	18.88	257
	STARK	Shoals silt loam	Sh	18.88	18.91	172
	STARK	Fitchville silt loam, 2 to 6 percent slopes	FcB	18.91	18.95	191
	STARK	Shoals silt loam	Sh	18.95	18.99	187
	STARK	Canfield silt loam, 6 to 12 percent slopes	CdC	18.99	19.01	154
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	19.01	19.05	201
	STARK	Canfield silt loam, 6 to 12 percent slopes	CdC	19.05	19.07	102
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	19.07	19.10	171
	STARK	Ravenna silt loam, 0 to 2 percent slopes	ReA	19.10	19.13	129
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	19.13	19.25	668

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	STARK	Ravenna silt loam, 0 to 2 percent slopes	ReA	19.25	19.29	200
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	19.29	19.31	114
	STARK	Sebring silt loam	Sb	19.31	19.34	149
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	19.34	19.36	101
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	19.36	19.37	57
	STARK	Fitchville silt loam, 0 to 2 percent slopes	FcA	19.37	19.39	113
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	19.39	19.41	84
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	19.41	19.48	363
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	19.48	19.50	103
	STARK	Fitchville silt loam, 0 to 2 percent slopes	FcA	19.50	19.64	764
	STARK	Wadsworth silt loam, 6 to 12 percent slopes	WaC	19.64	19.68	172
	STARK	Wadsworth silt loam, 2 to 6 percent slopes	WaB	19.68	19.78	569
	STARK	Rittman silt loam, 6 to 12 percent slopes, moderately eroded	RsC2	19.78	19.86	384
	STARK	Wadsworth silt loam, 2 to 6 percent slopes	WaB	19.86	20.03	940
	STARK	Shoals silt loam	Sh	20.03	20.11	402
	STARK	Rittman silt loam, 2 to 6 percent slopes	RsB	20.11	20.27	842
	STARK	Rittman silt loam, 6 to 12 percent slopes, moderately eroded	RsC2	20.27	20.33	321
	STARK	Wadsworth silt loam, 2 to 6 percent slopes	WaB	20.33	20.38	275
	STARK	Rittman silt loam, 6 to 12 percent slopes, moderately eroded	RsC2	20.38	20.45	369
	STARK	Wadsworth silt loam, 2 to 6 percent slopes	WaB	20.45	20.52	355

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	STARK	Rittman silt loam, 6 to 12 percent slopes, moderately eroded	RsC2	20.52	20.53	71
	STARK	Wadsworth silt loam, 2 to 6 percent slopes	WaB	20.53	20.60	356
	STARK	Sebring silt loam, till substratum	Se	20.60	20.63	155
	STARK	Conotton gravelly loam, 2 to 6 percent slopes	CyB	20.63	20.78	773
	STARK	Ravenna silt loam, 0 to 2 percent slopes	ReA	20.78	20.81	197
	STARK	Sebring silt loam, till substratum	Se	20.81	20.84	162
	STARK	Wadsworth silt loam, 0 to 2 percent slopes	WaA	20.84	20.98	702
	STARK	Rittman silt loam, 2 to 6 percent slopes	RsB	20.98	21.00	108
	STARK	Wadsworth silt loam, 0 to 2 percent slopes	WaA	21.00	21.10	552
	STARK	Wadsworth silt loam, 2 to 6 percent slopes	WaB	21.10	21.12	112
	STARK	Wadsworth silt loam, 0 to 2 percent slopes	WaA	21.12	21.16	191
	STARK	Wadsworth silt loam, 2 to 6 percent slopes	WaB	21.16	21.25	466
	STARK	Wadsworth silt loam, 6 to 12 percent slopes	WaC	21.25	21.29	238
	STARK	Weinbach silt loam, 0 to 2 percent slopes	WhA	21.29	21.33	175
	STARK	Weinbach silt loam, 2 to 6 percent slopes	WhB	21.33	21.42	501
	STARK	Wadsworth silt loam, 0 to 2 percent slopes	WaA	21.42	21.59	910
	STARK	Wadsworth silt loam, 2 to 6 percent slopes	WaB	21.59	21.79	1047
	STARK	Wadsworth silt loam, 0 to 2 percent slopes	WaA	21.79	21.86	385
	STARK	Wadsworth silt loam, 2 to 6 percent slopes	WaB	21.86	21.98	596
	STARK	Wadsworth silt loam, 6 to 12 percent slopes, moderately eroded	WaC2	21.98	22.01	177

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	STARK	Rittman silt loam, 12 to 18 percent slopes, moderately eroded	RsD2	22.01	22.03	123
	STARK	Wadsworth silt loam, 2 to 6 percent slopes	WaB	22.03	22.06	151
	STARK	Rittman silt loam, 12 to 18 percent slopes, moderately eroded	RsD2	22.06	22.07	14
	STARK	Rittman silt loam, 6 to 12 percent slopes, moderately eroded	RsC2	22.07	22.13	352
	STARK	Wadsworth silt loam, 2 to 6 percent slopes	WaB	22.13	22.24	566
	STARK	Wadsworth silt loam, 6 to 12 percent slopes, moderately eroded	WaC2	22.24	22.27	161
	STARK	Shoals silt loam	Sh	22.27	22.30	137
	STARK	Wadsworth silt loam, 2 to 6 percent slopes	WaB	22.30	22.33	155
	STARK	Rittman silt loam, 6 to 12 percent slopes, moderately eroded	RsC2	22.33	22.43	546
	STARK	Wadsworth silt loam, 6 to 12 percent slopes, moderately eroded	WaC2	22.43	22.48	286
	STARK	Sebring silt loam, till substratum	Se	22.48	22.50	107
	STARK	Wadsworth silt loam, 6 to 12 percent slopes, moderately eroded	WaC2	22.50	22.53	141
	STARK	Wadsworth silt loam, 2 to 6 percent slopes	WaB	22.53	22.62	482
	STARK	Wadsworth silt loam, 6 to 12 percent slopes, moderately eroded	WaC2	22.62	22.71	447
	STARK	Wadsworth silt loam, 2 to 6 percent slopes	WaB	22.71	22.80	489
	STARK	Wadsworth silt loam, 6 to 12 percent slopes, moderately eroded	WaC2	22.80	22.85	281
	STARK	Wadsworth silt loam, 2 to 6 percent slopes	WaB	22.85	23.29	2319
	STARK	Sebring silt loam, till substratum	Se	23.29	23.36	339

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	STARK	Wadsworth silt loam, 2 to 6 percent slopes	WaB	23.36	23.39	162
	STARK	Sebring silt loam, till substratum	Se	23.39	23.41	120
	STARK	Wadsworth silt loam, 2 to 6 percent slopes	WaB	23.41	23.63	1163
	STARK	Wadsworth silt loam, 0 to 2 percent slopes	WaA	23.63	23.77	729
	STARK	Wadsworth silt loam, 2 to 6 percent slopes	WaB	23.77	23.80	178
	STARK	Weinbach silt loam, 0 to 2 percent slopes	WhA	23.80	23.83	177
	STARK	Sloan silt loam	Sl	23.83	23.91	381
	STARK	Ravenna silt loam, 0 to 2 percent slopes	ReA	23.91	24.08	923
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	24.08	24.16	427
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	24.16	24.29	694
	STARK	Wooster silt loam, 6 to 12 percent slopes, moderately eroded	WuC2	24.29	24.41	637
	STARK	Luray silt loam	Ly	24.41	24.43	79
	STARK	Wooster silt loam, 6 to 12 percent slopes, moderately eroded	WuC2	24.43	24.50	362
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	24.50	24.51	87
	STARK	Wooster silt loam, 6 to 12 percent slopes, moderately eroded	WuC2	24.51	24.61	510
	STARK	Canfield silt loam, 6 to 12 percent slopes, moderately eroded	CdC2	24.61	24.63	82
	STARK	Wooster silt loam, 6 to 12 percent slopes, moderately eroded	WuC2	24.63	24.67	209
	STARK	Wooster silt loam, 12 to 18 percent slopes, moderately eroded	WuD2	24.67	24.71	231
	STARK	Wooster silt loam, 6 to 12 percent slopes, moderately eroded	WuC2	24.71	24.73	100

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	24.73	24.86	697
	STARK	Luray silt loam	Ly	24.86	24.90	221
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	24.90	24.91	62
	STARK	Wooster silt loam, 6 to 12 percent slopes, moderately eroded	WuC2	24.91	24.93	71
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	24.93	24.97	200
	STARK	Luray silt loam	Ly	24.97	24.99	114
	STARK	Weinbach silt loam, 0 to 2 percent slopes	WhA	24.99	25.07	450
	STARK	Fitchville silt loam, 0 to 2 percent slopes	FcA	25.07	25.15	418
	STARK	Wooster silt loam, 6 to 12 percent slopes	WuC	25.15	25.22	354
	STARK	Chili gravelly loam, 6 to 12 percent slopes, moderately eroded	CoC2	25.22	25.24	139
	STARK	Chili loam, 2 to 6 percent slopes	CnB	25.24	25.29	240
	STARK	Chili gravelly loam, 6 to 12 percent slopes, moderately eroded	CoC2	25.29	25.37	416
	STARK	Chili loam, 2 to 6 percent slopes	CnB	25.37	25.57	1045
	STARK	Ravenna silt loam, 0 to 2 percent slopes	ReA	25.57	25.59	109
	STARK	Chili gravelly loam, 6 to 12 percent slopes	CoC	25.59	25.73	732
	STARK	Bogart silt loam, 2 to 6 percent slopes	BoB	25.73	25.75	148
	STARK	Chili silt loam, 6 to 12 percent slopes, moderately eroded	CpC2	25.75	25.87	595
	STARK	Chili silt loam, 0 to 2 percent slopes	CpA	25.87	25.91	212
	STARK	Chili silt loam, 2 to 6 percent slopes	CpB	25.91	25.93	135
	STARK	Luray silt loam, gravelly subsoil variant	Lz	25.93	26.23	1578
	STARK	Chili silt loam, 6 to 12 percent slopes	CpC	26.23	26.39	837

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	STARK	Weinbach silt loam, 0 to 2 percent slopes	WhA	26.39	26.49	523
	STARK	Luray silt loam	Ly	26.49	26.51	136
	STARK	Sloan silt loam	Sl	26.51	26.54	150
	STARK	Willette muck	Wt	26.54	26.59	257
	STARK	Fitchville silt loam, 0 to 2 percent slopes	FcA	26.59	26.64	274
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	26.64	26.67	165
	STARK	Wooster silt loam, 12 to 18 percent slopes, moderately eroded	WuD2	26.67	26.71	185
	STARK	Canfield silt loam, 2 to 6 percent slopes	CdB	26.71	26.76	240
	STARK	Chili silt loam, 2 to 6 percent slopes	CpB	26.76	26.80	257
	STARK	Wooster silt loam, 6 to 12 percent slopes, moderately eroded	WuC2	26.80	26.86	275
	STARK	Ravenna silt loam, 2 to 6 percent slopes	ReB	26.86	26.93	381
	STARK	Carlisle muck	Ch	26.93	27.06	696
	STARK	Chili silt loam, 2 to 6 percent slopes	CpB	27.06	27.15	493
	STARK	Willette muck	Wt	27.15	27.25	489
	STARK	Fitchville silt loam, 0 to 2 percent slopes	FcA	27.25	27.25	7
	STARK	Chili silt loam, 6 to 12 percent slopes, moderately eroded	CpC2	27.25	27.32	390
	STARK	Fitchville silt loam, 0 to 2 percent slopes	FcA	27.32	27.33	23
	STARK	Chili silt loam, 6 to 12 percent slopes, moderately eroded	CpC2	27.33	27.43	566
	STARK	Fitchville silt loam, 0 to 2 percent slopes	FcA	27.43	27.46	125
	STARK	Chili silt loam, 6 to 12 percent slopes, moderately eroded	CpC2	27.46	27.52	312
	STARK	Fitchville silt loam, 0 to 2 percent slopes	FcA	27.52	27.55	196

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	STARK	Chili silt loam, 6 to 12 percent slopes, moderately eroded	CpC2	27.55	27.62	363
	STARK	Chili silt loam, 2 to 6 percent slopes	CpB	27.62	27.89	1419
	STARK	Fitchville silt loam, 0 to 2 percent slopes	FcA	27.89	27.93	232
	STARK	Bogart silt loam, 2 to 6 percent slopes	BoB	27.93	28.13	1051
	STARK	Fitchville silt loam, 0 to 2 percent slopes	FcA	28.13	28.24	559
	STARK	Chili silt loam, 2 to 6 percent slopes	CpB	28.24	28.39	821
	STARK	Chili silt loam, 6 to 12 percent slopes, moderately eroded	CpC2	28.39	28.42	140
	STARK	Chili silt loam, 2 to 6 percent slopes	CpB	28.42	28.48	329
	STARK	Weinbach silt loam, 0 to 2 percent slopes	WhA	28.48	28.50	62
	STARK	Sebring silt loam	Sb	28.50	28.55	294
	STARK	Luray silt loam	Ly	28.55	28.61	334
	STARK	Fitchville silt loam, 0 to 2 percent slopes	FcA	28.61	28.68	329
	STARK	Weinbach silt loam, 0 to 2 percent slopes	WhA	28.68	28.73	258
	STARK	Chili silt loam, 6 to 12 percent slopes	CpC	28.73	28.82	526
	STARK	Fitchville silt loam, 0 to 2 percent slopes	FcA	28.82	28.85	149
	STARK	Willette muck	Wt	28.85	28.90	264
	STARK	Luray silt loam	Ly	28.90	28.93	158
	STARK	Weinbach silt loam, 0 to 2 percent slopes	WhA	28.93	28.94	39
	STARK	Weinbach silt loam, 2 to 6 percent slopes	WhB	28.94	28.99	278
	STARK	Weinbach silt loam, 0 to 2 percent slopes	WhA	28.99	28.99	10
	STARK	Carlisle muck	Ch	28.99	29.01	102
	STARK	Weinbach silt loam, 0 to 2 percent slopes	WhA	29.01	29.04	113

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	STARK	Carlisle muck	Ch	29.04	29.05	91
	STARK	Luray silt loam	Ly	29.05	29.08	138
	STARK	Weinbach silt loam, 2 to 6 percent slopes	WhB	29.08	29.10	98
	STARK	Luray silt loam	Ly	29.10	29.13	159
	STARK	Fitchville silt loam, 2 to 6 percent slopes	FcB	29.13	29.14	87
	STARK	Chili gravelly loam, 12 to 18 percent slopes, moderately eroded	CoD2	29.14	29.16	103
	STARK	Chili silt loam, 6 to 12 percent slopes, moderately eroded	CpC2	29.16	29.21	230
	STARK	Carlisle muck	Ch	29.21	29.25	224
	STARK	Chili silt loam, 6 to 12 percent slopes, moderately eroded	CpC2	29.25	29.31	316
	STARK	Chili gravelly loam, 12 to 18 percent slopes, moderately eroded	CoD2	29.31	29.33	90
	STARK	Glenford silt loam, 2 to 6 percent slopes	GfB	29.33	29.36	167
	STARK	Luray silt loam	Ly	29.36	29.45	492
	STARK	Glenford silt loam, 2 to 6 percent slopes	GfB	29.45	29.48	151
	STARK	Wheeling silt loam, 2 to 6 percent slopes	WrB	29.48	29.53	280
	STARK	Chili gravelly loam, 6 to 12 percent slopes	CoC	29.53	29.62	481
	STARK	Fitchville silt loam, 0 to 2 percent slopes	FcA	29.62	29.66	202
	STARK	Conotton gravelly loam, 12 to 18 percent slopes, moderately eroded	CyD2	29.66	29.69	160
	STARK	Chili gravelly loam, 6 to 12 percent slopes	CoC	29.69	29.71	111
	STARK	Conotton gravelly loam, 12 to 18 percent slopes, moderately eroded	CyD2	29.71	29.78	361
	STARK	Chili gravelly loam, 6 to 12 percent slopes	CoC	29.78	29.85	348
	STARK	Bogart silt loam, 2 to 6 percent slopes	BoB	29.85	29.87	142

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	STARK	Luray silt loam	Ly	29.87	29.92	230
	STARK	Fitchville silt loam, 0 to 2 percent slopes	FcA	29.92	29.92	2
	STARK	Chili silt loam, 2 to 6 percent slopes	CpB	29.92	29.97	271
	STARK	Fitchville silt loam, 0 to 2 percent slopes	FcA	29.97	29.99	127
	STARK	Weinbach silt loam, 0 to 2 percent slopes	WhA	29.99	30.02	145
	STARK	Luray silt loam	Ly	30.02	30.04	112
	STARK	Shoals silt loam	Sh	30.04	30.08	214
	STARK	Mentor silt loam, 2 to 6 percent slopes	MeB	30.08	30.12	175
	STARK	Wooster silt loam, 6 to 12 percent slopes, moderately eroded	WuC2	30.12	30.28	863
	STARK	Wheeling silt loam, 2 to 6 percent slopes	WrB	30.28	30.42	726
	STARK	Chili silt loam, 2 to 6 percent slopes	CpB	30.42	30.60	986
	STARK	Luray silt loam	Ly	30.60	30.62	77
	STARK	Chili silt loam, 2 to 6 percent slopes	CpB	30.62	30.87	1309
	STARK	Bogart silt loam, 0 to 2 percent slopes	BoA	30.87	30.90	163
	STARK	Weinbach silt loam, 0 to 2 percent slopes	WhA	30.90	30.94	205
	STARK	Bogart silt loam, 0 to 2 percent slopes	BoA	30.94	31.01	412
	STARK	Sebring silt loam	Sb	31.01	31.20	957
	STARK	Latham silt loam, 12 to 18 percent slopes	LaD	31.20	31.25	289
	STARK	Weinbach silt loam, 2 to 6 percent slopes	WhB	31.25	31.27	102
	STARK	Chili silt loam, 6 to 12 percent slopes	CpC	31.27	31.29	118
	STARK	Sebring silt loam	Sb	31.29	31.41	620
	STARK	Weinbach silt loam, 2 to 6 percent slopes	WhB	31.41	31.45	236

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	STARK	Chili silt loam, 6 to 12 percent slopes, moderately eroded	CpC2	31.45	31.47	60
	STARK	Chili gravelly loam, 12 to 18 percent slopes, moderately eroded	CoD2	31.47	31.49	133
	STARK	Wheeling silt loam, 6 to 12 percent slopes	WrC	31.49	31.55	309
	STARK	Chili silt loam, 6 to 12 percent slopes	CpC	31.55	31.61	335
	STARK	Chili silt loam, 2 to 6 percent slopes	CpB	31.61	31.67	289
	STARK	Weinbach silt loam, 2 to 6 percent slopes	WhB	31.67	31.71	223
	STARK	Chili silt loam, 6 to 12 percent slopes	CpC	31.71	31.75	217
	STARK	Conotton gravelly loam, 18 to 25 percent slopes, moderately eroded	CyE2	31.75	31.81	339
	STARK	Chili silt loam, 2 to 6 percent slopes	CpB	31.81	31.95	716
	STARK	Chili silt loam, 6 to 12 percent slopes	CpC	31.95	32.02	346
	STARK	Chili silt loam, 2 to 6 percent slopes	CpB	32.02	32.05	163
	STARK	Chili silt loam, 6 to 12 percent slopes	CpC	32.05	32.10	306
	STARK	Chili gravelly loam, 12 to 18 percent slopes, moderately eroded	CoD2	32.10	32.13	114
	STARK	Chili silt loam, 2 to 6 percent slopes	CpB	32.13	32.15	110
	STARK	Chili silt loam, 6 to 12 percent slopes, moderately eroded	CpC2	32.15	32.19	237
	STARK	Chili silt loam, 2 to 6 percent slopes	CpB	32.19	32.26	348
	STARK	Chili silt loam, 6 to 12 percent slopes, moderately eroded	CpC2	32.26	32.37	592
	STARK	Conotton gravelly loam, 18 to 25 percent slopes, moderately eroded	CyE2	32.37	32.38	38

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	STARK	Chili gravelly loam, 12 to 18 percent slopes, moderately eroded	CoD2	32.38	32.41	196
	STARK	Chili silt loam, 0 to 2 percent slopes	CpA	32.41	32.47	317
	STARK	Chili gravelly loam, 12 to 18 percent slopes, moderately eroded	CoD2	32.47	32.48	18
	STARK	Chili silt loam, 6 to 12 percent slopes	CpC	32.48	32.52	234
	STARK	Damascus loam	Da	32.52	32.67	759
	STARK	Carlisle muck	Ch	32.67	32.72	295
	STARK	Carlisle muck	Cg	32.72	32.74	75
	SUMMIT	Carlisle muck	Cg	32.74	32.74	12
	SUMMIT	Damascus loam	Da	32.74	32.76	116
	SUMMIT	Carlisle muck	Cg	32.76	32.80	222
	SUMMIT	Linwood muck	Ld	32.80	33.02	1160
	SUMMIT	Glenford silt loam, 0 to 2 percent slopes	GfA	33.02	33.08	332
	SUMMIT	Chili silt loam, 2 to 6 percent slopes	CpB	33.08	33.12	182
	SUMMIT	Conotton-Oshtemo complex, 18 to 25 percent slopes	CyE	33.12	33.15	164
	SUMMIT	Oshtemo sandy loam, 6 to 12 percent slopes	OsC	33.15	33.20	249
	SUMMIT	Chili silt loam, 2 to 6 percent slopes	CpB	33.20	33.24	232
	SUMMIT	Wheeling silt loam, 0 to 2 percent slopes	WrA	33.24	33.29	260
	SUMMIT	Chili silt loam, 2 to 6 percent slopes	CpB	33.29	33.46	899
	SUMMIT	Chili silt loam, 6 to 12 percent slopes	CpC	33.46	33.48	123
	SUMMIT	Canfield silt loam, 2 to 6 percent slopes	CdB	33.48	33.74	1338
	SUMMIT	Wooster silt loam, 6 to 12 percent slopes	WuC	33.74	33.76	106
	SUMMIT	Canfield silt loam, 2 to 6 percent slopes	CdB	33.76	33.77	64

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	SUMMIT	Ravenna silt loam, 0 to 2 percent slopes	ReA	33.77	33.78	28
	SUMMIT	Canfield silt loam, 2 to 6 percent slopes	CdB	33.78	33.80	140
	SUMMIT	Udorthents	Ua	33.80	33.88	402
	SUMMIT	Fitchville silt loam, 0 to 2 percent slopes	FcA	33.88	33.98	532
	SUMMIT	Ravenna silt loam, 0 to 2 percent slopes	ReA	33.98	34.05	369
	SUMMIT	Canfield silt loam, 2 to 6 percent slopes	CdB	34.05	34.09	193
	SUMMIT	Ravenna silt loam, 0 to 2 percent slopes	ReA	34.09	34.12	191
	SUMMIT	Canfield silt loam, 2 to 6 percent slopes	CdB	34.12	34.22	537
	SUMMIT	Ravenna silt loam, 0 to 2 percent slopes	ReA	34.22	34.26	186
	SUMMIT	Fitchville silt loam, 0 to 2 percent slopes	FcA	34.26	34.34	443
	SUMMIT	Sebring silt loam	Sb	34.34	34.42	411
	SUMMIT	Ravenna silt loam, 0 to 2 percent slopes	ReA	34.42	34.46	190
	SUMMIT	Ravenna silt loam, 2 to 6 percent slopes	ReB	34.46	34.54	453
	SUMMIT	Canfield silt loam, 2 to 6 percent slopes	CdB	34.54	34.58	217
	SUMMIT	Fitchville silt loam, 0 to 2 percent slopes	FcA	34.58	34.67	471
	SUMMIT	Ravenna silt loam, 0 to 2 percent slopes	ReA	34.67	34.77	501
	SUMMIT	Canfield silt loam, 2 to 6 percent slopes	CdB	34.77	34.85	436
	SUMMIT	Ravenna silt loam, 0 to 2 percent slopes	ReA	34.85	34.88	155
	SUMMIT	Canfield silt loam, 2 to 6 percent slopes	CdB	34.88	35.05	899
	SUMMIT	Ravenna silt loam, 2 to 6 percent slopes	ReB	35.05	35.26	1112
	SUMMIT	Canfield silt loam, 2 to 6 percent slopes	CdB	35.26	35.35	499

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	SUMMIT	Canadice silty clay loam	Ca	35.35	35.43	376
	SUMMIT	Fitchville silt loam, 0 to 2 percent slopes	FcA	35.43	35.44	83
	SUMMIT	Bogart loam, 0 to 2 percent slopes	BgA	35.44	35.48	182
	SUMMIT	Wooster silt loam, 2 to 6 percent slopes	WuB	35.48	35.53	294
	SUMMIT	Canfield silt loam, 2 to 6 percent slopes	CdB	35.53	35.61	393
	SUMMIT	Canfield silt loam, 6 to 12 percent slopes	CdC	35.61	35.63	124
	SUMMIT	Canfield silt loam, 2 to 6 percent slopes	CdB	35.63	35.66	165
	SUMMIT	Canfield silt loam, 6 to 12 percent slopes	CdC	35.66	35.72	314
	SUMMIT	Canfield silt loam, 2 to 6 percent slopes	CdB	35.72	35.79	388
	SUMMIT	Wooster silt loam, 12 to 18 percent, moderately eroded	WuD2	35.79	35.82	130
	SUMMIT	Chili silt loam, 6 to 12 percent slopes	CpC	35.82	35.85	150
	SUMMIT	Wooster silt loam, 12 to 18 percent, moderately eroded	WuD2	35.85	35.95	524
	SUMMIT	Chili silt loam, 6 to 12 percent slopes	CpC	35.95	36.01	311
	SUMMIT	Chili loam, 0 to 2 percent slopes	CnA	36.01	36.04	194
	SUMMIT	Chili silt loam, 6 to 12 percent slopes	CpC	36.04	36.09	257
	SUMMIT	Sebring silt loam	Sb	36.09	36.14	236
	SUMMIT	Chili silt loam, 6 to 12 percent slopes	CpC	36.14	36.15	61
	SUMMIT	Chili silt loam, 0 to 2 percent slopes	CpA	36.15	36.27	677
	SUMMIT	Oshtemo sandy loam, 6 to 12 percent slopes	OsC	36.27	36.34	320
	SUMMIT	Conotton-Oshtemo complex, 12 to 18 percent slopes	CyD	36.34	36.38	255
	SUMMIT	Sebring silt loam	Sb	36.38	36.42	186
	SUMMIT	Chili silt loam, 6 to 12 percent slopes	CpC	36.42	36.46	204

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	SUMMIT	Chili silt loam, 2 to 6 percent slopes	CpB	36.46	36.57	614
	SUMMIT	Chili silt loam, 6 to 12 percent slopes	CpC	36.57	36.62	257
	SUMMIT	Sebring silt loam	Sb	36.62	36.71	478
	SUMMIT	Glenford silt loam, 0 to 2 percent slopes	GfA	36.71	36.74	167
	SUMMIT	Chili silt loam, 6 to 12 percent slopes	CpC	36.74	36.92	948
	SUMMIT	Chili silt loam, 2 to 6 percent slopes	CpB	36.92	37.00	388
	SUMMIT	Conotton-Oshtemo complex, 12 to 18 percent slopes	CyD	37.00	37.02	125
	SUMMIT	Chili silt loam, 2 to 6 percent slopes	CpB	37.02	37.04	81
	SUMMIT	Conotton-Oshtemo complex, 12 to 18 percent slopes	CyD	37.04	37.06	120
	SUMMIT	Chili loam, 6 to 12 percent slopes	CnC	37.06	37.08	102
	SUMMIT	Conotton-Oshtemo complex, 12 to 18 percent slopes	CyD	37.08	37.12	208
	SUMMIT	Oshtemo sandy loam, 2 to 6 percent slopes	OsB	37.12	37.14	110
	SUMMIT	Sebring silt loam	Sb	37.14	37.16	104
	SUMMIT	Oshtemo sandy loam, 2 to 6 percent slopes	OsB	37.16	37.23	398
	SUMMIT	Conotton-Oshtemo complex, 12 to 18 percent slopes	CyD	37.23	37.30	366
	SUMMIT	Carlisle muck	Cg	37.30	37.35	221
	SUMMIT	Wooster silt loam, 6 to 12 percent slopes	WuC	37.35	37.38	178
	SUMMIT	Carlisle muck	Cg	37.38	37.46	429
	SUMMIT	Glenford silt loam, 2 to 6 percent slopes	GfB	37.46	37.54	419
	SUMMIT	Carlisle muck	Cg	37.54	37.57	152
	SUMMIT	Chili silt loam, 6 to 12 percent slopes	CpC	37.57	37.67	535
	SUMMIT	Carlisle muck	Cg	37.67	37.85	961

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	SUMMIT	Wooster silt loam, 12 to 18 percent slopes	WuD	37.85	37.96	595
	SUMMIT	Carlisle muck	Cg	37.96	38.25	1490
	SUMMIT	Chili loam, 2 to 6 percent slopes	CnB	38.25	38.27	144
	SUMMIT	Carlisle muck	Cg	38.27	38.30	125
	SUMMIT	Chili loam, 2 to 6 percent slopes	CnB	38.30	38.40	519
	SUMMIT	Conotton-Oshtemo complex, 12 to 18 percent slopes	CyD	38.40	38.44	238
	SUMMIT	Lorain silty clay loam	Ln	38.44	38.46	97
	SUMMIT	Glenford silt loam, 2 to 6 percent slopes	GfB	38.46	38.62	870
	SUMMIT	Sebring silt loam	Sb	38.62	38.67	266
	SUMMIT	Carlisle muck	Cg	37.67	37.85	961
	SUMMIT	Wooster silt loam, 12 to 18 percent slopes	WuD	37.85	37.96	595
	SUMMIT	Carlisle muck	Cg	37.96	38.25	1490
	SUMMIT	Chili loam, 2 to 6 percent slopes	CnB	38.25	38.27	144
	SUMMIT	Carlisle muck	Cg	38.27	38.30	125
	SUMMIT	Chili loam, 2 to 6 percent slopes	CnB	38.30	38.40	519
	SUMMIT	Conotton-Oshtemo complex, 12 to 18 percent slopes	CyD	38.40	38.44	238
	SUMMIT	Lorain silty clay loam	Ln	38.44	38.46	97
	SUMMIT	Glenford silt loam, 2 to 6 percent slopes	GfB	38.46	38.62	870
	SUMMIT	Sebring silt loam	Sb	38.62	38.67	266
	SUMMIT	Fitchville silt loam, 0 to 2 percent slopes	FcA	38.67	38.72	252
	SUMMIT	Sebring silt loam	Sb	38.72	38.74	115
	SUMMIT	Damascus loam	Da	38.74	38.80	287
	SUMMIT	Chili-Wooster complex, 6 to 12 percent slopes, moderately eroded	CwC2	38.80	39.03	1235
	SUMMIT	Chili loam, 2 to 6 percent slopes	CnB	39.03	39.19	827
	SUMMIT	Chili-Wooster complex, 6 to 12 percent slopes, moderately eroded	CwC2	39.19	39.27	403

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	SUMMIT	Chili gravelly loam, 12 to 18 percent slopes, moderately eroded	CoD2	39.27	39.29	113
	SUMMIT	Chili-Wooster complex, 6 to 12 percent slopes, moderately eroded	CwC2	39.29	39.49	1066
	SUMMIT	Conotton-Oshtemo complex, 25 to 50 percent slopes	CyF	39.49	39.53	231
	SUMMIT	Udorthents, sanitary landfill	Uf	39.53	39.63	523
	SUMMIT	Conotton-Oshtemo complex, 12 to 18 percent slopes	CyD	39.63	39.63	15
	SUMMIT	Carlisle muck	Cg	39.63	39.93	1563
	SUMMIT	Jimtown loam, 0 to 2 percent slopes	JtA	39.93	40.05	607
	SUMMIT	Wooster silt loam, 6 to 12 percent slopes, moderately eroded	WuC2	40.05	40.06	90
	SUMMIT	Jimtown loam, 0 to 2 percent slopes	JtA	40.06	40.08	81
	SUMMIT	Wooster silt loam, 6 to 12 percent slopes, moderately eroded	WuC2	40.08	40.25	891
	SUMMIT	Chili gravelly loam, 6 to 12 percent slopes, moderately eroded	CoC2	40.25	40.30	264
	SUMMIT	Chili silt loam, 2 to 6 percent slopes	CpB	40.30	40.35	284
	SUMMIT	Udorthents, sanitary landfill	Uf	40.35	40.36	43
	SUMMIT	Orrville silt loam	Or	40.36	40.40	245
	SUMMIT	Bogart loam, 2 to 6 percent slopes	BgB	40.40	40.41	33
	SUMMIT	Wooster silt loam, 18 to 25 percent slopes, moderately eroded	WuE2	40.41	40.44	145
	SUMMIT	Canfield silt loam, 2 to 6 percent slopes	CdB	40.44	40.53	472
	SUMMIT	Wooster silt loam, 12 to 18 percent, moderately eroded	WuD2	40.53	40.59	306
	SUMMIT	Wooster silt loam, 6 to 12 percent slopes, moderately eroded	WuC2	40.59	40.61	115

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	SUMMIT	Wooster silt loam, 12 to 18 percent, moderately eroded	WuD2	40.61	40.63	131
	SUMMIT	Wooster silt loam, 2 to 6 percent slopes	WuB	40.63	41.14	2658
	SUMMIT	Wooster silt loam, 6 to 12 percent slopes, moderately eroded	WuC2	41.14	41.17	197
	SUMMIT	Chili gravelly loam, 12 to 18 percent slopes, moderately eroded	CoD2	41.17	41.23	276
	SUMMIT	Wooster silt loam, 6 to 12 percent slopes, moderately eroded	WuC2	41.23	41.33	545
	SUMMIT	Wooster silt loam, 2 to 6 percent slopes	WuB	41.33	41.38	267
	SUMMIT	Wooster silt loam, 6 to 12 percent slopes, moderately eroded	WuC2	41.38	41.41	181
	SUMMIT	Loudonville silt loam, 12 to 18 percent slopes	LoD	41.41	41.45	189
	SUMMIT	Wooster silt loam, 2 to 6 percent slopes	WuB	41.45	41.48	175
	SUMMIT	Wooster silt loam, 6 to 12 percent slopes, moderately eroded	WuC2	41.48	41.55	359
	SUMMIT	Wooster silt loam, 2 to 6 percent slopes	WuB	41.55	41.58	179
	SUMMIT	Canfield silt loam, 2 to 6 percent slopes	CdB	41.58	41.69	553
	SUMMIT	Wooster silt loam, 6 to 12 percent slopes, moderately eroded	WuC2	41.69	41.78	505
	SUMMIT	Canfield silt loam, 2 to 6 percent slopes	CdB	41.78	41.84	292
	SUMMIT	Sebring silt loam	Sb	41.84	41.89	242
	SUMMIT	Canfield silt loam, 0 to 2 percent slopes	CdA	41.89	41.91	132
	SUMMIT	Glenford silt loam, 2 to 6 percent slopes	GfB	41.91	41.93	106
	SUMMIT	Sebring silt loam	Sb	41.93	41.94	26
	SUMMIT	Chili silt loam, 2 to 6 percent slopes	CpB	41.94	42.05	611

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	SUMMIT	Sebring silt loam	Sb	42.05	42.14	469
	SUMMIT	Wooster silt loam, 6 to 12 percent slopes, moderately eroded	WuC2	42.14	42.17	169
	SUMMIT	Wooster silt loam, 2 to 6 percent slopes	WuB	42.17	42.22	243
	SUMMIT	Wooster silt loam, 6 to 12 percent slopes, moderately eroded	WuC2	42.22	42.30	445
	SUMMIT	Wooster silt loam, 2 to 6 percent slopes	WuB	42.30	42.37	331
	SUMMIT	Wooster silt loam, 6 to 12 percent slopes, moderately eroded	WuC2	42.37	42.48	629
	SUMMIT	Wooster silt loam, 2 to 6 percent slopes	WuB	42.48	42.50	86
	SUMMIT	Canfield silt loam, 2 to 6 percent slopes	CdB	42.50	42.94	2337
	SUMMIT	Wooster silt loam, 2 to 6 percent slopes	WuB	42.94	42.96	79
	SUMMIT	Wooster silt loam, 6 to 12 percent slopes, moderately eroded	WuC2	42.96	42.98	137
	SUMMIT	Wooster silt loam, 12 to 18 percent, moderately eroded	WuD2	42.98	43.01	146
	SUMMIT	Jimtown loam, 0 to 2 percent slopes	JtA	43.01	43.07	294
	SUMMIT	Bogart loam, 0 to 2 percent slopes	BgA	43.07	43.16	466
	SUMMIT	Sebring silt loam	Sb	43.16	43.30	781
	SUMMIT	Jimtown loam, 0 to 2 percent slopes	JtA	43.30	43.43	677
	SUMMIT	Wooster silt loam, 6 to 12 percent slopes, moderately eroded	WuC2	43.43	43.45	79
	SUMMIT	Wooster silt loam, 12 to 18 percent slopes	WuD	43.45	43.49	235
	SUMMIT	Wooster silt loam, 6 to 12 percent slopes, moderately eroded	WuC2	43.49	43.78	1508
	SUMMIT	Canfield silt loam, 2 to 6 percent slopes	CdB	43.78	43.89	601

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	SUMMIT	Wooster silt loam, 12 to 18 percent, moderately eroded	WuD2	43.89	43.96	382
	SUMMIT	Wooster silt loam, 6 to 12 percent slopes, moderately eroded	WuC2	43.96	43.97	51
	SUMMIT	Wooster silt loam, 12 to 18 percent, moderately eroded	WuD2	43.97	44.00	151
	SUMMIT	Wooster silt loam, 6 to 12 percent slopes, moderately eroded	WuC2	44.00	44.06	314
	SUMMIT	Wooster silt loam, 12 to 18 percent, moderately eroded	WuD2	44.06	44.12	295
	SUMMIT	Wooster silt loam, 6 to 12 percent slopes, moderately eroded	WuC2	44.12	44.14	105
	SUMMIT	Canfield silt loam, 2 to 6 percent slopes	CdB	44.14	44.15	90
	SUMMIT	Wooster silt loam, 6 to 12 percent slopes, moderately eroded	WuC2	44.15	44.38	1190
	SUMMIT	Wooster silt loam, 12 to 18 percent, moderately eroded	WuD2	44.38	44.41	141
	SUMMIT	Wooster silt loam, 6 to 12 percent slopes, moderately eroded	WuC2	44.41	44.43	118
	SUMMIT	Wooster silt loam, 12 to 18 percent, moderately eroded	WuD2	44.43	44.45	102
	SUMMIT	Wooster silt loam, 6 to 12 percent slopes, moderately eroded	WuC2	44.45	44.50	281
	SUMMIT	Wooster silt loam, 18 to 25 percent slopes, moderately eroded	WuE2	44.50	44.57	343
	SUMMIT	Chili gravelly loam, 6 to 12 percent slopes, moderately eroded	CoC2	44.57	44.59	102
	SUMMIT	Bogart loam, 2 to 6 percent slopes	BgB	44.59	44.69	563
	SUMMIT	Holly silt loam	Ho	44.69	44.73	216
	SUMMIT	Fitchville silt loam, 2 to 6 percent slopes	FcB	44.73	44.77	188

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	SUMMIT	Wooster silt loam, 6 to 12 percent slopes, moderately eroded	WuC2	44.77	44.89	665
	SUMMIT	Wooster silt loam, 12 to 18 percent, moderately eroded	WuD2	44.89	44.95	284
	SUMMIT	Wooster silt loam, 25 to 50 percent slopes, moderately eroded	WuF2	44.95	44.99	209
	SUMMIT	Wooster silt loam, 12 to 18 percent, moderately eroded	WuD2	44.99	45.03	199
	SUMMIT	Wooster silt loam, 6 to 12 percent slopes, moderately eroded	WuC2	45.03	45.27	1281
	SUMMIT	Wooster silt loam, 2 to 6 percent slopes	WuB	45.27	45.34	364
	SUMMIT	Canfield silt loam, 2 to 6 percent slopes	CdB	45.34	45.38	212
	SUMMIT	Wooster silt loam, 2 to 6 percent slopes	WuB	45.38	45.43	273
	SUMMIT	Canfield silt loam, 2 to 6 percent slopes	CdB	45.43	45.47	220
	SUMMIT	Wooster silt loam, 2 to 6 percent slopes	WuB	45.47	45.56	464
	SUMMIT	Canfield silt loam, 2 to 6 percent slopes	CdB	45.56	45.58	114
	SUMMIT	Wooster silt loam, 2 to 6 percent slopes	WuB	45.58	45.67	484
	SUMMIT	Loudonville silt loam, 12 to 18 percent slopes	LoD	45.67	45.73	316
	SUMMIT	Dekalb sandy loam, 25 to 70 percent slopes	DkF	45.73	45.77	199
	SUMMIT	Oshtemo sandy loam, 2 to 6 percent slopes	OsB	45.77	45.78	72
	SUMMIT	Wheeling silt loam, 2 to 6 percent slopes	WrB	45.78	45.85	365
	SUMMIT	Chili loam, 2 to 6 percent slopes	CnB	45.85	45.95	526
	SUMMIT	Holly silt loam, alkaline	Hy	45.95	45.99	194
	SUMMIT	Chagrin silt loam, alkaline	Ck	45.99	46.00	76
	SUMMIT	Water	W	46.00	46.02	96

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	SUMMIT	Udorthents, sanitary landfill	Uf	46.02	46.05	131
	SUMMIT	Loudonville silt loam, 2 to 6 percent slopes	LoB	46.05	46.07	140
	SUMMIT	Wooster silt loam, 12 to 18 percent, moderately eroded	WuD2	46.07	46.14	334
	SUMMIT	Wooster silt loam, 6 to 12 percent slopes, moderately eroded	WuC2	46.14	46.17	196
	SUMMIT	Wooster silt loam, 2 to 6 percent slopes	WuB	46.17	46.27	518
	SUMMIT	Canfield silt loam, 2 to 6 percent slopes	CdB	46.27	46.43	823
	SUMMIT	Wooster silt loam, 2 to 6 percent slopes	WuB	46.43	46.54	616
	SUMMIT	Wooster silt loam, 6 to 12 percent slopes, moderately eroded	WuC2	46.54	46.72	940
	SUMMIT	Canfield silt loam, 2 to 6 percent slopes	CdB	46.72	46.74	121
	SUMMIT	Holly silt loam	Ho	46.74	46.80	282
	SUMMIT	Chili silt loam, 2 to 6 percent slopes	CpB	46.80	46.84	242
	SUMMIT	Sebring silt loam	Sb	46.84	46.87	145
	SUMMIT	Wheeling silt loam, 2 to 6 percent slopes	WrB	46.87	46.89	78
	SUMMIT	Sebring silt loam	Sb	46.89	46.91	123
	SUMMIT	Chili loam, 2 to 6 percent slopes	CnB	46.91	46.95	235
	SUMMIT	Bogart loam, 0 to 2 percent slopes	BgA	46.95	46.99	218
	SUMMIT	Sebring silt loam	Sb	46.99	47.05	284
	SUMMIT	Chili silt loam, 2 to 6 percent slopes	CpB	47.05	47.09	217
	SUMMIT	Sebring silt loam	Sb	47.09	47.18	455
	SUMMIT	Ravenna silt loam, 2 to 6 percent slopes	ReB	47.18	47.29	592
	SUMMIT	Canfield silt loam, 6 to 12 percent slopes, moderately eroded	CdC2	47.29	47.33	200
	SUMMIT	Canfield silt loam, 2 to 6 percent slopes	CdB	47.33	47.46	721

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	SUMMIT	Canfield silt loam, 6 to 12 percent slopes, moderately eroded	CdC2	47.46	47.57	564
	SUMMIT	Fitchville silt loam, 0 to 2 percent slopes	FcA	47.57	47.72	816
	SUMMIT	Canfield silt loam, 2 to 6 percent slopes	CdB	47.72	47.79	348
	SUMMIT	Ravenna silt loam, 2 to 6 percent slopes	ReB	47.79	47.81	105
	SUMMIT	Canfield silt loam, sandstone substratum, 2 to 6 percent slopes	CeB	47.81	47.86	271
	SUMMIT	Canfield silt loam, 2 to 6 percent slopes	CdB	47.86	47.89	142
	SUMMIT	Ravenna silt loam, 0 to 2 percent slopes	ReA	47.89	48.00	603
	SUMMIT	Canfield silt loam, 2 to 6 percent slopes	CdB	48.00	48.09	452
	XSUMMIT	Canfield silt loam, 2 to 6 percent slopes	CdB	48.09	48.10	66
	SUMMIT	Wooster silt loam, 12 to 18 percent, moderately eroded	WuD2	44.99	45.03	199
	SUMMIT	Wooster silt loam, 6 to 12 percent slopes, moderately eroded	WuC2	45.03	45.27	1281
	SUMMIT	Wooster silt loam, 2 to 6 percent slopes	WuB	45.27	45.34	364
	SUMMIT	Canfield silt loam, 2 to 6 percent slopes	CdB	45.34	45.38	212
	SUMMIT	Wooster silt loam, 2 to 6 percent slopes	WuB	45.38	45.43	273
	SUMMIT	Canfield silt loam, 2 to 6 percent slopes	CdB	45.43	45.47	220
	SUMMIT	Wooster silt loam, 2 to 6 percent slopes	WuB	45.47	45.56	464
	SUMMIT	Canfield silt loam, 2 to 6 percent slopes	CdB	45.56	45.58	114
	SUMMIT	Wooster silt loam, 2 to 6 percent slopes	WuB	45.58	45.67	484
	SUMMIT	Loudonville silt loam, 12 to 18 percent slopes	LoD	45.67	45.73	316

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	SUMMIT	Dekalb sandy loam, 25 to 70 percent slopes	DkF	45.73	45.77	199
	SUMMIT	Oshtemo sandy loam, 2 to 6 percent slopes	OsB	45.77	45.78	72
	SUMMIT	Wheeling silt loam, 2 to 6 percent slopes	WrB	45.78	45.85	365
	SUMMIT	Chili loam, 2 to 6 percent slopes	CnB	45.85	45.95	526
	SUMMIT	Holly silt loam, alkaline	Hy	45.95	45.99	194
	SUMMIT	Chagrin silt loam, alkaline	Ck	45.99	46.00	76
	SUMMIT	Water	W	46.00	46.02	96
	SUMMIT	Udorthents, sanitary landfill	Uf	46.02	46.05	131
	SUMMIT	Loudonville silt loam, 2 to 6 percent slopes	LoB	46.05	46.07	140
	SUMMIT	Wooster silt loam, 12 to 18 percent, moderately eroded	WuD2	46.07	46.14	334
	SUMMIT	Wooster silt loam, 6 to 12 percent slopes, moderately eroded	WuC2	46.14	46.17	196
	SUMMIT	Wooster silt loam, 2 to 6 percent slopes	WuB	46.17	46.27	518
	SUMMIT	Canfield silt loam, 2 to 6 percent slopes	CdB	46.27	46.43	823
	SUMMIT	Wooster silt loam, 2 to 6 percent slopes	WuB	46.43	46.54	616
	SUMMIT	Wooster silt loam, 6 to 12 percent slopes, moderately eroded	WuC2	46.54	46.72	940
	SUMMIT	Canfield silt loam, 2 to 6 percent slopes	CdB	46.72	46.74	121
	SUMMIT	Holly silt loam	Ho	46.74	46.80	282
	SUMMIT	Chili silt loam, 2 to 6 percent slopes	CpB	46.80	46.84	242
	SUMMIT	Sebring silt loam	Sb	46.84	46.87	145
	SUMMIT	Wheeling silt loam, 2 to 6 percent slopes	WrB	46.87	46.89	78
	SUMMIT	Sebring silt loam	Sb	46.89	46.91	123
	SUMMIT	Chili loam, 2 to 6 percent slopes	CnB	46.91	46.95	235
	SUMMIT	Bogart loam, 0 to 2 percent slopes	BgA	46.95	46.99	218

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	SUMMIT	Sebring silt loam	Sb	46.99	47.05	284
	SUMMIT	Chili silt loam, 2 to 6 percent slopes	CpB	47.05	47.09	217
	SUMMIT	Sebring silt loam	Sb	47.09	47.18	455
	SUMMIT	Ravenna silt loam, 2 to 6 percent slopes	ReB	47.18	47.29	592
	SUMMIT	Canfield silt loam, 6 to 12 percent slopes, moderately eroded	CdC2	47.29	47.33	200
	SUMMIT	Canfield silt loam, 2 to 6 percent slopes	CdB	47.33	47.46	721
	SUMMIT	Canfield silt loam, 6 to 12 percent slopes, moderately eroded	CdC2	47.46	47.57	564
	SUMMIT	Fitchville silt loam, 0 to 2 percent slopes	FcA	47.57	47.72	816
	SUMMIT	Canfield silt loam, 2 to 6 percent slopes	CdB	47.72	47.79	348
	SUMMIT	Ravenna silt loam, 2 to 6 percent slopes	ReB	47.79	47.81	105
	SUMMIT	Canfield silt loam, sandstone substratum, 2 to 6 percent slopes	CeB	47.81	47.86	271
	SUMMIT	Canfield silt loam, 2 to 6 percent slopes	CdB	47.86	47.89	142
	SUMMIT	Ravenna silt loam, 0 to 2 percent slopes	ReA	47.89	48.00	603
	SUMMIT	Canfield silt loam, 2 to 6 percent slopes	CdB	48.00	48.09	452
	SUMMIT	Canfield silt loam, 2 to 6 percent slopes	CdB	48.09	48.10	66
	WAYNE	Canfield silt loam, 2 to 6 percent slopes	CdB	48.10	48.11	49
	WAYNE	Ravenna silt loam, 0 to 2 percent slopes	ReA	48.11	48.12	65
	WAYNE	Canfield silt loam, 6 to 12 percent slopes	CdC	48.12	48.18	288
	WAYNE	Canfield silt loam, 2 to 6 percent slopes	CdB	48.18	48.39	1113
	WAYNE	Canfield silt loam, 6 to 12 percent slopes	CdC	48.39	48.43	252

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	WAYNE	Canfield silt loam, 2 to 6 percent slopes	CdB	48.43	48.78	1846
	WAYNE	Ravenna silt loam, 0 to 2 percent slopes	ReA	48.78	48.82	165
	WAYNE	Canfield silt loam, 2 to 6 percent slopes	CdB	48.82	48.90	452
	WAYNE	Canfield silt loam, 6 to 12 percent slopes	CdC	48.90	49.08	963
	WAYNE	Canfield silt loam, 2 to 6 percent slopes	CdB	49.08	49.19	583
	WAYNE	Ravenna silt loam, 0 to 2 percent slopes	ReA	49.19	49.25	319
	WAYNE	Canfield silt loam, 2 to 6 percent slopes	CdB	49.25	49.30	242
	WAYNE	Ravenna silt loam, 0 to 2 percent slopes	ReA	49.30	49.53	1197
	WAYNE	Canfield silt loam, 2 to 6 percent slopes, eroded	CdB2	49.53	49.65	634
	WAYNE	Canfield silt loam, 6 to 12 percent slopes, eroded	CdC2	49.65	49.67	142
	WAYNE	Canfield silt loam, 2 to 6 percent slopes, eroded	CdB2	49.67	49.74	370
	WAYNE	Canfield silt loam, 2 to 6 percent slopes	CdB	49.74	49.88	721
	WAYNE	Canfield silt loam, 6 to 12 percent slopes	CdC	49.88	49.94	327
	WAYNE	Canfield silt loam, 2 to 6 percent slopes	CdB	49.94	50.10	837
	WAYNE	Glenford silt loam, 2 to 6 percent slopes	GfB	50.10	50.13	141
	WAYNE	Canfield silt loam, 2 to 6 percent slopes	CdB	50.13	50.16	181
	WAYNE	Canfield silt loam, 6 to 12 percent slopes, eroded	CdC2	50.16	50.20	195
	WAYNE	Glenford silt loam, 2 to 6 percent slopes	GfB	50.20	50.23	155
	WAYNE	Orrville silt loam, occasionally flooded	Or	50.23	50.34	610
	WAYNE	Glenford silt loam, 2 to 6 percent slopes	GfB	50.34	50.45	574

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	WAYNE	Glenford silt loam, 6 to 12 percent slopes	GfC	50.45	50.58	695
	WAYNE	Canfield silt loam, 2 to 6 percent slopes	CdB	50.58	50.64	321
	WAYNE	Canfield silt loam, 6 to 12 percent slopes	CdC	50.64	50.73	462
	WAYNE	Wooster-Riddles silt loams, 6 to 12 percent slopes, eroded	WuC2	50.73	50.88	795
	WAYNE	Glenford silt loam, 2 to 6 percent slopes	GfB	50.88	50.93	240
	WAYNE	Wooster-Riddles silt loams, 6 to 12 percent slopes, eroded	WuC2	50.93	50.98	287
	WAYNE	Glenford silt loam, 2 to 6 percent slopes	GfB	50.98	51.08	502
	WAYNE	Ravenna silt loam, 0 to 2 percent slopes	ReA	51.08	51.17	511
	WAYNE	Canfield silt loam, 2 to 6 percent slopes	CdB	51.17	51.42	1302
	WAYNE	Canfield silt loam, 6 to 12 percent slopes	CdC	51.42	51.54	650
	WAYNE	Wooster-Riddles silt loams, 12 to 18 percent slopes, eroded	WuD2	51.54	51.59	266
	WAYNE	Ravenna silt loam, 0 to 2 percent slopes	ReA	51.59	51.60	42
	WAYNE	Wooster-Riddles silt loams, 12 to 18 percent slopes, eroded	WuD2	51.60	51.77	862
	WAYNE	Wooster-Riddles silt loams, 6 to 12 percent slopes, eroded	WuC2	51.77	51.86	483
	WAYNE	Ravenna silt loam, 2 to 6 percent slopes	ReB	51.86	51.90	227
	WAYNE	Wooster-Riddles silt loams, 6 to 12 percent slopes, eroded	WuC2	51.90	51.96	300
	WAYNE	Ravenna silt loam, 2 to 6 percent slopes	ReB	51.96	52.00	244
	WAYNE	Wooster-Riddles silt loams, 6 to 12 percent slopes, eroded	WuC2	52.00	52.04	199
	WAYNE	Ravenna silt loam, 2 to 6 percent slopes	ReB	52.04	52.07	147
	WAYNE	Wooster-Riddles silt loams, 6 to 12 percent slopes, eroded	WuC2	52.07	52.10	175

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	WAYNE	Ravenna silt loam, 0 to 2 percent slopes	ReA	52.10	52.12	108
	WAYNE	Canfield silt loam, 2 to 6 percent slopes	CdB	52.12	52.15	171
	WAYNE	Ravenna silt loam, 2 to 6 percent slopes	ReB	52.15	52.22	325
	WAYNE	Canfield silt loam, 2 to 6 percent slopes	CdB	52.22	52.26	233
	WAYNE	Ravenna silt loam, 2 to 6 percent slopes	ReB	52.26	52.30	226
	WAYNE	Canfield silt loam, 2 to 6 percent slopes	CdB	52.30	52.36	282
	WAYNE	Canfield silt loam, 6 to 12 percent slopes, eroded	CdC2	52.36	52.44	443
	WAYNE	Canfield silt loam, 2 to 6 percent slopes	CdB	52.44	52.55	585
	WAYNE	Glenford silt loam, 2 to 6 percent slopes	GfB	52.55	52.59	198
	WAYNE	Glenford silt loam, 6 to 12 percent slopes, eroded	GfC2	52.59	52.59	24
	WAYNE	Orrville silt loam, occasionally flooded	Or	52.59	52.63	178
	WAYNE	Glenford silt loam, 2 to 6 percent slopes	GfB	52.63	52.76	717
	WAYNE	Bogart loam, 2 to 6 percent slopes	BtB	52.76	52.87	548
	WAYNE	Glenford silt loam, 2 to 6 percent slopes	GfB	52.87	52.98	589
	WAYNE	Orrville silt loam, occasionally flooded	Or	52.98	53.06	412
	WAYNE	Glenford silt loam, 2 to 6 percent slopes	GfB	53.06	53.20	734
	WAYNE	Canfield silt loam, 6 to 12 percent slopes, eroded	CdC2	53.20	53.37	937
	WAYNE	Canfield silt loam, 2 to 6 percent slopes	CdB	53.37	53.56	985
	WAYNE	Ravenna silt loam, 0 to 2 percent slopes	ReA	53.56	53.60	205
	WAYNE	Canfield silt loam, 2 to 6 percent slopes	CdB	53.60	53.63	173

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	WAYNE	Ravenna silt loam, 2 to 6 percent slopes	ReB	53.63	53.65	103
	WAYNE	Ravenna silt loam, 0 to 2 percent slopes	ReA	53.65	53.68	173
	WAYNE	Ravenna silt loam, 2 to 6 percent slopes	ReB	53.68	53.78	485
	WAYNE	Ravenna silt loam, 0 to 2 percent slopes	ReA	53.78	53.94	892
	WAYNE	Canfield silt loam, 2 to 6 percent slopes	CdB	53.94	53.99	224
	WAYNE	Canfield silt loam, 6 to 12 percent slopes	CdC	53.99	54.07	415
	WAYNE	Wooster-Riddles silt loams, 6 to 12 percent slopes, eroded	WuC2	54.07	54.10	185
	WAYNE	Canfield silt loam, 6 to 12 percent slopes	CdC	54.10	54.16	321
	WAYNE	Wooster-Riddles silt loams, 6 to 12 percent slopes, eroded	WuC2	54.16	54.22	320
	MEDINA	Wooster-Riddles silt loams, 6 to 12 percent slopes, eroded	WuC2	54.22	54.23	40
	MEDINA	Wooster-Riddles silt loams, 6 to 12 percent slopes, eroded	WvC2	54.23	54.30	401
	MEDINA	Canfield silt loam, 2 to 6 percent slopes	CdB	54.30	54.39	436
	MEDINA	Ravenna silt loam, 2 to 6 percent slopes	ReB	54.39	54.41	140
	MEDINA	Wooster-Riddles silt loams, 2 to 6 percent slopes	WvB	54.41	54.48	350
	MEDINA	Wooster silt loam, 6 to 12 percent slopes, moderately eroded	WuC2	54.48	54.53	275
	MEDINA	Wooster-Riddles silt loams, 2 to 6 percent slopes	WvB	54.53	54.57	226
	MEDINA	Bogart loam, 2 to 6 percent slopes	BtB	54.57	54.68	553
	MEDINA	Chili loam, 2 to 6 percent slopes	CnB	54.68	54.72	201
	MEDINA	Jimtown loam, 0 to 2 percent slopes	JtA	54.72	54.84	661
	MEDINA	Olmsted loam	Od	54.84	54.89	264
	MEDINA	Bogart loam, 2 to 6 percent slopes	BtB	54.89	54.98	462

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	MEDINA	Euclid silt loam, occasionally flooded	EvA	54.98	55.19	1124
	MEDINA	Luray silt loam	Ly	55.19	55.28	484
	MEDINA	Jimtown loam, 0 to 2 percent slopes	JtA	55.28	55.41	670
	MEDINA	Luray silt loam	Ly	55.41	55.48	344
	MEDINA	Fitchville silt loam, 2 to 6 percent slopes	FcB	55.48	55.56	454
	MEDINA	Chili gravelly loam, 12 to 25 percent slopes, moderately eroded	CoE2	55.56	55.60	172
	MEDINA	Wooster silt loam, 2 to 6 percent slopes	WuB	55.60	55.69	508
	MEDINA	Chili gravelly loam, 6 to 12 percent slopes, moderately eroded	CoC2	55.69	55.74	237
	MEDINA	Oshtemo sandy loam, 2 to 6 percent slopes	OtB	55.74	55.78	253
	MEDINA	Fitchville silt loam, 2 to 6 percent slopes	FcB	55.78	55.83	258
	MEDINA	Luray silt loam	Ly	55.83	55.94	579
	MEDINA	Chili gravelly loam, 6 to 12 percent slopes, moderately eroded	CoC2	55.94	55.97	140
	MEDINA	Glenford silt loam, 2 to 6 percent slopes	GfB	55.97	56.11	743
	MEDINA	Wooster silt loam, 12 to 25 percent slopes, moderately eroded	WuE2	56.11	56.24	690
	MEDINA	Rittman silt loam, 25 to 70 percent slopes	RsF	56.24	56.29	255
	MEDINA	Rittman silt loam, 6 to 12 percent slopes, moderately eroded	RsC2	56.29	56.46	895
	MEDINA	Rittman silt loam, 2 to 6 percent slopes	RsB	56.46	56.80	1803
	MEDINA	Rittman silt loam, 6 to 12 percent slopes, moderately eroded	RsC2	56.80	56.83	176
	MEDINA	Rittman silt loam, 2 to 6 percent slopes	RsB	56.83	56.84	28

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	MEDINA	Rittman silt loam, 25 to 70 percent slopes	RsF	56.84	56.86	113
	MEDINA	Lobdell silt loam	Le	56.86	56.90	209
	MEDINA	Rittman silt loam, 6 to 12 percent slopes, moderately eroded	RsC2	56.90	57.05	775
	MEDINA	Rittman silt loam, 2 to 6 percent slopes	RsB	57.05	57.23	942
	MEDINA	Wadsworth silt loam, 0 to 2 percent slopes	WaA	57.23	57.35	672
	MEDINA	Rittman silt loam, 2 to 6 percent slopes	RsB	57.35	57.52	907
	MEDINA	Wadsworth silt loam, 2 to 6 percent slopes	WaB	57.52	57.59	340
	MEDINA	Rittman silt loam, 6 to 12 percent slopes, moderately eroded	RsC2	57.59	57.70	586
	MEDINA	Rittman silt loam, 25 to 70 percent slopes	RsF	57.70	57.71	76
	MEDINA	Lobdell silt loam	Le	57.71	57.77	308
	MEDINA	Rittman silt loam, 2 to 6 percent slopes	RsB	57.77	57.83	306
	MEDINA	Rittman silt loam, 6 to 12 percent slopes, moderately eroded	RsC2	57.83	57.85	126
	MEDINA	Lobdell silt loam	Le	57.85	57.91	310
	MEDINA	Rittman silt loam, 6 to 12 percent slopes, moderately eroded	RsC2	57.91	57.98	345
	MEDINA	Rittman silt loam, 2 to 6 percent slopes	RsB	57.98	58.14	856
	MEDINA	Wadsworth silt loam, 2 to 6 percent slopes	WaB	58.14	58.21	380
	MEDINA	Wadsworth silt loam, 0 to 2 percent slopes	WaA	58.21	58.26	254
	MEDINA	Miner silty clay loam	Mr	58.26	58.33	383
	MEDINA	Wadsworth silt loam, 0 to 2 percent slopes	WaA	58.33	58.57	1256
	MEDINA	Wadsworth silt loam, 2 to 6 percent slopes	WaB	58.57	58.69	626

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	MEDINA	Wadsworth silt loam, 0 to 2 percent slopes	WaA	58.69	58.86	898
	MEDINA	Wadsworth silt loam, 2 to 6 percent slopes	WaB	58.86	59.48	3279
	MEDINA	Sebring silt loam, till substratum	St	59.48	59.57	472
	MEDINA	Wadsworth silt loam, 2 to 6 percent slopes	WaB	59.57	59.63	303
	MEDINA	Sebring silt loam, till substratum	St	59.63	59.73	557
	MEDINA	Wadsworth silt loam, 0 to 2 percent slopes	WaA	59.73	59.76	152
	MEDINA	Rittman silt loam, 2 to 6 percent slopes	RsB	59.76	59.85	478
	MEDINA	Wadsworth silt loam, 0 to 2 percent slopes	WaA	59.85	59.93	416
	MEDINA	Rittman silt loam, 2 to 6 percent slopes	RsB	59.93	60.02	455
	MEDINA	Rittman silt loam, 6 to 12 percent slopes, moderately eroded	RsC2	60.02	60.04	127
	MEDINA	Wadsworth silt loam, 0 to 2 percent slopes	WaA	60.04	60.09	269
	MEDINA	Rittman silt loam, 2 to 6 percent slopes	RsB	60.09	60.13	181
	MEDINA	Wadsworth silt loam, 0 to 2 percent slopes	WaA	60.13	60.15	149
	MEDINA	Udorthents, loamy	Ud	60.15	60.27	635
	MEDINA	Rittman silt loam, 2 to 6 percent slopes	RsB	60.27	60.52	1274
	MEDINA	Wadsworth silt loam, 2 to 6 percent slopes	WaB	60.52	60.55	172
	MEDINA	Rittman silt loam, 2 to 6 percent slopes, moderately eroded	RsB2	60.55	60.60	275
	MEDINA	Wadsworth silt loam, 2 to 6 percent slopes	WaB	60.60	60.61	31
	MEDINA	Rittman silt loam, 2 to 6 percent slopes, moderately eroded	RsB2	60.61	60.65	221
	MEDINA	Wadsworth silt loam, 2 to 6 percent slopes	WaB	60.65	60.72	363
	MEDINA	Rittman silt loam, 2 to 6 percent slopes, moderately eroded	RsB2	60.72	60.74	133

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	MEDINA	Wadsworth silt loam, 0 to 2 percent slopes	WaA	60.74	60.80	328
	MEDINA	Wadsworth silt loam, 2 to 6 percent slopes	WaB	60.80	60.89	444
	MEDINA	Chili loam, 6 to 12 percent slopes	CnC	60.89	60.93	223
	MEDINA	Wadsworth silt loam, 0 to 2 percent slopes	WaA	60.93	61.12	985
	MEDINA	Rittman silt loam, 2 to 6 percent slopes, moderately eroded	RsB2	61.12	61.17	267
	MEDINA	Wadsworth silt loam, 0 to 2 percent slopes	WaA	61.17	61.44	1442
	MEDINA	Wadsworth silt loam, 2 to 6 percent slopes	WaB	61.44	61.52	415
	MEDINA	Rittman silt loam, 6 to 12 percent slopes, moderately eroded	RsC2	61.52	61.59	393
	MEDINA	Wadsworth silt loam, 2 to 6 percent slopes	WaB	61.59	61.66	362
	MEDINA	Rittman silt loam, 6 to 12 percent slopes, moderately eroded	RsC2	61.66	61.69	122
	MEDINA	Wadsworth silt loam, 2 to 6 percent slopes	WaB	61.69	61.73	214
	MEDINA	Rittman silt loam, 6 to 12 percent slopes, moderately eroded	RsC2	61.73	61.78	273
	MEDINA	Wadsworth silt loam, 0 to 2 percent slopes	WaA	61.78	62.12	1782
	MEDINA	Wadsworth silt loam, 2 to 6 percent slopes	WaB	62.12	62.17	290
	MEDINA	Rittman silt loam, 12 to 25 percent slopes, moderately eroded	RsE2	62.17	62.23	328
	MEDINA	Orrville silt loam	Or	62.23	62.30	332
	MEDINA	Rittman silt loam, 25 to 70 percent slopes	RsF	62.30	62.34	229
	MEDINA	Wadsworth silt loam, 2 to 6 percent slopes	WaB	62.34	62.52	942
	MEDINA	Rittman silt loam, 6 to 12 percent slopes, moderately eroded	RsC2	62.52	62.55	152

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	MEDINA	Wadsworth silt loam, 2 to 6 percent slopes	WaB	62.55	62.58	196
	MEDINA	Rittman silt loam, 6 to 12 percent slopes, moderately eroded	RsC2	62.58	62.61	151
	MEDINA	Rittman silt loam, 2 to 6 percent slopes	RsB	62.61	62.77	853
	MEDINA	Wadsworth silt loam, 2 to 6 percent slopes	WaB	62.77	62.82	242
	MEDINA	Rittman silt loam, 2 to 6 percent slopes	RsB	62.82	62.89	361
	MEDINA	Udorthents, loamy	Ud	62.89	63.01	630
	MEDINA	Rittman silt loam, 2 to 6 percent slopes	RsB	63.01	63.02	65
	MEDINA	Rittman silt loam, 6 to 12 percent slopes, moderately eroded	RsC2	63.02	63.04	135
	MEDINA	Rittman silt loam, 2 to 6 percent slopes	RsB	63.04	63.09	248
	MEDINA	Rittman silt loam, 6 to 12 percent slopes, moderately eroded	RsC2	63.09	63.15	299
	MEDINA	Orrville silt loam	Or	63.15	63.18	177
	MEDINA	Rittman silt loam, 12 to 25 percent slopes, moderately eroded	RsE2	63.18	63.22	203
	MEDINA	Wadsworth silt loam, 2 to 6 percent slopes	WaB	63.22	63.33	566
	MEDINA	Rittman silt loam, 6 to 12 percent slopes, moderately eroded	RsC2	63.33	63.37	229
	MEDINA	Wadsworth silt loam, 2 to 6 percent slopes	WaB	63.37	63.50	680
	MEDINA	Rittman silt loam, 6 to 12 percent slopes, moderately eroded	RsC2	63.50	63.54	189
	MEDINA	Miner silty clay loam	Mr	63.54	63.56	147
	MEDINA	Wadsworth silt loam, 0 to 2 percent slopes	WaA	63.56	63.59	160
	MEDINA	Rittman silt loam, 2 to 6 percent slopes	RsB	63.59	63.67	424

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	MEDINA	Rittman silt loam, 2 to 6 percent slopes, moderately eroded	RsB2	63.67	63.75	378
	MEDINA	Wadsworth silt loam, 2 to 6 percent slopes	WaB	63.75	63.82	381
	MEDINA	Rittman silt loam, 2 to 6 percent slopes, moderately eroded	RsB2	63.82	64.02	1086
	MEDINA	Rittman silt loam, 6 to 12 percent slopes, moderately eroded	RsC2	64.02	64.09	354
	MEDINA	Rittman silt loam, 12 to 25 percent slopes, moderately eroded	RsE2	64.09	64.16	380
	MEDINA	Rittman silt loam, 6 to 12 percent slopes, moderately eroded	RsC2	64.16	64.23	345
	MEDINA	Rittman silt loam, 2 to 6 percent slopes	RsB	64.23	64.27	242
	MEDINA	Rittman silt loam, 6 to 12 percent slopes, moderately eroded	RsC2	64.27	64.37	511
	MEDINA	Rittman silt loam, 12 to 25 percent slopes, moderately eroded	RsE2	64.37	64.42	249
	MEDINA	Rittman silt loam, 2 to 6 percent slopes, moderately eroded	RsB2	64.42	64.51	510
	MEDINA	Rittman silt loam, 12 to 25 percent slopes, moderately eroded	RsE2	64.51	64.59	380
	MEDINA	Rittman silt loam, 6 to 12 percent slopes, moderately eroded	RsC2	64.59	64.65	365
	MEDINA	Rittman silt loam, 2 to 6 percent slopes	RsB	64.65	64.80	762
	MEDINA	Rittman silt loam, 6 to 12 percent slopes, moderately eroded	RsC2	64.80	64.89	467
	MEDINA	Rittman silt loam, 2 to 6 percent slopes	RsB	64.89	65.01	636
	MEDINA	Rittman silt loam, 6 to 12 percent slopes, moderately eroded	RsC2	65.01	65.07	351
	MEDINA	Lobdell silt loam	Le	65.07	65.12	254

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	MEDINA	Bogart loam, 2 to 6 percent slopes	BtB	65.12	65.14	98
	MEDINA	Rittman silt loam, 12 to 25 percent slopes, moderately eroded	RsE2	65.14	65.20	332
	MEDINA	Rittman silt loam, 2 to 6 percent slopes, moderately eroded	RsB2	65.20	65.25	226
	MEDINA	Rittman silt loam, 6 to 12 percent slopes, moderately eroded	RsC2	65.25	65.35	552
	MEDINA	Rittman silt loam, 2 to 6 percent slopes, moderately eroded	RsB2	65.35	65.43	402
	MEDINA	Wadsworth silt loam, 2 to 6 percent slopes	WaB	65.43	65.45	96
	MEDINA	Rittman silt loam, 2 to 6 percent slopes, moderately eroded	RsB2	65.45	65.46	49
	MEDINA	Wadsworth silt loam, 2 to 6 percent slopes	WaB	65.46	65.49	179
	MEDINA	Wadsworth silt loam, 0 to 2 percent slopes	WaA	65.49	65.59	548
	MEDINA	Rittman silt loam, 2 to 6 percent slopes	RsB	65.59	65.68	466
	MEDINA	Lobdell silt loam	Le	65.68	65.80	641
	MEDINA	Rittman silt loam, 2 to 6 percent slopes, moderately eroded	RsB2	65.80	65.83	168
	MEDINA	Udorthents, loamy	Ud	65.83	65.87	207
	MEDINA	Rittman silt loam, 2 to 6 percent slopes, moderately eroded	RsB2	65.87	65.88	26
	MEDINA	Bennington silt loam, 2 to 6 percent slopes	BnB	65.88	65.95	390
	MEDINA	Rittman silt loam, 2 to 6 percent slopes, moderately eroded	RsB2	65.95	66.01	301
	MEDINA	Bennington silt loam, 2 to 6 percent slopes	BnB	66.01	66.16	789
	MEDINA	Bennington silt loam, 0 to 2 percent slopes	BnA	66.16	66.27	571
	MEDINA	Fitchville silt loam, 0 to 2 percent slopes	FcA	66.27	66.31	212
	MEDINA	Bennington silt loam, 2 to 6 percent slopes	BnB	66.31	66.36	256

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	MEDINA	Bennington silt loam, 0 to 2 percent slopes	BnA	66.36	66.38	132
	MEDINA	Bennington silt loam, 2 to 6 percent slopes	BnB	66.38	66.40	105
	MEDINA	Bennington silt loam, 0 to 2 percent slopes	BnA	66.40	66.44	236
	MEDINA	Bennington silt loam, 2 to 6 percent slopes	BnB	66.44	66.54	477
	MEDINA	Cardington silt loam, 12 to 25 percent slopes, moderately eroded	CgE2	66.54	66.56	137
	MEDINA	Cardington silt loam, 6 to 12 percent slopes, moderately eroded	CgC2	66.56	66.59	132
	MEDINA	Bennington silt loam, 2 to 6 percent slopes	BnB	66.59	66.61	122
	MEDINA	Cardington silt loam, 6 to 12 percent slopes, moderately eroded	CgC2	66.61	66.63	119
	MEDINA	Cardington silt loam, 12 to 25 percent slopes, moderately eroded	CgE2	66.63	66.67	184
	MEDINA	Orrville silt loam	Or	66.67	66.67	18
	MEDINA	Rittman silt loam, 25 to 70 percent slopes	RsF	66.67	66.68	49
	MEDINA	Chili loam, 2 to 6 percent slopes	CnB	66.68	66.71	171
	MEDINA	Fitchville silt loam, 0 to 2 percent slopes	FcA	66.71	66.73	87
	MEDINA	Chili loam, 2 to 6 percent slopes	CnB	66.73	66.75	128
	MEDINA	Fitchville silt loam, 0 to 2 percent slopes	FcA	66.75	66.80	277
	MEDINA	Holly silt loam	Hy	66.80	66.87	348
	MEDINA	Chili silt loam, 6 to 12 percent slopes	CpC	66.87	66.90	164
	MEDINA	Holly silt loam	Hy	66.90	66.99	443
	MEDINA	Cardington silt loam, 6 to 12 percent slopes, moderately eroded	CgC2	66.99	67.01	150
	MEDINA	Cardington silt loam, 2 to 6 percent slopes	CgB	67.01	67.06	220

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	MEDINA	Bennington silt loam, 2 to 6 percent slopes	BnB	67.06	67.09	197
	MEDINA	Cardington silt loam, 2 to 6 percent slopes	CgB	67.09	67.14	271
	MEDINA	Chili silt loam, 6 to 12 percent slopes	CpC	67.14	67.20	283
	MEDINA	Chili silt loam, 2 to 6 percent slopes	CpB	67.20	67.31	593
	MEDINA	Chili silt loam, 6 to 12 percent slopes	CpC	67.31	67.35	224
	MEDINA	Fitchville silt loam, 0 to 2 percent slopes	FcA	67.35	67.39	175
	MEDINA	Canadice silty clay loam	Ca	67.39	67.42	190
	MEDINA	Fitchville silt loam, 0 to 2 percent slopes	FcA	67.42	67.46	176
	MEDINA	Canadice silty clay loam	Ca	67.46	67.49	173
	MEDINA	Glenford silt loam, 2 to 6 percent slopes	GfB	67.49	67.54	298
	MEDINA	Wallkill silt loam	Wc	67.54	67.62	397
	MEDINA	Oshtemo sandy loam, 2 to 6 percent slopes	OtB	67.62	67.66	205
	MEDINA	Wallkill silt loam	Wc	67.66	67.75	497
	MEDINA	Holly silt loam	Hy	67.75	67.93	945
	MEDINA	Canadice silty clay loam	Ca	67.93	67.94	23
	MEDINA	Sebring silt loam, till substratum	St	67.94	68.01	401
	MEDINA	Fitchville silt loam, 0 to 2 percent slopes	FcA	68.01	68.08	376
	MEDINA	Caneadea silt loam, 0 to 2 percent slopes	CcA	68.08	68.09	33
	MEDINA	Canadice silty clay loam	Ca	68.09	68.12	180
	MEDINA	Caneadea silt loam, 0 to 2 percent slopes	CcA	68.12	68.25	649
	MEDINA	Canadice silty clay loam	Ca	68.25	68.37	627
	MEDINA	Sebring silt loam	Sg	68.37	68.52	841
	MEDINA	Chili gravelly loam, 6 to 12 percent slopes, moderately eroded	CoC2	68.52	68.56	163
	MEDINA	Sebring silt loam	Sg	68.56	68.60	257

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	MEDINA	Chili loam, 2 to 6 percent slopes	CnB	68.60	68.64	162
	MEDINA	Cardington silt loam, 6 to 12 percent slopes, moderately eroded	CgC2	68.64	68.75	586
	MEDINA	Bennington silt loam, 2 to 6 percent slopes	BnB	68.75	68.82	395
	MEDINA	Cardington silt loam, 6 to 12 percent slopes, moderately eroded	CgC2	68.82	68.91	492
	MEDINA	Cardington silt loam, 2 to 6 percent slopes	CgB	68.91	68.97	309
	MEDINA	Cardington silt loam, 6 to 12 percent slopes, moderately eroded	CgC2	68.97	69.00	141
	MEDINA	Bennington silt loam, 2 to 6 percent slopes	BnB	69.00	69.08	437
	MEDINA	Jimtown loam, 0 to 2 percent slopes	JtA	69.08	69.09	56
	MEDINA	Bennington silt loam, 2 to 6 percent slopes	BnB	69.09	69.13	179
	MEDINA	Cardington silt loam, 2 to 6 percent slopes	CgB	69.13	69.14	96
	MEDINA	Bennington silt loam, 0 to 2 percent slopes	BnA	69.14	69.18	213
	MEDINA	Miner silty clay loam	Mr	69.18	69.33	758
	MEDINA	Bennington silt loam, 0 to 2 percent slopes	BnA	69.33	69.42	476
	MEDINA	Bennington silt loam, 2 to 6 percent slopes	BnB	69.42	69.44	123
	MEDINA	Bennington silt loam, 0 to 2 percent slopes	BnA	69.44	69.47	144
	MEDINA	Bennington silt loam, 2 to 6 percent slopes	BnB	69.47	69.53	336
	MEDINA	Jimtown loam, 0 to 2 percent slopes	JtA	69.53	69.62	444
	MEDINA	Bennington silt loam, 2 to 6 percent slopes	BnB	69.62	69.76	735
	MEDINA	Bogart loam, 2 to 6 percent slopes	BtB	69.76	69.86	533
	MEDINA	Orrville silt loam	Or	69.86	69.99	720

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	MEDINA	Ellsworth silt loam, 25 to 70 percent slopes	ElF	69.99	70.04	231
	MEDINA	Ellsworth silt loam, 2 to 6 percent slopes	ElB	70.04	70.06	95
	MEDINA	Ellsworth silt loam, 25 to 70 percent slopes	ElF	70.06	70.13	414
	MEDINA	Orrville silt loam	Or	70.13	70.38	1280
	MEDINA	Ellsworth silt loam, 12 to 25 percent slopes, moderately eroded	ElE2	70.38	70.53	831
	MEDINA	Ellsworth silt loam, 2 to 6 percent slopes, moderately eroded	ElB2	70.53	70.56	116
	MEDINA	Ellsworth silt loam, 12 to 25 percent slopes, moderately eroded	ElE2	70.56	70.59	183
	MEDINA	Lobdell silt loam	Le	70.59	70.59	21
	MEDINA	Ellsworth silt loam, 12 to 25 percent slopes, moderately eroded	ElE2	70.59	70.60	38
	MEDINA	Ellsworth silt loam, 2 to 6 percent slopes, moderately eroded	ElB2	70.60	70.61	65
	MEDINA	Lobdell silt loam	Le	70.61	70.62	40
	MEDINA	Orrville silt loam	Or	70.62	70.66	185
	MEDINA	Ellsworth silt loam, 12 to 25 percent slopes, moderately eroded	ElE2	70.66	70.68	151
	MEDINA	Ellsworth silt loam, 2 to 6 percent slopes, moderately eroded	ElB2	70.68	70.80	620
	MEDINA	Ellsworth silt loam, 6 to 12 percent slopes, moderately eroded	ElC2	70.80	70.83	173
	MEDINA	Ellsworth silt loam, 2 to 6 percent slopes	ElB	70.83	70.88	257
	MEDINA	Ellsworth silt loam, 12 to 25 percent slopes, moderately eroded	ElE2	70.88	70.89	35
	MEDINA	Ellsworth silt loam, 6 to 12 percent slopes, moderately eroded	ElC2	70.89	70.91	88

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	MEDINA	Orrville silt loam	Or	70.91	70.96	276
	MEDINA	Chili silt loam, 2 to 6 percent slopes	CpB	70.96	70.99	169
	MEDINA	Ellsworth silt loam, 12 to 25 percent slopes, moderately eroded	ElE2	70.99	71.07	399
	MEDINA	Mahoning silt loam, 2 to 6 percent slopes	MgB	71.07	71.21	775
	MEDINA	Ellsworth silt loam, 6 to 12 percent slopes, moderately eroded	ElC2	71.21	71.26	248
	MEDINA	Mahoning silt loam, 2 to 6 percent slopes	MgB	71.26	71.30	233
	MEDINA	Ellsworth silt loam, 6 to 12 percent slopes, moderately eroded	ElC2	71.30	71.38	415
	MEDINA	Mahoning silt loam, 2 to 6 percent slopes	MgB	71.38	71.49	569
	MEDINA	Mahoning silt loam, 0 to 2 percent slopes	MgA	71.49	71.53	185
	MEDINA	Mahoning silt loam, 2 to 6 percent slopes	MgB	71.53	71.60	397
	MEDINA	Ellsworth silt loam, 2 to 6 percent slopes, moderately eroded	ElB2	71.60	71.71	582
	MEDINA	Mahoning silt loam, 2 to 6 percent slopes	MgB	71.71	71.74	159
	MEDINA	Ellsworth silt loam, 2 to 6 percent slopes, moderately eroded	ElB2	71.74	71.76	109
	MEDINA	Ellsworth silt loam, 12 to 25 percent slopes, moderately eroded	ElE2	71.76	71.79	143
	MEDINA	Ellsworth silt loam, 6 to 12 percent slopes, moderately eroded	ElC2	71.79	71.83	215
	MEDINA	Ellsworth silt loam, 12 to 25 percent slopes, moderately eroded	ElE2	71.83	71.88	288
	MEDINA	Ellsworth silt loam, 2 to 6 percent slopes, moderately eroded	ElB2	71.88	71.93	243

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	MEDINA	Ellsworth silt loam, 12 to 25 percent slopes, moderately eroded	ElE2	71.93	71.94	31
	MEDINA	Ellsworth silt loam, 2 to 6 percent slopes, moderately eroded	ElB2	71.94	72.05	576
	MEDINA	Mahoning silt loam, 2 to 6 percent slopes	MgB	72.05	72.09	252
	MEDINA	Ellsworth silt loam, 2 to 6 percent slopes, moderately eroded	ElB2	72.09	72.15	291
	MEDINA	Mahoning silt loam, 2 to 6 percent slopes	MgB	72.15	72.15	13
	MEDINA	Ellsworth silt loam, 6 to 12 percent slopes, moderately eroded	ElC2	72.15	72.18	137
	MEDINA	Ellsworth silt loam, 2 to 6 percent slopes, moderately eroded	ElB2	72.18	72.35	933
	MEDINA	Ellsworth silt loam, 12 to 25 percent slopes, moderately eroded	ElE2	72.35	72.42	340
	MEDINA	Ellsworth silt loam, 2 to 6 percent slopes	ElB	72.42	72.52	519
	MEDINA	Orrville silt loam	Or	72.52	72.57	265
	MEDINA	Ellsworth silt loam, 12 to 25 percent slopes, moderately eroded	ElE2	72.57	72.58	52
	MEDINA	Ellsworth silt loam, 2 to 6 percent slopes, moderately eroded	ElB2	72.58	72.59	82
	MEDINA	Ellsworth silt loam, 12 to 25 percent slopes, moderately eroded	ElE2	72.59	72.62	139
	MEDINA	Ellsworth silt loam, 6 to 12 percent slopes, moderately eroded	ElC2	72.62	72.63	60
	MEDINA	Ellsworth silt loam, 2 to 6 percent slopes, moderately eroded	ElB2	72.63	72.70	357
	MEDINA	Mahoning silt loam, 0 to 2 percent slopes	MgA	72.70	72.86	860
	MEDINA	Mahoning silt loam, 2 to 6 percent slopes	MgB	72.86	72.90	190

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	MEDINA	Mahoning silt loam, 0 to 2 percent slopes	MgA	72.90	72.92	113
	MEDINA	Mahoning silt loam, 2 to 6 percent slopes	MgB	72.92	72.95	192
	MEDINA	Mahoning silt loam, 0 to 2 percent slopes	MgA	72.95	73.02	370
	MEDINA	Mahoning silt loam, 2 to 6 percent slopes	MgB	73.02	73.05	145
	MEDINA	Mahoning silt loam, 0 to 2 percent slopes	MgA	73.05	73.18	669
	MEDINA	Mahoning silt loam, 2 to 6 percent slopes	MgB	73.18	73.21	151
	MEDINA	Mahoning silt loam, 0 to 2 percent slopes	MgA	73.21	73.27	330
	MEDINA	Mahoning silt loam, 2 to 6 percent slopes	MgB	73.27	73.41	729
	MEDINA	Mahoning silt loam, 0 to 2 percent slopes	MgA	73.41	73.46	260
	MEDINA	Mahoning silt loam, 2 to 6 percent slopes	MgB	73.46	73.81	1864
	MEDINA	Ellsworth silt loam, 12 to 25 percent slopes, moderately eroded	ElE2	73.81	73.84	152
	MEDINA	Lobdell silt loam	Le	73.84	73.86	119
	MEDINA	Ellsworth silt loam, 12 to 25 percent slopes, moderately eroded	ElE2	73.86	73.88	98
	MEDINA	Orrville silt loam	Or	73.88	73.95	371
	MEDINA	Ellsworth silt loam, 12 to 25 percent slopes, moderately eroded	ElE2	73.95	73.97	111
	MEDINA	Mahoning silt loam, 2 to 6 percent slopes	MgB	73.97	74.00	165
	MEDINA	Ellsworth silt loam, 12 to 25 percent slopes, moderately eroded	ElE2	74.00	74.12	602
	MEDINA	Mahoning silt loam, 2 to 6 percent slopes	MgB	74.12	74.35	1240
	MEDINA	Ellsworth silt loam, 12 to 25 percent slopes, moderately eroded	ElE2	74.35	74.42	366
	MEDINA	Orrville silt loam	Or	74.42	74.46	193

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	MEDINA	Ellsworth silt loam, 6 to 12 percent slopes, moderately eroded	EIC2	74.46	74.47	63
	MEDINA	Mahoning silt loam, 2 to 6 percent slopes	MgB	74.47	74.59	620
	MEDINA	Mahoning silt loam, 0 to 2 percent slopes	MgA	74.59	74.67	459
	MEDINA	Mahoning silt loam, 2 to 6 percent slopes	MgB	74.67	74.99	1662
	MEDINA	Mahoning silt loam, 0 to 2 percent slopes	MgA	74.99	75.01	118
	MEDINA	Mahoning silt loam, 2 to 6 percent slopes	MgB	75.01	75.14	702
	MEDINA	Mahoning silt loam, 0 to 2 percent slopes	MgA	75.14	75.43	1528
	MEDINA	Mahoning silt loam, 2 to 6 percent slopes	MgB	75.43	75.53	500
	MEDINA	Ellsworth silt loam, 2 to 6 percent slopes, moderately eroded	EIB2	75.53	75.60	412
	MEDINA	Orrville silt loam	Or	75.60	75.64	178
	MEDINA	Mahoning silt loam, 2 to 6 percent slopes	MgB	75.64	75.74	537
	MEDINA	Mahoning silt loam, 0 to 2 percent slopes	MgA	75.74	75.90	826
	MEDINA	Mahoning silt loam, 2 to 6 percent slopes	MgB	75.90	75.91	53
	MEDINA	Mahoning silt loam, 0 to 2 percent slopes	MgA	75.91	76.01	567
	MEDINA	Mahoning silt loam, 2 to 6 percent slopes	MgB	76.01	76.14	647
	MEDINA	Mahoning silt loam, 0 to 2 percent slopes	MgA	76.14	76.20	321
	MEDINA	Mahoning silt loam, 2 to 6 percent slopes	MgB	76.20	76.24	252
	MEDINA	Mahoning silt loam, 0 to 2 percent slopes	MgA	76.24	76.43	963
	MEDINA	Mahoning silt loam, 2 to 6 percent slopes	MgB	76.43	76.45	123
	MEDINA	Condit silt loam, 0 to 1 percent slopes	Cy	76.45	76.55	505

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	MEDINA	Mahoning silt loam, 0 to 2 percent slopes	MgA	76.55	76.75	1099
	MEDINA	Condit silt loam, 0 to 1 percent slopes	Cy	76.75	76.79	202
	MEDINA	Mahoning silt loam, 0 to 2 percent slopes	MgA	76.79	76.99	1048
	MEDINA	Mahoning silt loam, sandstone substratum, 0 to 2 percent slopes	MlA	76.99	77.00	72
	MEDINA	Mahoning silt loam, 2 to 6 percent slopes	MgB	77.00	77.20	1025
	LORAIN	Mahoning silt loam, 2 to 6 percent slopes	MgB	77.20	77.21	35
	LORAIN	Mahoning silt loam, 2 to 6 percent slopes	MgB	77.21	77.28	393
	LORAIN	Mahoning silt loam, 0 to 2 percent slopes	MgA	77.28	78.31	5422
	LORAIN	Trumbull silty clay loam, 0 to 2 percent slopes	TrA	78.31	78.39	439
	LORAIN	Mahoning silt loam, 0 to 2 percent slopes	MgA	78.39	78.57	971
	LORAIN	Mahoning silt loam, 2 to 6 percent slopes	MgB	78.57	78.75	907
	LORAIN	Mahoning silt loam, 0 to 2 percent slopes	MgA	78.75	79.04	1543
	LORAIN	Mahoning silt loam, 2 to 6 percent slopes	MgB	79.04	79.15	581
	LORAIN	Trumbull silty clay loam, 0 to 2 percent slopes	TrA	79.15	79.28	693
	LORAIN	Mahoning silt loam, 2 to 6 percent slopes	MgB	79.28	79.31	191
	LORAIN	Mahoning silt loam, 0 to 2 percent slopes	MgA	79.31	80.54	6443
	LORAIN	Mahoning silt loam, 2 to 6 percent slopes	MgB	80.54	80.66	673
	LORAIN	Ellsworth silt loam, 6 to 12 percent slopes, moderately eroded	ElC2	80.66	80.71	244
	LORAIN	Mahoning silt loam, 2 to 6 percent slopes	MgB	80.71	80.95	1263
	LORAIN	Orrville silt loam	Or	80.95	81.03	419

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	LORAIN	Mahoning silt loam, 2 to 6 percent slopes	MgB	81.03	81.18	830
	LORAIN	Mahoning silt loam, 0 to 2 percent slopes	MgA	81.18	81.52	1768
	LORAIN	Trumbull silty clay loam, 0 to 2 percent slopes	TrA	81.52	81.56	229
	LORAIN	Mahoning silt loam, 0 to 2 percent slopes	MgA	81.56	81.74	926
	LORAIN	Trumbull silty clay loam, 0 to 2 percent slopes	TrA	81.74	81.83	477
	LORAIN	Mahoning silt loam, 0 to 2 percent slopes	MgA	81.83	81.91	412
	LORAIN	Mahoning silt loam, 2 to 6 percent slopes	MgB	81.91	81.96	262
	LORAIN	Mahoning silt loam, 0 to 2 percent slopes	MgA	81.96	82.39	2281
	LORAIN	Mahoning silt loam, 2 to 6 percent slopes	MgB	82.39	82.52	685
	LORAIN	Ellsworth silt loam, 6 to 12 percent slopes, moderately eroded	ElC2	82.52	82.57	299
	LORAIN	Mahoning silt loam, 0 to 2 percent slopes	MgA	82.57	82.59	90
	LORAIN	Mahoning silt loam, 2 to 6 percent slopes	MgB	82.59	82.91	1690
	LORAIN	Bogart loam, 2 to 6 percent slopes	BtB	82.91	82.99	396
	LORAIN	Chili loam, 0 to 2 percent slopes	ClA	82.99	83.16	927
	LORAIN	Fitchville silt loam, low terrace, 0 to 2 percent slopes	FdA	83.16	83.20	214
	LORAIN	Tioga fine sandy loam	Tg	83.20	83.32	635
	LORAIN	Water	W	83.32	83.33	45
	LORAIN	Ellsworth silt loam, 12 to 18 percent slopes, moderately eroded	ElD2	83.33	83.36	168
	LORAIN	Mahoning silt loam, 0 to 2 percent slopes	MgA	83.36	83.43	340
	LORAIN	Water	W	83.43	83.45	143
	LORAIN	Mahoning silt loam, 0 to 2 percent slopes	MgA	83.45	83.90	2336

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	LORAIN	Trumbull silty clay loam, 0 to 2 percent slopes	TrA	83.90	83.94	202
	LORAIN	Rawson loam, 0 to 2 percent slopes	RdA	83.94	84.00	321
	LORAIN	Trumbull silty clay loam, 0 to 2 percent slopes	TrA	84.00	84.03	193
	LORAIN	Mahoning silt loam, 0 to 2 percent slopes	MgA	84.03	84.17	713
	LORAIN	Trumbull silty clay loam, 0 to 2 percent slopes	TrA	84.17	84.19	127
	LORAIN	Mahoning silt loam, 0 to 2 percent slopes	MgA	84.19	84.34	793
	LORAIN	Trumbull silty clay loam, 0 to 2 percent slopes	TrA	84.34	84.39	270
	LORAIN	Mahoning silt loam, 0 to 2 percent slopes	MgA	84.39	84.58	985
	LORAIN	Trumbull silty clay loam, 0 to 2 percent slopes	TrA	84.58	84.63	256
	LORAIN	Mahoning silt loam, 0 to 2 percent slopes	MgA	84.63	84.68	261
	LORAIN	Trumbull silty clay loam, 0 to 2 percent slopes	TrA	84.68	84.73	293
	LORAIN	Mahoning silt loam, 0 to 2 percent slopes	MgA	84.73	84.93	1045
	LORAIN	Trumbull silty clay loam, 0 to 2 percent slopes	TrA	84.93	85.00	348
	LORAIN	Mahoning silt loam, 0 to 2 percent slopes	MgA	85.00	85.02	120
	LORAIN	Trumbull silty clay loam, 0 to 2 percent slopes	TrA	85.02	85.05	151
	LORAIN	Mahoning silt loam, 0 to 2 percent slopes	MgA	85.05	85.16	575
	LORAIN	Mahoning silt loam, 2 to 6 percent slopes, moderately eroded	MgB2	85.16	85.20	229
	LORAIN	Orrville silt loam	Or	85.20	85.23	181
	LORAIN	Mahoning silt loam, 2 to 6 percent slopes	MgB	85.23	85.36	658
	LORAIN	Mahoning silt loam, 0 to 2 percent slopes	MgA	85.36	85.50	764

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	LORAIN	Trumbull silty clay loam, 0 to 2 percent slopes	TrA	85.50	85.53	121
	LORAIN	Mahoning silt loam, 2 to 6 percent slopes	MgB	85.53	85.62	480
	LORAIN	Mahoning silt loam, 0 to 2 percent slopes	MgA	85.62	85.76	777
	LORAIN	Mahoning silt loam, 2 to 6 percent slopes	MgB	85.76	85.79	130
	LORAIN	Mahoning silt loam, 0 to 2 percent slopes	MgA	85.79	85.88	456
	LORAIN	Trumbull silty clay loam, 0 to 2 percent slopes	TrA	85.88	85.94	332
	LORAIN	Mahoning silt loam, 0 to 2 percent slopes	MgA	85.94	86.21	1417
	LORAIN	Trumbull silty clay loam, 0 to 2 percent slopes	TrA	86.21	86.31	546
	LORAIN	Mahoning silt loam, 0 to 2 percent slopes	MgA	86.31	86.41	528
	LORAIN	Miner silty clay loam	Mr	86.41	86.43	101
	LORAIN	Mahoning silt loam, 0 to 2 percent slopes	MgA	86.43	86.67	1296
	LORAIN	Mahoning silt loam, 2 to 6 percent slopes	MgB	86.67	86.68	32
	LORAIN	Mahoning silt loam, 0 to 2 percent slopes	MgA	86.68	86.81	660
	LORAIN	Orrville silt loam	Or	86.81	86.86	312
	LORAIN	Trumbull silty clay loam, 0 to 2 percent slopes	TrA	86.86	86.88	61
	LORAIN	Mahoning silt loam, 0 to 2 percent slopes	MgA	86.88	87.06	949
	LORAIN	Trumbull silty clay loam, 0 to 2 percent slopes	TrA	87.06	87.12	360
	LORAIN	Mahoning silt loam, 0 to 2 percent slopes	MgA	87.12	87.33	1081
	LORAIN	Trumbull silty clay loam, 0 to 2 percent slopes	TrA	87.33	87.41	425
	LORAIN	Mahoning silt loam, 0 to 2 percent slopes	MgA	87.41	87.53	630
	LORAIN	Miner silty clay loam	Mr	87.53	87.60	357

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	LORAIN	Mahoning silt loam, 0 to 2 percent slopes	MgA	87.60	87.62	115
	LORAIN	Miner silty clay loam	Mr	87.62	87.71	479
	LORAIN	Haskins loam, 0 to 2 percent slopes	HsA	87.71	87.79	406
	LORAIN	Mahoning silt loam, 0 to 2 percent slopes	MgA	87.79	87.89	567
	LORAIN	Ellsworth silt loam, 2 to 6 percent slopes, moderately eroded	ElB2	87.89	87.91	87
	LORAIN	Orrville silt loam	Or	87.91	87.95	201
	LORAIN	Ellsworth silt loam, 2 to 6 percent slopes, moderately eroded	ElB2	87.95	87.98	188
	LORAIN	Haskins loam, 0 to 2 percent slopes	HsA	87.98	88.37	2018
	LORAIN	Lobdell silt loam	Lb	88.37	88.39	142
	LORAIN	Fitchville silt loam, low terrace, 0 to 2 percent slopes	FdA	88.39	88.43	177
	LORAIN	Ellsworth silt loam, 6 to 12 percent slopes, moderately eroded	ElC2	88.43	88.45	142
	LORAIN	Haskins loam, 0 to 2 percent slopes	HsA	88.45	88.70	1332
	LORAIN	Haskins loam, 2 to 6 percent slopes	HsB	88.70	88.74	197
	LORAIN	Haskins loam, 0 to 2 percent slopes	HsA	88.74	88.80	319
	LORAIN	Fitchville silt loam, low terrace, 0 to 2 percent slopes	FdA	88.80	88.83	168
	LORAIN	Water	W	88.83	88.85	78
	LORAIN	Fitchville silt loam, low terrace, 0 to 2 percent slopes	FdA	88.85	88.95	558
	LORAIN	Lobdell silt loam	Lb	88.95	88.96	20
	LORAIN	Water	W	88.96	88.97	52
	LORAIN	Lobdell silt loam	Lb	88.97	88.98	79
	LORAIN	Fitchville silt loam, low terrace, 0 to 2 percent slopes	FdA	88.98	89.06	422
	LORAIN	Lobdell silt loam	Lb	89.06	89.11	226

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	LORAIN	Fitchville silt loam, low terrace, 0 to 2 percent slopes	FdA	89.11	89.14	205
	LORAIN	Lobdell silt loam	Lb	89.14	89.20	267
	LORAIN	Fitchville silt loam, low terrace, 0 to 2 percent slopes	FdA	89.20	89.21	99
	LORAIN	Lobdell silt loam	Lb	89.21	89.26	224
	LORAIN	Fitchville silt loam, low terrace, 0 to 2 percent slopes	FdA	89.26	89.32	338
	LORAIN	Ellsworth silt loam, 12 to 18 percent slopes, moderately eroded	ElD2	89.32	89.35	164
	LORAIN	Mahoning-Tiro silt loams, 0 to 2 percent slopes	MkA	89.35	89.44	467
	LORAIN	Trumbull silty clay loam, 0 to 2 percent slopes	TrA	89.44	89.48	227
	LORAIN	Mahoning-Tiro silt loams, 0 to 2 percent slopes	MkA	89.48	89.56	399
	LORAIN	Trumbull silty clay loam, 0 to 2 percent slopes	TrA	89.56	89.58	126
	LORAIN	Mahoning-Tiro silt loams, 2 to 6 percent slopes	MkB	89.58	89.74	818
	LORAIN	Mahoning silt loam, 0 to 2 percent slopes	MgA	89.74	90.04	1586
	LORAIN	Trumbull silty clay loam, 0 to 2 percent slopes	TrA	90.04	90.06	144
	LORAIN	Mahoning silt loam, 0 to 2 percent slopes	MgA	90.06	90.17	576
	LORAIN	Mahoning silt loam, 2 to 6 percent slopes	MgB	90.17	90.34	861
	LORAIN	Mahoning silt loam, 0 to 2 percent slopes	MgA	90.34	90.43	470
	LORAIN	Mahoning silt loam, 2 to 6 percent slopes	MgB	90.43	90.47	207
	LORAIN	Mahoning silt loam, 0 to 2 percent slopes	MgA	90.47	90.55	468
	LORAIN	Ellsworth silt loam, 2 to 6 percent slopes	ElB	90.55	90.57	94
	LORAIN	Mahoning silt loam, 0 to 2 percent slopes	MgA	90.57	90.71	722
	LORAIN	Mahoning silt loam, 2 to 6 percent slopes	MgB	90.71	90.77	313

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	LORAIN	Mahoning silt loam, 0 to 2 percent slopes	MgA	90.77	90.93	849
	LORAIN	Trumbull silty clay loam, 0 to 2 percent slopes	TrA	90.93	90.98	269
	LORAIN	Mahoning silt loam, 0 to 2 percent slopes	MgA	90.98	91.39	2171
	LORAIN	Trumbull silty clay loam, 0 to 2 percent slopes	TrA	91.39	91.45	335
	LORAIN	Mahoning silt loam, 0 to 2 percent slopes	MgA	91.45	91.57	638
	LORAIN	Trumbull silty clay loam, 0 to 2 percent slopes	TrA	91.57	91.61	189
	LORAIN	Mahoning silt loam, 0 to 2 percent slopes	MgA	91.61	91.66	284
	LORAIN	Trumbull silty clay loam, 0 to 2 percent slopes	TrA	91.66	91.78	625
	LORAIN	Mahoning silt loam, 0 to 2 percent slopes	MgA	91.78	92.06	1453
	LORAIN	Trumbull silty clay loam, 0 to 2 percent slopes	TrA	92.06	92.10	199
	LORAIN	Mahoning silt loam, 0 to 2 percent slopes	MgA	92.10	92.62	2768
	LORAIN	Trumbull silty clay loam, 0 to 2 percent slopes	TrA	92.62	92.73	580
	LORAIN	Mahoning silt loam, 0 to 2 percent slopes	MgA	92.73	93.01	1497
	LORAIN	Trumbull silty clay loam, 0 to 2 percent slopes	TrA	93.01	93.04	150
	LORAIN	Mahoning-Tiro silt loams, 0 to 2 percent slopes	MkA	93.04	93.29	1312
	LORAIN	Miner silty clay loam	Mr	93.29	93.34	259
	LORAIN	Trumbull silty clay loam, 0 to 2 percent slopes	TrA	93.34	93.57	1194
	LORAIN	Mahoning-Tiro silt loams, 0 to 2 percent slopes	MkA	93.57	94.20	3354
	LORAIN	Mahoning silt loam, 0 to 2 percent slopes	MgA	94.20	94.34	732
	LORAIN	Miner silty clay loam	Mr	94.34	94.40	346
	LORAIN	Mahoning silt loam, 0 to 2 percent slopes	MgA	94.40	94.76	1879

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	LORAIN	Mitiwanga silt loam, 2 to 6 percent slopes	MtB	94.76	95.28	2763
	LORAIN	Mahoning silt loam, 0 to 2 percent slopes	MgA	95.28	95.35	365
	LORAIN	Miner silty clay loam	Mr	95.35	95.40	239
	LORAIN	Mahoning silt loam, 0 to 2 percent slopes	MgA	95.40	95.56	873
	LORAIN	Miner silty clay loam	Mr	95.56	95.59	132
	LORAIN	Mahoning-Tiro silt loams, 0 to 2 percent slopes	MkA	95.59	95.68	498
	LORAIN	Miner silty clay loam	Mr	95.68	95.73	223
	LORAIN	Mahoning-Tiro silt loams, 0 to 2 percent slopes	MkA	95.73	95.75	145
	LORAIN	Miner silty clay loam	Mr	95.75	95.87	615
	LORAIN	Mahoning-Tiro silt loams, 0 to 2 percent slopes	MkA	95.87	95.93	315
	LORAIN	Bogart loam, 2 to 6 percent slopes	BtB	95.93	95.97	217
	LORAIN	Miner silty clay loam	Mr	95.97	96.02	249
	LORAIN	Mahoning-Tiro silt loams, 0 to 2 percent slopes	MkA	96.02	96.35	1773
	LORAIN	Trumbull silty clay loam, 0 to 2 percent slopes	TrA	96.35	96.40	241
	LORAIN	Mahoning silt loam, 0 to 2 percent slopes	MgA	96.40	96.45	258
	LORAIN	Mahoning-Tiro silt loams, 0 to 2 percent slopes	MkA	96.45	96.53	452
	LORAIN	Trumbull silty clay loam, 0 to 2 percent slopes	TrA	96.53	96.69	855
	LORAIN	Mahoning-Tiro silt loams, 0 to 2 percent slopes	MkA	96.69	97.04	1818
	LORAIN	Sebring silt loam	Sb	97.04	97.05	73
	LORAIN	Mahoning-Tiro silt loams, 0 to 2 percent slopes	MkA	97.05	97.31	1352
	LORAIN	Sebring silt loam	Sb	97.31	97.37	331
	LORAIN	Mahoning-Tiro silt loams, 0 to 2 percent slopes	MkA	97.37	97.53	825
	LORAIN	Mahoning silt loam, 2 to 6 percent slopes	MgB	97.53	97.68	819

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	LORAIN	Ellsworth silt loam, 6 to 12 percent slopes, moderately eroded	ElC2	97.68	97.82	716
	LORAIN	Bogart loam, 2 to 6 percent slopes	BtB	97.82	97.82	1
	LORAIN	Ellsworth silt loam, 2 to 6 percent slopes	ElB	97.82	97.85	148
	LORAIN	Bogart loam, 0 to 2 percent slopes	BtA	97.85	97.91	341
	LORAIN	Jimtown loam, 0 to 2 percent slopes	JtA	97.91	97.95	198
	LORAIN	Bogart loam, 0 to 2 percent slopes	BtA	97.95	97.99	225
	LORAIN	Orrville silt loam	Or	97.99	98.09	511
	LORAIN	Ellsworth silt loam, 18 to 50 percent slopes, moderately eroded	ElF2	98.09	98.21	622
	LORAIN	Alexandria silt loam, 25 to 50 percent slopes	AgF	98.21	98.21	22
	ERIE	Alexandria silt loam, 25 to 50 percent slopes	AgF	98.21	98.22	68
	ERIE	Cardington silt loam, 2 to 6 percent slopes	CaB	98.22	98.41	989
	ERIE	Bennington silt loam, 0 to 2 percent slopes	BgA	98.41	98.45	226
	ERIE	Cardington silt loam, 2 to 6 percent slopes	CaB	98.45	98.50	240
	ERIE	Condit silt loam, 0 to 1 percent slopes	CoA	98.50	98.57	353
	ERIE	Haskins loam, 0 to 2 percent slopes	HkA	98.57	98.62	312
	ERIE	Bennington silt loam, 0 to 2 percent slopes	BgA	98.62	98.76	693
	ERIE	Haskins loam, 0 to 2 percent slopes	HkA	98.76	98.83	381
	ERIE	Bennington silt loam, 0 to 2 percent slopes	BgA	98.83	98.91	413
	ERIE	Miner silty clay loam, 0 to 1 percent slopes	MrA	98.91	98.94	203
	ERIE	Bennington silt loam, 2 to 6 percent slopes	BgB	98.94	98.97	118

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	ERIE	Bennington silt loam, 0 to 2 percent slopes	BgA	98.97	99.01	224
	ERIE	Bennington silt loam, 2 to 6 percent slopes	BgB	99.01	99.06	282
	ERIE	Miner silty clay loam, 0 to 1 percent slopes	MrA	99.06	99.18	610
	ERIE	Bennington silt loam, 2 to 6 percent slopes	BgB	99.18	99.20	126
	ERIE	Miner silty clay loam, 0 to 1 percent slopes	MrA	99.20	99.22	90
	ERIE	Bennington silt loam, 2 to 6 percent slopes	BgB	99.22	99.32	537
	ERIE	Bennington silt loam, 0 to 2 percent slopes	BgA	99.32	99.36	195
	ERIE	Bennington silt loam, 2 to 6 percent slopes	BgB	99.36	99.41	286
	ERIE	Mermill silty clay loam, 0 to 1 percent slopes	MeA	99.41	99.43	120
	ERIE	Haskins loam, 0 to 2 percent slopes	HkA	99.43	99.46	138
	ERIE	Mermill silty clay loam, 0 to 1 percent slopes	MeA	99.46	99.48	86
	ERIE	Haskins loam, 0 to 2 percent slopes	HkA	99.48	99.49	79
	ERIE	Bennington silt loam, 2 to 6 percent slopes	BgB	99.49	99.52	149
	ERIE	Bennington silt loam, 0 to 2 percent slopes	BgA	99.52	99.65	660
	ERIE	Udorthents, loamy, 0 to 6 percent slopes	UdB	99.65	99.73	443
	ERIE	Bennington silt loam, 0 to 2 percent slopes	BgA	99.73	99.81	440
	ERIE	Cardington silt loam, 2 to 6 percent slopes	CaB	99.81	99.86	228
	ERIE	Bennington silt loam, 0 to 2 percent slopes	BgA	99.86	99.97	585
	ERIE	Bennington silt loam, 2 to 6 percent slopes	BgB	99.97	99.99	102
	ERIE	Bennington silt loam, 0 to 2 percent slopes	BgA	99.99	100.07	451

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	ERIE	Chili loam, loamy substratum, 2 to 6 percent slopes	ChB	100.07	100.20	675
	ERIE	Amanda-Dekalb-Rock outcrop association, 40 to 70 percent slopes	AnG	100.20	100.34	718
	ERIE	Orrville silt loam, bedrock substratum, 0 to 2 percent slopes, occasionally flooded	OpA	100.34	100.38	263
	ERIE	Water	W	100.38	100.42	172
	ERIE	Orrville silt loam, bedrock substratum, 0 to 2 percent slopes, occasionally flooded	OpA	100.42	100.44	130
	ERIE	Amanda-Dekalb-Rock outcrop association, 40 to 70 percent slopes	AnG	100.44	100.50	312
	ERIE	Wakeman sandy loam, 2 to 6 percent slopes	WaB	100.50	100.57	356
	ERIE	Bennington silt loam, 0 to 2 percent slopes	BgA	100.57	101.00	2260
	ERIE	Cardington silt loam, 2 to 6 percent slopes	CaB	101.00	101.04	253
	ERIE	Condit silt loam, 0 to 1 percent slopes	CoA	101.04	101.07	132
	ERIE	Bennington silt loam, 0 to 2 percent slopes	BgA	101.07	101.13	294
	ERIE	Condit silt loam, 0 to 1 percent slopes	CoA	101.13	101.18	315
	ERIE	Cardington silt loam, 2 to 6 percent slopes	CaB	101.18	101.20	85
	ERIE	Rawson sandy loam, 0 to 2 percent slopes	RcA	101.20	101.26	316
	ERIE	Condit silt loam, 0 to 1 percent slopes	CoA	101.26	101.28	87
	ERIE	Rawson sandy loam, 0 to 2 percent slopes	RcA	101.28	101.48	1054
	ERIE	Cardington silt loam, 2 to 6 percent slopes	CaB	101.48	101.69	1105
	ERIE	Orrville silt loam, bedrock substratum, 0 to 2 percent slopes, occasionally flooded	OpA	101.69	101.71	150
	ERIE	Cardington silty clay loam, 6 to 12 percent slopes, eroded	CbC2	101.71	101.74	112

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	ERIE	Orrville silt loam, bedrock substratum, 0 to 2 percent slopes, occasionally flooded	OpA	101.74	101.78	251
	ERIE	Cardington silty clay loam, 6 to 12 percent slopes, eroded	CbC2	101.78	101.83	232
	ERIE	Orrville silt loam, bedrock substratum, 0 to 2 percent slopes, occasionally flooded	OpA	101.83	101.90	376
	ERIE	Cardington silty clay loam, 6 to 12 percent slopes, eroded	CbC2	101.90	101.94	194
	ERIE	Cardington silt loam, 2 to 6 percent slopes	CaB	101.94	101.96	108
	ERIE	Cardington silty clay loam, 6 to 12 percent slopes, eroded	CbC2	101.96	101.99	186
	ERIE	Cardington silt loam, 2 to 6 percent slopes	CaB	101.99	102.00	47
	ERIE	Cardington silty clay loam, 6 to 12 percent slopes, eroded	CbC2	102.00	102.05	258
	ERIE	Cardington silt loam, 2 to 6 percent slopes	CaB	102.05	102.09	193
	ERIE	Cardington silty clay loam, 6 to 12 percent slopes, eroded	CbC2	102.09	102.11	150
	ERIE	Cardington silt loam, 2 to 6 percent slopes	CaB	102.11	102.15	189
	ERIE	Bennington silt loam, 0 to 2 percent slopes	BgA	102.15	102.20	283
	ERIE	Cardington silt loam, 2 to 6 percent slopes	CaB	102.20	102.23	121
	ERIE	Cardington silty clay loam, 6 to 12 percent slopes, eroded	CbC2	102.23	102.24	57
	ERIE	Bennington silt loam, 0 to 2 percent slopes	BgA	102.24	102.27	172
	ERIE	Condit silt loam, 0 to 1 percent slopes	CoA	102.27	102.30	142
	ERIE	Bennington silt loam, 0 to 2 percent slopes	BgA	102.30	102.44	748
	ERIE	Condit silt loam, 0 to 1 percent slopes	CoA	102.44	102.51	359
	ERIE	Bennington silt loam, 0 to 2 percent slopes	BgA	102.51	102.52	75
	ERIE	Condit silt loam, 0 to 1 percent slopes	CoA	102.52	102.52	15

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	ERIE	Bennington silt loam, 0 to 2 percent slopes	BgA	102.52	102.55	136
	ERIE	Condit silt loam, 0 to 1 percent slopes	CoA	102.55	102.65	531
	ERIE	Bennington silt loam, 0 to 2 percent slopes	BgA	102.65	102.79	725
	ERIE	Condit silt loam, 0 to 1 percent slopes	CoA	102.79	102.84	300
	ERIE	Cardington silt loam, 2 to 6 percent slopes	CaB	102.84	102.89	249
	ERIE	Condit silt loam, 0 to 1 percent slopes	CoA	102.89	102.96	378
	ERIE	Cardington silt loam, 2 to 6 percent slopes	CaB	102.96	102.99	135
	ERIE	Condit silt loam, 0 to 1 percent slopes	CoA	102.99	103.02	182
	ERIE	Bennington silt loam, 2 to 6 percent slopes	BgB	103.02	103.07	266
	ERIE	Bennington silt loam, 0 to 2 percent slopes	BgA	103.07	103.09	87
	ERIE	Bennington silt loam, 2 to 6 percent slopes	BgB	103.09	103.13	239
	ERIE	Condit silt loam, 0 to 1 percent slopes	CoA	103.13	103.23	524
	ERIE	Oshtemo loamy sand, 0 to 6 percent slopes	OsB	103.23	103.30	339
	ERIE	Holly silt loam, 0 to 1 percent slopes, occasionally flooded	HoA	103.30	103.34	245
	ERIE	Bennington silt loam, 0 to 2 percent slopes	BgA	103.34	103.38	195
	ERIE	Holly silt loam, 0 to 1 percent slopes, occasionally flooded	HoA	103.38	103.38	5
	ERIE	Bennington silt loam, 0 to 2 percent slopes	BgA	103.38	103.41	165
	ERIE	Holly silt loam, 0 to 1 percent slopes, occasionally flooded	HoA	103.41	103.48	330
	ERIE	Jimtown loam, 0 to 2 percent slopes	JtA	103.48	103.55	408
	ERIE	Holly silt loam, 0 to 1 percent slopes, occasionally flooded	HoA	103.55	103.57	110

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	ERIE	Jimtown loam, 0 to 2 percent slopes	JtA	103.57	103.76	985
	ERIE	Chili loam, loamy substratum, 2 to 6 percent slopes	ChB	103.76	103.93	874
	ERIE	Condit silt loam, 0 to 1 percent slopes	CoA	103.93	103.95	106
	ERIE	Haskins loam, 0 to 2 percent slopes	HkA	103.95	103.97	114
	ERIE	Bennington silt loam, 2 to 6 percent slopes	BgB	103.97	104.02	255
	ERIE	Mitiwanga silt loam, 0 to 2 percent slopes	MxA	104.02	104.39	1974
	ERIE	Bennington silt loam, 2 to 6 percent slopes	BgB	104.39	104.55	860
	ERIE	Bennington silt loam, 0 to 2 percent slopes	BgA	104.55	104.65	536
	ERIE	Jimtown loam, 0 to 2 percent slopes	JtA	104.65	104.73	412
	ERIE	Oshtemo loamy sand, 0 to 6 percent slopes	OsB	104.73	104.81	409
	ERIE	Jimtown loam, 0 to 2 percent slopes	JtA	104.81	104.83	81
	ERIE	Haskins loam, 0 to 2 percent slopes	HkA	104.83	104.85	138
	ERIE	Elnora loamy fine sand, 0 to 4 percent slopes	EnA	104.85	104.90	272
	ERIE	Mermill silty clay loam, 0 to 1 percent slopes	MeA	104.90	104.92	105
	ERIE	Rimer loamy fine sand, 0 to 2 percent slopes	RgA	104.92	104.95	148
	ERIE	Jimtown loam, 0 to 2 percent slopes	JtA	104.95	105.00	260
	ERIE	Mermill silty clay loam, 0 to 1 percent slopes	MeA	105.00	105.02	102
	ERIE	Elnora loamy fine sand, 0 to 4 percent slopes	EnA	105.02	105.09	360
	ERIE	Mermill silty clay loam, 0 to 1 percent slopes	MeA	105.09	105.11	120
	ERIE	Oshtemo loamy sand, 0 to 6 percent slopes	OsB	105.11	105.25	747

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	ERIE	Mermill silty clay loam, 0 to 1 percent slopes	MeA	105.25	105.28	127
	ERIE	Bixler loamy fine sand, 0 to 2 percent slopes	BkA	105.28	105.37	474
	ERIE	Elnora loamy fine sand, 0 to 4 percent slopes	EnA	105.37	105.40	204
	ERIE	Bixler loamy fine sand, 0 to 2 percent slopes	BkA	105.40	105.42	59
	ERIE	Mermill silty clay loam, 0 to 1 percent slopes	MeA	105.42	105.48	340
	ERIE	Condit silt loam, 0 to 1 percent slopes	CoA	105.48	105.54	312
	ERIE	Haskins loam, 0 to 2 percent slopes	HkA	105.54	105.59	253
	ERIE	Mermill silty clay loam, 0 to 1 percent slopes	MeA	105.59	105.61	142
	ERIE	Haskins loam, 0 to 2 percent slopes	HkA	105.61	105.85	1261
	ERIE	Rawson sandy loam, 2 to 6 percent slopes	RcB	105.85	105.88	151
	ERIE	Mermill silty clay loam, 0 to 1 percent slopes	MeA	105.88	106.09	1084
	ERIE	Millgrove loam, 0 to 1 percent slopes	MgA	106.09	106.35	1377
	ERIE	Tuscola fine sandy loam, 2 to 6 percent slopes	TuB	106.35	106.38	155
	ERIE	Jimtown loam, 0 to 2 percent slopes	JtA	106.38	106.41	178
	ERIE	Millgrove loam, 0 to 1 percent slopes	MgA	106.41	106.60	1003
	ERIE	Jimtown loam, 0 to 2 percent slopes	JtA	106.60	106.63	150
	ERIE	Millgrove loam, 0 to 1 percent slopes	MgA	106.63	106.67	224
	ERIE	Oshtemo loamy sand, 0 to 6 percent slopes	OsB	106.67	106.72	263
	ERIE	Millgrove loam, 0 to 1 percent slopes	MgA	106.72	106.77	272
	ERIE	Jimtown loam, 0 to 2 percent slopes	JtA	106.77	106.79	115

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	ERIE	Millgrove loam, 0 to 1 percent slopes	MgA	106.79	106.94	763
	ERIE	Udipsamments-Spinks complex, 0 to 6 percent slopes	UcB	106.94	107.02	450
	ERIE	Millgrove loam, 0 to 1 percent slopes	MgA	107.02	107.03	54
	ERIE	Udipsamments-Spinks complex, 0 to 6 percent slopes	UcB	107.03	107.03	2
	ERIE	Jimtown loam, 0 to 2 percent slopes	JtA	107.03	107.12	476
	ERIE	Wakeman sandy loam, 2 to 6 percent slopes	WaB	107.12	107.22	494
	ERIE	Wakeman sandy loam, 6 to 12 percent slopes	WaC	107.22	107.25	175
	ERIE	Millgrove loam, 0 to 1 percent slopes	MgA	107.25	107.29	216
	ERIE	Jimtown loam, 0 to 2 percent slopes	JtA	107.29	107.36	381
	ERIE	Udorthents, loamy, 0 to 6 percent slopes	UdB	107.36	107.39	134
	ERIE	Millgrove loam, 0 to 1 percent slopes	MgA	107.39	107.44	260
	ERIE	Jimtown loam, 0 to 2 percent slopes	JtA	107.44	107.52	443
	ERIE	Udipsamments-Spinks complex, 0 to 6 percent slopes	UcB	107.52	107.82	1576
	ERIE	Conotton loam, 2 to 6 percent slopes	CtB	107.82	107.86	209
	ERIE	Jimtown loam, 0 to 2 percent slopes	JtA	107.86	107.88	96
	ERIE	Conotton loam, 2 to 6 percent slopes	CtB	107.88	107.91	138
	ERIE	Jimtown loam, 0 to 2 percent slopes	JtA	107.91	107.94	161
	ERIE	Conotton loam, 2 to 6 percent slopes	CtB	107.94	107.94	35
	ERIE	Conotton gravelly loam, 6 to 12 percent slopes	CuC	107.94	107.97	152
	ERIE	Allis clay loam, 0 to 2 percent slopes	AkA	107.97	107.99	105

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	ERIE	Condit silt loam, 0 to 1 percent slopes	CoA	107.99	108.03	216
	ERIE	Allis clay loam, 0 to 2 percent slopes	AkA	108.03	108.11	432
	ERIE	Amanda-Dekalb-Rock outcrop association, 40 to 70 percent slopes	AnG	108.11	108.13	97
	ERIE	Millgrove loam, 0 to 1 percent slopes	MgA	108.13	108.17	222
	ERIE	Bennington silt loam, 0 to 2 percent slopes	BgA	108.17	108.19	87
	ERIE	Milford silty clay loam, 0 to 1 percent slopes	MfA	108.19	108.61	2224
	ERIE	Kibbie fine sandy loam, 0 to 2 percent slopes	KbA	108.61	108.72	558
	ERIE	Jimtown loam, 0 to 2 percent slopes	JtA	108.72	108.73	79
	ERIE	Kibbie fine sandy loam, 0 to 2 percent slopes	KbA	108.73	108.75	93
	ERIE	Jimtown loam, 0 to 2 percent slopes	JtA	108.75	108.76	58
	ERIE	Ogontz silt loam, 2 to 6 percent slopes	OhB	108.76	108.80	210
	ERIE	Bennington silt loam, 0 to 2 percent slopes	BgA	108.80	108.87	375
	ERIE	Bennington silt loam, 2 to 6 percent slopes	BgB	108.87	108.93	301
	ERIE	Cardington silty clay loam, 6 to 12 percent slopes, eroded	CbC2	108.93	108.95	132
	ERIE	Holly silt loam, 0 to 1 percent slopes, occasionally flooded	HoA	108.95	108.98	130
	ERIE	Zurich silt loam, 12 to 18 percent slopes, eroded	ZuD2	108.98	109.00	129
	ERIE	Del Rey silt loam, 0 to 2 percent slopes	DeA	109.00	109.02	76
	ERIE	Ogontz silt loam, 2 to 6 percent slopes	OhB	109.02	109.06	222
	ERIE	Del Rey silt loam, 0 to 2 percent slopes	DeA	109.06	109.11	258
	ERIE	Zurich silt loam, 25 to 40 percent slopes	ZuF	109.11	109.12	72

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	ERIE	Holly silt loam, 0 to 1 percent slopes, occasionally flooded	HoA	109.12	109.25	654
	ERIE	Orrville silt loam, bedrock substratum, 0 to 2 percent slopes, occasionally flooded	OpA	109.25	109.26	87
	ERIE	Holly silt loam, 0 to 1 percent slopes, occasionally flooded	HoA	109.26	109.32	300
	ERIE	Zurich silt loam, 25 to 40 percent slopes	ZuF	109.32	109.34	121
	ERIE	Tuscola fine sandy loam, 2 to 6 percent slopes	TuB	109.34	109.37	148
	ERIE	Kibbie fine sandy loam, 0 to 2 percent slopes	KbA	109.37	109.44	395
	ERIE	Colwood loam, 0 to 1 percent slopes	CmA	109.44	109.51	356
	ERIE	Kibbie fine sandy loam, 0 to 2 percent slopes	KbA	109.51	109.55	175
	ERIE	Colwood loam, 0 to 1 percent slopes	CmA	109.55	109.65	547
	ERIE	Kibbie fine sandy loam, 0 to 2 percent slopes	KbA	109.65	109.79	761
	ERIE	Zurich silt loam, 25 to 40 percent slopes	ZuF	109.79	109.81	71
	ERIE	Holly silt loam, 0 to 1 percent slopes, occasionally flooded	HoA	109.81	109.87	330
	ERIE	Zurich silt loam, 25 to 40 percent slopes	ZuF	109.87	109.91	207
	ERIE	Ogontz silt loam, 2 to 6 percent slopes	OhB	109.91	109.92	78
	ERIE	Bixler loamy fine sand, 0 to 2 percent slopes	BkA	109.92	109.96	182
	ERIE	Tuscola fine sandy loam, 2 to 6 percent slopes	TuB	109.96	109.98	116
	ERIE	Kibbie fine sandy loam, 0 to 2 percent slopes	KbA	109.98	110.07	458
	ERIE	Bixler loamy fine sand, 0 to 2 percent slopes	BkA	110.07	110.16	485
	ERIE	Bixler loamy fine sand, 2 to 6 percent slopes	BkB	110.16	110.19	183
	ERIE	Zurich silt loam, 25 to 40 percent slopes	ZuF	110.19	110.22	124

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	ERIE	Holly silt loam, 0 to 1 percent slopes, occasionally flooded	HoA	110.22	110.27	305
	ERIE	Zurich silt loam, 18 to 25 percent slopes, eroded	ZuE2	110.27	110.30	117
	ERIE	Ogontz silt loam, 2 to 6 percent slopes	OhB	110.30	110.32	107
	ERIE	Bixler loamy fine sand, 0 to 2 percent slopes	BkA	110.32	110.45	683
	ERIE	Zurich silt loam, 18 to 25 percent slopes, eroded	ZuE2	110.45	110.46	96
	ERIE	Holly silt loam, 0 to 1 percent slopes, occasionally flooded	HoA	110.46	110.47	58
	ERIE	Zurich silt loam, 12 to 18 percent slopes, eroded	ZuD2	110.47	110.53	267
	ERIE	Bixler loamy fine sand, 0 to 2 percent slopes	BkA	110.53	110.58	268
	ERIE	Colwood loam, 0 to 1 percent slopes	CmA	110.58	110.63	281
	ERIE	Kibbie fine sandy loam, 0 to 2 percent slopes	KbA	110.63	110.76	665
	ERIE	Colwood loam, 0 to 1 percent slopes	CmA	110.76	110.85	506
	ERIE	Kibbie fine sandy loam, 0 to 2 percent slopes	KbA	110.85	110.98	662
	ERIE	Bixler loamy fine sand, 0 to 2 percent slopes	BkA	110.98	111.03	307
	ERIE	Kibbie fine sandy loam, 0 to 2 percent slopes	KbA	111.03	111.09	302
	ERIE	Colwood loam, 0 to 1 percent slopes	CmA	111.09	111.12	137
	ERIE	Kibbie fine sandy loam, 0 to 2 percent slopes	KbA	111.12	111.15	172
	ERIE	Bixler loamy fine sand, 0 to 2 percent slopes	BkA	111.15	111.20	263
	ERIE	Tuscola fine sandy loam, 2 to 6 percent slopes	TuB	111.20	111.22	108
	ERIE	Tuscola fine sandy loam, 0 to 2 percent slopes	TuA	111.22	111.32	511
	ERIE	Zurich silt loam, 25 to 40 percent slopes	ZuF	111.32	111.34	125

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	ERIE	Holly silt loam, 0 to 1 percent slopes, occasionally flooded	HoA	111.34	111.38	208
	ERIE	Zurich silt loam, 25 to 40 percent slopes	ZuF	111.38	111.40	128
	ERIE	Tuscola fine sandy loam, 0 to 2 percent slopes	TuA	111.40	111.45	259
	ERIE	Kibbie fine sandy loam, 0 to 2 percent slopes	KbA	111.45	111.62	879
	ERIE	Tuscola fine sandy loam, 0 to 2 percent slopes	TuA	111.62	111.64	110
	ERIE	Kibbie fine sandy loam, 0 to 2 percent slopes	KbA	111.64	111.65	56
	ERIE	Tuscola fine sandy loam, 0 to 2 percent slopes	TuA	111.65	111.68	142
	ERIE	Zurich silt loam, 25 to 40 percent slopes	ZuF	111.68	111.70	132
	ERIE	Holly silt loam, 0 to 1 percent slopes, occasionally flooded	HoA	111.70	111.73	133
	ERIE	Saylesville silt loam, 25 to 40 percent slopes	SbF	111.73	111.74	66
	ERIE	Shinrock silt loam, 2 to 6 percent slopes	ShB	111.74	111.77	162
	ERIE	Tuscola fine sandy loam, 0 to 2 percent slopes	TuA	111.77	111.80	162
	ERIE	Rimer loamy fine sand, 0 to 2 percent slopes	RgA	111.80	111.86	299
	ERIE	Shinrock silt loam, 2 to 6 percent slopes	ShB	111.86	111.92	331
	ERIE	Saylesville silt loam, 25 to 40 percent slopes	SbF	111.92	112.02	539
	ERIE	Del Rey silt loam, 0 to 2 percent slopes	DeA	112.02	112.04	88
	ERIE	Saylesville silt loam, 25 to 40 percent slopes	SbF	112.04	112.07	161
	ERIE	Del Rey silt loam, 0 to 2 percent slopes	DeA	112.07	112.11	220
	ERIE	Saylesville silt loam, 25 to 40 percent slopes	SbF	112.11	112.14	165
	ERIE	Holly silt loam, 0 to 1 percent slopes, occasionally flooded	HoA	112.14	112.15	38

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	ERIE	Saylesville silt loam, 25 to 40 percent slopes	SbF	112.15	112.19	201
	ERIE	Del Rey silt loam, 0 to 2 percent slopes	DeA	112.19	112.24	259
	ERIE	Shinrock silty clay loam, 12 to 18 percent slopes, eroded	SkD2	112.24	112.38	736
	ERIE	Saylesville silt loam, 25 to 40 percent slopes	SbF	112.38	112.48	540
	ERIE	Holly silt loam, 0 to 1 percent slopes, occasionally flooded	HoA	112.48	112.51	153
	ERIE	Saylesville silt loam, 25 to 40 percent slopes	SbF	112.51	112.53	127
	ERIE	Shinrock silt loam, 2 to 6 percent slopes	ShB	112.53	112.61	401
	ERIE	Shinrock silty clay loam, 6 to 12 percent slopes, eroded	SkC2	112.61	112.62	74
	ERIE	Saylesville silt loam, 25 to 40 percent slopes	SbF	112.62	112.64	109
	ERIE	Shinrock silty clay loam, 6 to 12 percent slopes, eroded	SkC2	112.64	112.66	76
	ERIE	Saylesville silt loam, 25 to 40 percent slopes	SbF	112.66	112.69	157
	ERIE	Orrville silt loam, bedrock substratum, 0 to 2 percent slopes, occasionally flooded	OpA	112.69	112.79	533
	ERIE	Nolin silt loam, 0 to 2 percent slopes, occasionally flooded	NoA	112.79	112.84	261
	ERIE	Water	W	112.84	112.88	243
	ERIE	Nolin silt loam, 0 to 2 percent slopes, occasionally flooded	NoA	112.88	112.95	321
	ERIE	Saylesville silt loam, 25 to 40 percent slopes	SbF	112.95	112.97	130
	ERIE	Shinrock silt loam, 2 to 6 percent slopes	ShB	112.97	112.99	81
	ERIE	Saylesville silt loam, 25 to 40 percent slopes	SbF	112.99	113.02	208
	ERIE	Shinrock silty clay loam, 12 to 18 percent slopes, eroded	SkD2	113.02	113.05	159
	ERIE	Saylesville silt loam, 25 to 40 percent slopes	SbF	113.05	113.08	145

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	ERIE	Shinrock silty clay loam, 12 to 18 percent slopes, eroded	SkD2	113.08	113.16	399
	ERIE	Shinrock silt loam, 2 to 6 percent slopes	ShB	113.16	113.26	560
	ERIE	Shinrock silty clay loam, 6 to 12 percent slopes, eroded	SkC2	113.26	113.28	108
	ERIE	Shinrock silt loam, 2 to 6 percent slopes	ShB	113.28	113.30	82
	ERIE	Shinrock silty clay loam, 6 to 12 percent slopes, eroded	SkC2	113.30	113.41	594
	ERIE	Orrville silt loam, bedrock substratum, 0 to 2 percent slopes, occasionally flooded	OpA	113.41	113.49	396
	ERIE	Shinrock silty clay loam, 12 to 18 percent slopes, eroded	SkD2	113.49	113.56	373
	ERIE	Ogontz silt loam, 2 to 6 percent slopes	OhB	113.56	113.63	369
	ERIE	Ogontz fine sandy loam, 0 to 2 percent slopes	OgA	113.63	113.65	132
	ERIE	Ogontz silt loam, 2 to 6 percent slopes	OhB	113.65	113.71	296
	ERIE	Ogontz fine sandy loam, 0 to 2 percent slopes	OgA	113.71	113.83	641
	ERIE	Ogontz silt loam, 2 to 6 percent slopes	OhB	113.83	113.86	138
	ERIE	Shinrock silty clay loam, 6 to 12 percent slopes, eroded	SkC2	113.86	113.89	194
	ERIE	Ogontz silt loam, 2 to 6 percent slopes	OhB	113.89	113.91	86
	ERIE	Shinrock silty clay loam, 6 to 12 percent slopes, eroded	SkC2	113.91	114.03	611
	ERIE	Ogontz silt loam, 2 to 6 percent slopes	OhB	114.03	114.13	565
	ERIE	Zurich silt loam, 6 to 12 percent slopes, eroded	ZuC2	114.13	114.17	189
	ERIE	Ogontz fine sandy loam, 0 to 2 percent slopes	OgA	114.17	114.21	247
	ERIE	Zurich silt loam, 12 to 18 percent slopes, eroded	ZuD2	114.21	114.32	562
	ERIE	Zurich silt loam, 18 to 25 percent slopes, eroded	ZuE2	114.32	114.34	86

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	ERIE	Holly silt loam, 0 to 1 percent slopes, occasionally flooded	HoA	114.34	114.37	161
	ERIE	Zurich silt loam, 12 to 18 percent slopes, eroded	ZuD2	114.37	114.45	427
	ERIE	Ogontz silt loam, 2 to 6 percent slopes	OhB	114.45	114.66	1129
	ERIE	Zurich silt loam, 12 to 18 percent slopes, eroded	ZuD2	114.66	114.70	210
	ERIE	Zurich silt loam, 18 to 25 percent slopes, eroded	ZuE2	114.70	114.72	71
	ERIE	Holly silt loam, 0 to 1 percent slopes, occasionally flooded	HoA	114.72	114.75	193
	ERIE	Shinrock silty clay loam, 12 to 18 percent slopes, eroded	SkD2	114.75	114.86	545
	ERIE	Holly silt loam, 0 to 1 percent slopes, occasionally flooded	HoA	114.86	114.90	234
	ERIE	Shinrock silty clay loam, 12 to 18 percent slopes, eroded	SkD2	114.90	114.91	70
	ERIE	Zurich silt loam, 12 to 18 percent slopes, eroded	ZuD2	114.91	114.99	378
	ERIE	Shinrock silty clay loam, 12 to 18 percent slopes, eroded	SkD2	114.99	115.05	322
	ERIE	Tuscola fine sandy loam, 0 to 2 percent slopes	TuA	115.05	115.23	995
	ERIE	Kibbie fine sandy loam, 0 to 2 percent slopes	KbA	115.23	115.81	3031
	ERIE	Colwood loam, 0 to 1 percent slopes	CmA	115.81	115.87	314
	ERIE	Kibbie fine sandy loam, 0 to 2 percent slopes	KbA	115.87	116.19	1693
	ERIE	Haskins loam, 0 to 2 percent slopes	HkA	116.19	116.22	149
	ERIE	Pewamo silty clay loam, 0 to 1 percent slopes	PcA	116.22	117.26	5508
	ERIE	Jimtown loam, 0 to 2 percent slopes	JtA	117.26	117.31	247
	ERIE	Pewamo silty clay loam, 0 to 1 percent slopes	PcA	117.31	117.33	135
	ERIE	Bennington silt loam, 0 to 2 percent slopes	BgA	117.33	117.39	320

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	ERIE	Colwood silt loam, bedrock substratum, 0 to 1 percent slopes	CnA	117.39	117.52	674
	ERIE	Hornell silty clay loam, 0 to 2 percent slopes	HsA	117.52	117.56	188
	ERIE	Hornell silt loam, 2 to 6 percent slopes	HrB	117.56	117.59	162
	ERIE	Fries silty clay loam, 0 to 1 percent slopes	FrA	117.59	117.83	1283
	ERIE	Millgrove loam, 0 to 1 percent slopes	MgA	117.83	117.98	800
	ERIE	Elliott silt loam, bedrock substratum, 0 to 2 percent slopes	EcA	117.98	118.05	369
	ERIE	Millgrove loam, 0 to 1 percent slopes	MgA	118.05	118.14	459
	ERIE	Jimtown loam, 0 to 2 percent slopes	JtA	118.14	118.20	328
	ERIE	Millgrove loam, 0 to 1 percent slopes	MgA	118.20	118.28	401
	ERIE	Jimtown loam, 0 to 2 percent slopes	JtA	118.28	118.31	158
	ERIE	Colwood loam, 0 to 1 percent slopes	CmA	118.31	118.34	158
	ERIE	Jimtown loam, 0 to 2 percent slopes	JtA	118.34	118.43	506
	ERIE	Colwood loam, 0 to 1 percent slopes	CmA	118.43	118.57	708
	ERIE	Kibbie fine sandy loam, 0 to 2 percent slopes	KbA	118.57	118.58	77
	ERIE	Colwood loam, 0 to 1 percent slopes	CmA	118.58	118.62	203
	ERIE	Kibbie fine sandy loam, 0 to 2 percent slopes	KbA	118.62	118.65	183
	ERIE	Colwood silt loam, bedrock substratum, 0 to 1 percent slopes	CnA	118.65	118.72	326
	ERIE	Kibbie fine sandy loam, 0 to 2 percent slopes	KbA	118.72	118.75	161
	ERIE	Colwood silt loam, bedrock substratum, 0 to 1 percent slopes	CnA	118.75	118.76	48

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	ERIE	Kibbie fine sandy loam, 0 to 2 percent slopes	KbA	118.76	118.80	229
	ERIE	Colwood loam, 0 to 1 percent slopes	CmA	118.80	118.86	338
	ERIE	Hornell silty clay loam, 0 to 2 percent slopes	HsA	118.86	118.89	137
	ERIE	Colwood silt loam, bedrock substratum, 0 to 1 percent slopes	CnA	118.89	118.91	102
	ERIE	Jimtown loam, 0 to 2 percent slopes	JtA	118.91	118.96	250
	ERIE	Colwood silt loam, bedrock substratum, 0 to 1 percent slopes	CnA	118.96	119.01	266
	ERIE	Hornell silty clay loam, 0 to 2 percent slopes	HsA	119.01	119.12	625
	ERIE	Fries silty clay loam, 0 to 1 percent slopes	FrA	119.12	119.28	802
	ERIE	Hornell silty clay loam, 0 to 2 percent slopes	HsA	119.28	119.68	2145
	ERIE	Miner silt loam, bedrock substratum, 0 to 1 percent slopes	MsA	119.68	119.82	707
	ERIE	Pewamo silty clay loam, 0 to 1 percent slopes	PcA	119.82	120.09	1440
	ERIE	Miner silt loam, bedrock substratum, 0 to 1 percent slopes	MsA	120.09	120.09	29
	ERIE	Fries silty clay loam, 0 to 1 percent slopes	FrA	120.09	120.24	774
	ERIE	Hornell silty clay loam, 0 to 2 percent slopes	HsA	120.24	120.35	591
	ERIE	Kibbie fine sandy loam, 0 to 2 percent slopes	KbA	120.35	120.44	468
	ERIE	Hornell silty clay loam, 0 to 2 percent slopes	HsA	120.44	120.47	167
	ERIE	Miner silt loam, bedrock substratum, 0 to 1 percent slopes	MsA	120.47	120.51	202
	ERIE	Hornell silty clay loam, 0 to 2 percent slopes	HsA	120.51	120.61	522

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	ERIE	Miner silt loam, bedrock substratum, 0 to 1 percent slopes	MsA	120.61	120.69	445
	ERIE	Fries silty clay loam, 0 to 1 percent slopes	FrA	120.69	120.73	205
	ERIE	Hornell silty clay loam, 0 to 2 percent slopes	HsA	120.73	120.78	249
	ERIE	Fries silty clay loam, 0 to 1 percent slopes	FrA	120.78	120.82	224
	ERIE	Miner silt loam, bedrock substratum, 0 to 1 percent slopes	MsA	120.82	120.96	735
	ERIE	Kibbie fine sandy loam, 0 to 2 percent slopes	KbA	120.96	121.06	518
	ERIE	Bennington silt loam, 0 to 2 percent slopes	BgA	121.06	121.15	489
	ERIE	Kibbie fine sandy loam, 0 to 2 percent slopes	KbA	121.15	121.24	480
	ERIE	Mermill silty clay loam, 0 to 1 percent slopes	MeA	121.24	121.29	254
	ERIE	Kibbie fine sandy loam, 0 to 2 percent slopes	KbA	121.29	121.35	307
	ERIE	Rimer loamy fine sand, 0 to 2 percent slopes	RgA	121.35	121.36	35
	ERIE	Cardington silt loam, 2 to 6 percent slopes	CaB	121.36	121.37	85
	ERIE	Rawson sandy loam, 2 to 6 percent slopes	RcB	121.37	121.41	188
	ERIE	Cardington silt loam, 2 to 6 percent slopes	CaB	121.41	121.48	376
	ERIE	Bennington silt loam, 0 to 2 percent slopes	BgA	121.48	121.57	475
	ERIE	Joliet silt loam, 0 to 1 percent slopes	JuA	121.57	121.59	93
	ERIE	Holly silt loam, 0 to 1 percent slopes, occasionally flooded	HoA	121.59	121.61	142
	ERIE	Rawson sandy loam, 2 to 6 percent slopes	RcB	121.61	121.62	47
	ERIE	Spinks loamy fine sand, 0 to 6 percent slopes	SpB	121.62	121.72	526
	ERIE	Milton silt loam, 0 to 2 percent slopes	MnA	121.72	121.82	496

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	ERIE	Tuscola fine sandy loam, 0 to 2 percent slopes	TuA	121.82	121.89	397
	ERIE	Castalia very channery loam, 2 to 6 percent slopes	CcB	121.89	122.06	877
	ERIE	Ritchey loam, 0 to 2 percent slopes	RhA	122.06	122.25	1020
	ERIE	Milton silt loam, 0 to 2 percent slopes	MnA	122.25	122.56	1645
	ERIE	Dunbridge loamy sand, 2 to 6 percent slopes	DuB	122.56	122.57	44
	ERIE	Oshtemo loamy sand, 0 to 6 percent slopes	OsB	122.57	122.67	527
	ERIE	Millsdale silty clay loam, 0 to 1 percent slopes	MmA	122.67	122.98	1611
	ERIE	Randolph silt loam, 0 to 2 percent slopes	RaA	122.98	123.00	107
	ERIE	Millsdale silty clay loam, 0 to 1 percent slopes	MmA	123.00	123.17	911
	ERIE	Castalia very channery loam, 0 to 2 percent slopes	CcA	123.17	123.30	677
	ERIE	Dunbridge loamy sand, 0 to 2 percent slopes	DuA	123.30	123.38	430
	ERIE	Millsdale silty clay loam, 0 to 1 percent slopes	MmA	123.38	123.45	382
	ERIE	Castalia very channery loam, 0 to 2 percent slopes	CcA	123.45	123.50	260
	ERIE	Millsdale silty clay loam, 0 to 1 percent slopes	MmA	123.50	123.60	537
	ERIE	Randolph silt loam, 0 to 2 percent slopes	RaA	123.60	123.63	127
	ERIE	Castalia very channery loam, 0 to 2 percent slopes	CcA	123.63	123.68	289
	ERIE	Millsdale silty clay loam, 0 to 1 percent slopes	MmA	123.68	123.82	743
	ERIE	Joliet silt loam, 0 to 1 percent slopes	JuA	123.82	124.00	948
	ERIE	Castalia very channery loam, 2 to 6 percent slopes	CcB	124.00	124.02	119
	ERIE	Ritchey loam, 0 to 2 percent slopes	RhA	124.02	124.09	368

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	ERIE	Castalia very channery loam, 0 to 2 percent slopes	CcA	124.09	124.36	1431
	ERIE	Ritchey loam, 0 to 2 percent slopes	RhA	124.36	124.47	545
	ERIE	Tuscola fine sandy loam, 2 to 6 percent slopes	TuB	124.47	124.51	243
	ERIE	Kibbie fine sandy loam, 0 to 2 percent slopes	KbA	124.51	124.69	931
	ERIE	Tuscola fine sandy loam, 2 to 6 percent slopes	TuB	124.69	124.71	119
	ERIE	Colwood loam, 0 to 1 percent slopes	CmA	124.71	124.75	204
	ERIE	Kibbie fine sandy loam, 0 to 2 percent slopes	KbA	124.75	124.80	237
	ERIE	Colwood loam, 0 to 1 percent slopes	CmA	124.80	124.89	517
	ERIE	Kibbie fine sandy loam, 0 to 2 percent slopes	KbA	124.89	124.91	88
	ERIE	Mermill silty clay loam, 0 to 1 percent slopes	MeA	124.91	124.94	141
	ERIE	Kibbie fine sandy loam, 0 to 2 percent slopes	KbA	124.94	125.06	629
	ERIE	Colwood loam, 0 to 1 percent slopes	CmA	125.06	125.14	431
	ERIE	Kibbie fine sandy loam, 0 to 2 percent slopes	KbA	125.14	125.21	370
	ERIE	Colwood loam, 0 to 1 percent slopes	CmA	125.21	125.22	42
	ERIE	Kibbie fine sandy loam, 0 to 2 percent slopes	KbA	125.22	125.24	149
	ERIE	Colwood loam, 0 to 1 percent slopes	CmA	125.24	125.31	326
	ERIE	Bixler loamy fine sand, 0 to 2 percent slopes	BkA	125.31	125.47	852
	ERIE	Kibbie fine sandy loam, 0 to 2 percent slopes	KbA	125.47	125.55	443
	ERIE	Plumbrook fine sandy loam, 0 to 2 percent slopes	PmA	125.55	125.61	309
	ERIE	Kibbie fine sandy loam, 0 to 2 percent slopes	KbA	125.61	125.73	612

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	ERIE	Bixler loamy fine sand, 0 to 2 percent slopes	BkA	125.73	125.77	233
	ERIE	Plumbrook fine sandy loam, 0 to 2 percent slopes	PmA	125.77	125.87	514
	ERIE	Millsdale silty clay loam, 0 to 1 percent slopes	MmA	125.87	125.89	149
	ERIE	Randolph silt loam, 0 to 2 percent slopes	RaA	125.89	125.95	297
	ERIE	Millsdale silty clay loam, 0 to 1 percent slopes	MmA	125.95	125.99	189
	ERIE	Milton silt loam, 0 to 2 percent slopes	MnA	125.99	126.08	516
	ERIE	Millsdale silty clay loam, 0 to 1 percent slopes	MmA	126.08	126.11	134
	ERIE	Ritchey loam, 0 to 2 percent slopes	RhA	126.11	126.14	184
	ERIE	Castalia very channery loam, 0 to 2 percent slopes	CcA	126.14	126.25	567
	ERIE	Milton silt loam, 2 to 6 percent slopes	MnB	126.25	126.28	160
	ERIE	Milton silt loam, 0 to 2 percent slopes	MnA	126.28	126.43	798
	ERIE	Dunbridge loamy sand, 0 to 2 percent slopes	DuA	126.43	126.50	363
	ERIE	Ritchey loam, 6 to 12 percent slopes	RhC	126.50	126.52	114
	ERIE	Dunbridge loamy sand, 2 to 6 percent slopes	DuB	126.52	126.60	407
	ERIE	Rawson sandy loam, 0 to 2 percent slopes	RcA	126.60	126.65	268
	ERIE	Milton silt loam, 2 to 6 percent slopes	MnB	126.65	126.72	345
	ERIE	Ogontz silt loam, 2 to 6 percent slopes	OhB	126.72	126.78	325
	ERIE	Kibbie fine sandy loam, 0 to 2 percent slopes	KbA	126.78	127.10	1693
	ERIE	Ogontz silt loam, 2 to 6 percent slopes	OhB	127.10	127.14	230
	ERIE	Glenford silt loam, 2 to 6 percent slopes	GtB	127.14	127.15	18

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	SANDUSKY	Glenford silt loam, 2 to 6 percent slopes	GtB	127.15	127.17	126
	SANDUSKY	Kibbie fine sandy loam, 0 to 2 percent slopes	KbA	127.17	127.32	774
	SANDUSKY	Rimer loamy fine sand, 1 to 4 percent slopes	RoB	127.32	127.41	481
	SANDUSKY	Haskins sandy loam, 1 to 4 percent slopes	HaB	127.41	127.68	1460
	SANDUSKY	Mermill loam	Mo	127.68	127.71	112
	SANDUSKY	Haskins sandy loam, 1 to 4 percent slopes	HaB	127.71	127.76	290
	SANDUSKY	Mermill loam	Mo	127.76	127.84	440
	SANDUSKY	Haskins sandy loam, 1 to 4 percent slopes	HaB	127.84	127.86	64
	SANDUSKY	Kibbie fine sandy loam, 0 to 2 percent slopes	KbA	127.86	128.26	2142
	SANDUSKY	Belmore loam, 2 to 6 percent slopes	BaB	128.26	128.32	305
	SANDUSKY	Kibbie fine sandy loam, 0 to 2 percent slopes	KbA	128.32	128.37	259
	SANDUSKY	Haskins sandy loam, 1 to 4 percent slopes	HaB	128.37	128.45	444
	SANDUSKY	Belmore loam, 2 to 6 percent slopes	BaB	128.45	128.61	824
	SANDUSKY	Haskins sandy loam, 1 to 4 percent slopes	HaB	128.61	128.67	323
	SANDUSKY	Mermill loam	Mo	128.67	128.75	449
	SANDUSKY	Haskins sandy loam, 1 to 4 percent slopes	HaB	128.75	128.84	476
	SANDUSKY	Spinks fine sand, 2 to 6 percent slopes	SoB	128.84	129.05	1065
	SANDUSKY	Belmore loam, 2 to 6 percent slopes	BaB	129.05	129.21	887
	SANDUSKY	Kibbie fine sandy loam, 0 to 2 percent slopes	KbA	129.21	129.36	773
	SANDUSKY	Lenawee silty clay loam	Le	129.36	129.51	762
	SANDUSKY	Kibbie fine sandy loam, 0 to 2 percent slopes	KbA	129.51	129.51	36
	SANDUSKY	Lenawee silty clay loam	Le	129.51	129.75	1253

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	SANDUSKY	Haskins sandy loam, 1 to 4 percent slopes	HaB	129.75	129.82	362
	SANDUSKY	Lenawee silty clay loam	Le	129.82	129.87	289
	SANDUSKY	Kibbie fine sandy loam, 0 to 2 percent slopes	KbA	129.87	130.02	784
	SANDUSKY	Haskins sandy loam, 1 to 4 percent slopes	HaB	130.02	130.09	371
	SANDUSKY	Del Rey silt loam, 0 to 2 percent slopes	DeA	130.09	130.16	349
	SANDUSKY	Hoytville clay loam, 0 to 1 percent slopes	HoA	130.16	130.33	910
	SANDUSKY	Nappanee silt loam, 0 to 3 percent slopes	NpA	130.33	130.36	158
	SANDUSKY	Hoytville clay loam, 0 to 1 percent slopes	HoA	130.36	130.43	371
	SANDUSKY	Glynwood silt loam, 2 to 6 percent slopes	GwB	130.43	130.45	126
	SANDUSKY	Hoytville clay loam, 0 to 1 percent slopes	HoA	130.45	130.95	2621
	SANDUSKY	Glynwood silt loam, 2 to 6 percent slopes	GwB	130.95	131.04	460
	SANDUSKY	Nappanee silt loam, 0 to 3 percent slopes	NpA	131.04	131.22	940
	SANDUSKY	Hoytville clay loam, 0 to 1 percent slopes	HoA	131.22	131.50	1490
	SANDUSKY	Mermill loam	Mo	131.50	131.52	137
	SANDUSKY	Glynwood silt loam, 2 to 6 percent slopes	GwB	131.52	131.62	513
	SANDUSKY	Colwood fine sandy loam	Co	131.62	131.73	583
	SANDUSKY	Glynwood silt loam, 2 to 6 percent slopes	GwB	131.73	131.79	321
	SANDUSKY	Hoytville clay loam, 0 to 1 percent slopes	HoA	131.79	131.90	574
	SANDUSKY	Nappanee silt loam, 0 to 3 percent slopes	NpA	131.90	131.97	357
	SANDUSKY	Hoytville clay loam, 0 to 1 percent slopes	HoA	131.97	132.01	244
	SANDUSKY	Nappanee silt loam, 0 to 3 percent slopes	NpA	132.01	132.06	254

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	SANDUSKY	Kibbie fine sandy loam, 0 to 2 percent slopes	KbA	132.06	132.11	269
	SANDUSKY	Nappanee silt loam, 0 to 3 percent slopes	NpA	132.11	132.17	283
	SANDUSKY	Kibbie fine sandy loam, 0 to 2 percent slopes	KbA	132.17	132.25	414
	SANDUSKY	Hoytville clay loam, 0 to 1 percent slopes	HoA	132.25	132.31	367
	SANDUSKY	Nappanee silt loam, 0 to 3 percent slopes	NpA	132.31	132.37	295
	SANDUSKY	Rimer loamy fine sand, 1 to 4 percent slopes	RoB	132.37	132.64	1400
	SANDUSKY	Hoytville clay loam, 0 to 1 percent slopes	HoA	132.64	132.70	336
	SANDUSKY	Haskins sandy loam, 1 to 4 percent slopes	HaB	132.70	132.81	586
	SANDUSKY	Del Rey silt loam, 0 to 2 percent slopes	DeA	132.81	132.85	200
	SANDUSKY	Haskins sandy loam, 1 to 4 percent slopes	HaB	132.85	132.92	353
	SANDUSKY	Del Rey silt loam, 0 to 2 percent slopes	DeA	132.92	132.94	140
	SANDUSKY	Lenawee silty clay loam	Le	132.94	132.98	205
	SANDUSKY	Del Rey silt loam, 0 to 2 percent slopes	DeA	132.98	133.04	306
	SANDUSKY	Lenawee silty clay loam	Le	133.04	133.17	683
	SANDUSKY	Del Rey silt loam, 0 to 2 percent slopes	DeA	133.17	133.36	994
	SANDUSKY	Haskins sandy loam, 1 to 4 percent slopes	HaB	133.36	133.40	207
	SANDUSKY	Toledo silty clay	To	133.40	133.43	161
	SANDUSKY	Del Rey silt loam, 0 to 2 percent slopes	DeA	133.43	133.52	478
	SANDUSKY	Toledo silty clay	To	133.52	133.68	839
	SANDUSKY	Del Rey silt loam, 0 to 2 percent slopes	DeA	133.68	134.02	1800
	SANDUSKY	Toledo silty clay	To	134.02	134.06	217
	SANDUSKY	Del Rey silt loam, 0 to 2 percent slopes	DeA	134.06	134.09	191

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	SANDUSKY	Toledo silty clay	To	134.09	134.13	211
	SANDUSKY	Del Rey silt loam, 0 to 2 percent slopes	DeA	134.13	134.19	303
	SANDUSKY	Glenford silt loam, 2 to 6 percent slopes	GtB	134.19	134.26	371
	SANDUSKY	Del Rey silt loam, 0 to 2 percent slopes	DeA	134.26	134.33	369
	SANDUSKY	Lenawee silty clay loam	Le	134.33	134.43	519
	SANDUSKY	Del Rey silt loam, 0 to 2 percent slopes	DeA	134.43	134.80	1972
	SANDUSKY	Lenawee silty clay loam	Le	134.80	134.94	721
	SANDUSKY	Del Rey silt loam, 0 to 2 percent slopes	DeA	134.94	135.03	465
	SANDUSKY	Lenawee silty clay loam	Le	135.03	135.09	318
	SANDUSKY	Del Rey silt loam, 0 to 2 percent slopes	DeA	135.09	135.13	240
	SANDUSKY	Lenawee silty clay loam	Le	135.13	135.23	490
	SANDUSKY	Del Rey silt loam, 0 to 2 percent slopes	DeA	135.23	135.37	766
	SANDUSKY	Glenford silt loam, 2 to 6 percent slopes	GtB	135.37	135.44	356
	SANDUSKY	Shoals silt loam, frequently flooded	Sh	135.44	135.51	391
	SANDUSKY	Glenford silt loam, 2 to 6 percent slopes	GtB	135.51	135.56	227
	SANDUSKY	Del Rey silt loam, 0 to 2 percent slopes	DeA	135.56	135.63	367
	SANDUSKY	Lenawee silty clay loam	Le	135.63	135.63	25
	SANDUSKY	Del Rey silt loam, 0 to 2 percent slopes	DeA	135.63	135.84	1126
	SANDUSKY	Lenawee silty clay loam	Le	135.84	136.08	1275
	SANDUSKY	Glenford silt loam, 2 to 6 percent slopes	GtB	136.08	136.09	28
	SANDUSKY	Del Rey silt loam, 0 to 2 percent slopes	DeA	136.09	136.19	531
	SANDUSKY	Glenford silt loam, 2 to 6 percent slopes	GtB	136.19	136.19	13
	SANDUSKY	Lenawee silty clay loam	Le	136.19	136.43	1243

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	SANDUSKY	Del Rey silt loam, 0 to 2 percent slopes	DeA	136.43	136.54	592
	SANDUSKY	Lenawee silty clay loam	Le	136.54	136.60	334
	SANDUSKY	Del Rey silt loam, 0 to 2 percent slopes	DeA	136.60	136.65	233
	SANDUSKY	Lenawee silty clay loam	Le	136.65	136.73	451
	SANDUSKY	Glenford silt loam, 2 to 6 percent slopes	GtB	136.73	136.77	205
	SANDUSKY	Del Rey silt loam, 0 to 2 percent slopes	DeA	136.77	136.94	903
	SANDUSKY	Toledo silty clay	To	136.94	137.05	570
	SANDUSKY	Glenford silt loam, 2 to 6 percent slopes	GtB	137.05	137.14	477
	SANDUSKY	Shoals silt loam, frequently flooded	Sh	137.14	137.25	584
	SANDUSKY	Dixboro-Kibbie complex, 0 to 2 percent slopes	DkA	137.25	137.49	1241
	SANDUSKY	Del Rey silt loam, 0 to 2 percent slopes	DeA	137.49	137.56	371
	SANDUSKY	Lenawee silty clay loam	Le	137.56	138.42	4566
	SANDUSKY	Del Rey silt loam, 0 to 2 percent slopes	DeA	138.42	138.49	344
	SANDUSKY	Lenawee silty clay loam	Le	138.49	139.13	3370
	SANDUSKY	Rimer loamy fine sand, 1 to 4 percent slopes	RoB	139.13	139.20	374
	SANDUSKY	Glenford silt loam, 2 to 6 percent slopes	GtB	139.20	139.26	318
	SANDUSKY	Colwood fine sandy loam	Co	139.26	139.39	683
	SANDUSKY	Glenford silt loam, 2 to 6 percent slopes	GtB	139.39	139.43	246
	SANDUSKY	Del Rey silt loam, 0 to 2 percent slopes	DeA	139.43	139.48	245
	SANDUSKY	Lenawee silty clay loam	Le	139.48	139.51	186
	SANDUSKY	Del Rey silt loam, 0 to 2 percent slopes	DeA	139.51	139.59	426
	SANDUSKY	Lenawee silty clay loam	Le	139.59	140.15	2920
	SANDUSKY	Del Rey silt loam, 0 to 2 percent slopes	DeA	140.15	140.19	224
	SANDUSKY	Lenawee silty clay loam	Le	140.19	140.21	123

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	SANDUSKY	Del Rey silt loam, 0 to 2 percent slopes	DeA	140.21	140.24	123
	SANDUSKY	Lenawee silty clay loam	Le	140.24	140.26	142
	SANDUSKY	Del Rey silt loam, 0 to 2 percent slopes	DeA	140.26	140.33	357
	SANDUSKY	Lenawee silty clay loam	Le	140.33	140.36	178
	SANDUSKY	Del Rey silt loam, 0 to 2 percent slopes	DeA	140.36	140.61	1302
	SANDUSKY	Glenford silt loam, 2 to 6 percent slopes	GtB	140.61	140.69	416
	SANDUSKY	Saylesville silty clay loam, 6 to 12 percent slopes, eroded	SbC2	140.69	140.77	436
	SANDUSKY	Glenford silt loam, 2 to 6 percent slopes	GtB	140.77	140.82	270
	SANDUSKY	Mentor silt loam, 1 to 4 percent slopes	MeB	140.82	141.18	1879
	SANDUSKY	Toledo silty clay loam, ponded	Tp	141.18	141.20	119
	SANDUSKY	Rossburg silt loam, occasionally flooded	Rs	141.20	141.23	169
	SANDUSKY	Water	W	141.23	141.32	430
	SANDUSKY	Mentor silt loam, 1 to 4 percent slopes	MeB	141.32	141.45	691
	SANDUSKY	Toledo silty clay loam, ponded	Tp	141.45	141.48	189
	SANDUSKY	Mentor silt loam, 1 to 4 percent slopes	MeB	141.48	141.55	376
	SANDUSKY	Del Rey silt loam, 0 to 2 percent slopes	DeA	141.55	141.70	788
	SANDUSKY	Lenawee silty clay loam	Le	141.70	141.73	125
	SANDUSKY	Del Rey silt loam, 0 to 2 percent slopes	DeA	141.73	141.90	915
	SANDUSKY	Lenawee silty clay loam	Le	141.90	141.93	182
	SANDUSKY	Del Rey silt loam, 0 to 2 percent slopes	DeA	141.93	142.04	535
	SANDUSKY	Aquents, nearly level	An	142.04	142.13	476
	SANDUSKY	Lenawee silty clay loam	Le	142.13	142.54	2173
	SANDUSKY	Del Rey silt loam, 0 to 2 percent slopes	DeA	142.54	142.60	351
	SANDUSKY	Lenawee silty clay loam	Le	142.60	143.51	4760

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State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	SANDUSKY	Del Rey silt loam, 0 to 2 percent slopes	DeA	143.51	143.54	197
	SANDUSKY	Lenawee silty clay loam	Le	143.54	143.69	759
	SANDUSKY	Kibbie fine sandy loam, 0 to 2 percent slopes	KbA	143.69	143.77	454
	SANDUSKY	Colwood fine sandy loam	Co	143.77	144.03	1347
	SANDUSKY	Kibbie fine sandy loam, 0 to 2 percent slopes	KbA	144.03	144.25	1194
	SANDUSKY	Glenford silt loam, 2 to 6 percent slopes	GtB	144.25	144.29	213
	SANDUSKY	Shoals silt loam, frequently flooded	Sh	144.29	144.33	188
	SANDUSKY	Glenford silt loam, 2 to 6 percent slopes	GtB	144.33	144.47	767
	SANDUSKY	Dixboro-Kibbie complex, 0 to 2 percent slopes	DkA	144.47	144.70	1210
	SANDUSKY	Haskins sandy loam, 1 to 4 percent slopes	HaB	144.70	144.97	1429
	SANDUSKY	Millsdale silty clay loam	Ms	144.97	145.05	423
	SANDUSKY	Hoytville clay loam, 0 to 1 percent slopes	HoA	145.05	145.13	407
	SANDUSKY	Millsdale silty clay loam	Ms	145.13	145.15	121
	SANDUSKY	Hoytville clay loam, 0 to 1 percent slopes	HoA	145.15	146.23	5682
	SANDUSKY	Nappanee silt loam, 0 to 3 percent slopes	NpA	146.23	146.32	455
	SANDUSKY	Hoytville clay loam, 0 to 1 percent slopes	HoA	146.32	146.34	119
	SANDUSKY	Nappanee silt loam, 0 to 3 percent slopes	NpA	146.34	146.38	236
	SANDUSKY	Hoytville clay loam, 0 to 1 percent slopes	HoA	146.38	146.44	311
	SANDUSKY	Millsdale silty clay loam	Ms	146.44	146.65	1067
	SANDUSKY	Nappanee silt loam, 0 to 3 percent slopes	NpA	146.65	146.80	828
	SANDUSKY	Hoytville clay loam, 0 to 1 percent slopes	HoA	146.80	146.92	612
	SANDUSKY	Nappanee silt loam, 0 to 3 percent slopes	NpA	146.92	146.94	94

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	SANDUSKY	Hoytville clay loam, 0 to 1 percent slopes	HoA	146.94	147.03	506
	SANDUSKY	Nappanee silt loam, 0 to 3 percent slopes	NpA	147.03	147.16	655
	SANDUSKY	Hoytville clay loam, 0 to 1 percent slopes	HoA	147.16	147.36	1067
	SANDUSKY	Nappanee silt loam, 0 to 3 percent slopes	NpA	147.36	147.47	617
	SANDUSKY	Hoytville clay loam, 0 to 1 percent slopes	HoA	147.47	148.18	3718
	SANDUSKY	Glynwood silt loam, 2 to 6 percent slopes	GwB	148.18	148.27	501
	SANDUSKY	Shoals silt loam, frequently flooded	Sh	148.27	148.41	725
	SANDUSKY	Glynwood silt loam, 2 to 6 percent slopes	GwB	148.41	148.47	292
	SANDUSKY	Haskins sandy loam, 1 to 4 percent slopes	HaB	148.47	148.51	243
	SANDUSKY	Mermill loam	Mo	148.51	148.60	444
	SANDUSKY	Haskins sandy loam, 1 to 4 percent slopes	HaB	148.60	149.02	2210
	SANDUSKY	Nappanee silt loam, 0 to 3 percent slopes	NpA	149.02	149.32	1624
	SANDUSKY	Haskins sandy loam, 1 to 4 percent slopes	HaB	149.32	149.49	868
	SANDUSKY	Hoytville clay loam, 0 to 1 percent slopes	HoA	149.49	149.93	2321
	SANDUSKY	Nappanee silt loam, 0 to 3 percent slopes	NpA	149.93	150.00	402
	SANDUSKY	Hoytville clay loam, 0 to 1 percent slopes	HoA	150.00	150.02	95
	SANDUSKY	Nappanee silt loam, 0 to 3 percent slopes	NpA	150.02	150.06	208
	SANDUSKY	Hoytville clay loam, 0 to 1 percent slopes	HoA	150.06	150.54	2528
	SANDUSKY	Millsdale silty clay loam	Ms	150.54	150.61	359
	SANDUSKY	Hoytville clay loam, 0 to 1 percent slopes	HoA	150.61	150.76	808
	SANDUSKY	Haskins sandy loam, 1 to 4 percent slopes	HaB	150.76	150.79	146

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Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	SANDUSKY	Hoytville clay loam, 0 to 1 percent slopes	HoA	150.79	151.04	1324
	SANDUSKY	Millsdale silty clay loam	Ms	151.04	151.15	608
	SANDUSKY	Hoytville clay loam, 0 to 1 percent slopes	HoA	151.15	151.21	297
	SANDUSKY	Millsdale silty clay loam	Ms	151.21	151.26	244
	SANDUSKY	Castalia very stony loam, 1 to 6 percent slopes	ChB	151.26	151.37	576
	SANDUSKY	Hoytville clay loam, 0 to 1 percent slopes	HoA	151.37	151.55	990
	SANDUSKY	Haskins sandy loam, 1 to 4 percent slopes	HaB	151.55	151.65	515
	SANDUSKY	Hoytville clay loam, 0 to 1 percent slopes	HoA	151.65	151.80	788
	SANDUSKY	Haskins sandy loam, 1 to 4 percent slopes	HaB	151.80	151.84	235
	SANDUSKY	Hoytville clay loam, 0 to 1 percent slopes	HoA	151.84	151.87	154
	SANDUSKY	Haskins sandy loam, 1 to 4 percent slopes	HaB	151.87	151.91	202
	SANDUSKY	Hoytville clay loam, 0 to 1 percent slopes	HoA	151.91	152.33	2227
	SANDUSKY	Millsdale silty clay loam	Ms	152.33	152.39	279
	SANDUSKY	Castalia very stony loam, 1 to 6 percent slopes	ChB	152.39	152.56	921
	SANDUSKY	Millsdale silty clay loam	Ms	152.56	152.64	444
	SANDUSKY	Hoytville clay loam, 0 to 1 percent slopes	HoA	152.64	152.81	887
	SANDUSKY	Millsdale silty clay loam	Ms	152.81	152.92	560
	SANDUSKY	Dunbridge sandy loam, 1 to 4 percent slopes	DuB	152.92	152.98	300
	SANDUSKY	Millsdale silty clay loam	Ms	152.98	153.03	312
	SANDUSKY	Dunbridge sandy loam, 1 to 4 percent slopes	DuB	153.03	153.27	1240
	SANDUSKY	Millsdale silty clay loam	Ms	153.27	153.30	153
	SANDUSKY	Nappanee silt loam, 0 to 3 percent slopes	NpA	153.30	153.32	134
	SANDUSKY	Mermill loam	Mo	153.32	153.47	800

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	SANDUSKY	Nappanee silt loam, 0 to 3 percent slopes	NpA	153.47	153.52	245
	SANDUSKY	Shoals silt loam, frequently flooded	Sh	153.52	153.63	577
	SANDUSKY	Glynwood silt loam, 2 to 6 percent slopes	GwB	153.63	153.69	302
	SANDUSKY	Hoytville clay loam, 0 to 1 percent slopes	HoA	153.69	153.86	907
	SANDUSKY	Nappanee silt loam, 0 to 3 percent slopes	NpA	153.86	153.92	304
	SANDUSKY	Hoytville clay loam, 0 to 1 percent slopes	HoA	153.92	154.01	517
	SANDUSKY	Nappanee silt loam, 0 to 3 percent slopes	NpA	154.01	154.14	664
	SANDUSKY	Hoytville clay loam, 0 to 1 percent slopes	HoA	154.14	154.37	1222
	SANDUSKY	Millsdale silty clay loam	Ms	154.37	154.48	546
	SANDUSKY	Castalia very stony loam, 1 to 6 percent slopes	ChB	154.48	154.64	887
	SANDUSKY	Millsdale silty clay loam	Ms	154.64	154.73	445
	SANDUSKY	Hoytville clay loam, 0 to 1 percent slopes	HoA	154.73	155.13	2108
	SANDUSKY	Nappanee silt loam, 0 to 3 percent slopes	NpA	155.13	155.58	2417
	SANDUSKY	Hoytville clay loam, 0 to 1 percent slopes	HoA	155.58	156.47	4688
	SANDUSKY	Nappanee silt loam, 0 to 3 percent slopes	NpA	156.47	156.66	982
	SANDUSKY	Hoytville clay loam, 0 to 1 percent slopes	HoA	156.66	156.79	712
	SANDUSKY	Nappanee silt loam, 0 to 3 percent slopes	NpA	156.79	156.83	184
	SANDUSKY	Hoytville clay loam, 0 to 1 percent slopes	HoA	156.83	157.31	2530
	SANDUSKY	Nappanee silt loam, 0 to 3 percent slopes	NpA	157.31	157.37	330
	SANDUSKY	Haskins sandy loam, 1 to 4 percent slopes	HaB	157.37	157.41	230
	SANDUSKY	Water	W	157.41	157.44	119

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	SANDUSKY	Rossburg silt loam, occasionally flooded	Rs	157.44	157.47	192
	SANDUSKY	Haskins sandy loam, 1 to 4 percent slopes	HaB	157.47	157.51	199
	SANDUSKY	Mermill loam	Mo	157.51	157.59	414
	SANDUSKY	Nappanee silt loam, 0 to 3 percent slopes	NpA	157.59	157.70	614
	SANDUSKY	Lenawee silty clay loam	Le	157.70	157.80	520
	SANDUSKY	Hoytville clay loam, 0 to 1 percent slopes	HoA	157.80	158.03	1219
	SANDUSKY	Mermill loam	Mo	158.03	158.08	243
	SANDUSKY	Hoytville clay loam, 0 to 1 percent slopes	HoA	158.08	158.20	634
	SANDUSKY	Lenawee silty clay loam	Le	158.20	158.38	956
	SANDUSKY	Millsdale silty clay loam	Ms	158.38	158.40	103
	SANDUSKY	Castalia very stony loam, 1 to 6 percent slopes	ChB	158.40	158.43	143
	SANDUSKY	Millsdale silty clay loam	Ms	158.43	158.46	179
	SANDUSKY	Hoytville clay loam, 0 to 1 percent slopes	HoA	158.46	158.60	741
	SANDUSKY	Nappanee silt loam, 0 to 3 percent slopes	NpA	158.60	158.62	98
	SANDUSKY	Hoytville clay loam, 0 to 1 percent slopes	HoA	158.62	158.66	194
	WOOD	Hoytville clay loam, 0 to 1 percent slopes	HoA	158.66	158.66	9
	WOOD	Hoytville clay loam, 0 to 1 percent slopes	HoA	158.66	158.71	265
	WOOD	Nappanee loam, 0 to 2 percent slopes	NnA	158.71	158.72	76
	WOOD	Sloan silt loam, 0 to 1 percent slopes, frequently flooded	SnA	158.72	158.76	202
	WOOD	Hoytville clay loam, 0 to 1 percent slopes	HoA	158.76	158.93	871
	WOOD	Millsdale silty clay loam, 0 to 1 percent slopes	MhA	158.93	158.98	279
	WOOD	Castalia-Marblehead complex, very stony, 0 to 6 percent slopes	CbB	158.98	159.44	2453

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	WOOD	Randolph loam, 0 to 2 percent slopes	RbA	159.44	159.48	177
	WOOD	Nappanee loam, 0 to 2 percent slopes	NnA	159.48	159.52	232
	WOOD	Seward and Ottokee, till substratum, loamy fine sands, 0 to 2 percent slopes	SdA	159.52	159.54	121
	WOOD	Nappanee loam, 0 to 2 percent slopes	NnA	159.54	159.55	4
	WOOD	Hoytville clay loam, 0 to 1 percent slopes	HoA	159.55	159.58	208
	WOOD	Millsdale silty clay loam, 0 to 1 percent slopes	MhA	159.58	159.65	367
	WOOD	Castalia-Marblehead complex, very stony, 0 to 6 percent slopes	CbB	159.65	159.78	671
	WOOD	Randolph loam, 0 to 2 percent slopes	RbA	159.78	159.89	575
	WOOD	Millsdale silty clay loam, 0 to 1 percent slopes	MhA	159.89	159.90	55
	WOOD	Castalia-Marblehead complex, very stony, 0 to 6 percent slopes	CbB	159.90	159.95	249
	WOOD	Randolph loam, 0 to 2 percent slopes	RbA	159.95	160.02	374
	WOOD	Millsdale silty clay loam, 0 to 1 percent slopes	MhA	160.02	160.04	139
	WOOD	Hoytville clay loam, 0 to 1 percent slopes	HoA	160.04	160.85	4244
	WOOD	Millsdale silty clay loam, 0 to 1 percent slopes	MhA	160.85	160.93	425
	WOOD	Castalia-Marblehead complex, very stony, 0 to 6 percent slopes	CbB	160.93	161.00	361
	WOOD	Joliet silty clay loam, 0 to 1 percent slopes	JoA	161.00	161.08	415
	WOOD	Castalia-Marblehead complex, very stony, 0 to 6 percent slopes	CbB	161.08	161.08	6
	WOOD	Millsdale silty clay loam, 0 to 1 percent slopes	MhA	161.08	161.15	384
	WOOD	Hoytville clay loam, 0 to 1 percent slopes	HoA	161.15	161.52	1977
	WOOD	Mermill-Aurand complex, 0 to 1 percent slopes	MfA	161.52	161.69	850

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	WOOD	Hoytville clay loam, 0 to 1 percent slopes	HoA	161.69	162.13	2340
	WOOD	Nappanee loam, 2 to 6 percent slopes	NnB	162.13	162.16	148
	WOOD	Sloan silty clay loam, 0 to 1 percent slopes, frequently flooded	SpA	162.16	162.24	428
	WOOD	Nappanee loam, 2 to 6 percent slopes	NnB	162.24	162.26	133
	WOOD	Hoytville clay loam, 0 to 1 percent slopes	HoA	162.26	163.79	8087
	WOOD	Aurand loam, 0 to 2 percent slopes	AnA	163.79	163.88	431
	WOOD	Hoytville clay loam, 0 to 1 percent slopes	HoA	163.88	164.04	846
	WOOD	Nappanee sandy loam, 0 to 2 percent slopes	NmA	164.04	164.10	358
	WOOD	Hoytville clay loam, 0 to 1 percent slopes	HoA	164.10	164.14	177
	WOOD	Nappanee loam, 0 to 2 percent slopes	NnA	164.14	164.18	240
	WOOD	Hoytville clay loam, 0 to 1 percent slopes	HoA	164.18	164.19	54
	WOOD	Nappanee loam, 0 to 2 percent slopes	NnA	164.19	164.26	337
	WOOD	Hoytville clay loam, 0 to 1 percent slopes	HoA	164.26	164.29	161
	WOOD	Nappanee loam, 0 to 2 percent slopes	NnA	164.29	164.30	71
	WOOD	Nappanee sandy loam, 0 to 2 percent slopes	NmA	164.30	164.44	747
	WOOD	Nappanee loam, 0 to 2 percent slopes	NnA	164.44	164.49	245
	WOOD	Hoytville clay loam, 0 to 1 percent slopes	HoA	164.49	164.73	1254
	WOOD	Nappanee loam, 0 to 2 percent slopes	NnA	164.73	164.75	141
	WOOD	Hoytville clay loam, 0 to 1 percent slopes	HoA	164.75	164.78	154
	WOOD	Nappanee loam, 0 to 2 percent slopes	NnA	164.78	164.85	379

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	WOOD	Hoytville clay loam, 0 to 1 percent slopes	HoA	164.85	167.92	16180
	WOOD	Seward and Ottokee, till substratum, loamy fine sands, 0 to 2 percent slopes	SdA	167.92	168.05	691
	WOOD	Hoytville clay loam, 0 to 1 percent slopes	HoA	168.05	168.09	216
	WOOD	Millsdale silty clay loam, 0 to 1 percent slopes	MhA	168.09	168.11	123
	WOOD	Randolph loam, 0 to 2 percent slopes	RbA	168.11	168.15	180
	WOOD	Dunbridge-Spinks, deep to limestone, loamy fine sands, 2 to 6 percent slopes	DsB	168.15	168.40	1312
	WOOD	Castalia-Marblehead complex, very stony, 0 to 6 percent slopes	CbB	168.40	168.41	71
	WOOD	Randolph loam, 0 to 2 percent slopes	RbA	168.41	168.51	542
	WOOD	Castalia-Marblehead complex, very stony, 0 to 6 percent slopes	CbB	168.51	168.62	585
	WOOD	Randolph loam, 0 to 2 percent slopes	RbA	168.62	168.69	336
	WOOD	Hoytville clay loam, 0 to 1 percent slopes	HoA	168.69	168.97	1491
	WOOD	Aurand loam, 0 to 2 percent slopes	AnA	168.97	169.01	215
	WOOD	Aurand fine sandy loam, 0 to 2 percent slopes	AmA	169.01	169.12	567
	WOOD	Nappanee loam, 0 to 2 percent slopes	NnA	169.12	169.16	240
	WOOD	Hoytville clay loam, 0 to 1 percent slopes	HoA	169.16	170.61	7650
	WOOD	Mermill-Aurand complex, 0 to 1 percent slopes	MfA	170.61	171.18	3009
	WOOD	Hoytville clay loam, 0 to 1 percent slopes	HoA	171.18	171.88	3702
	WOOD	Mermill-Aurand complex, 0 to 1 percent slopes	MfA	171.88	171.97	444
	WOOD	Hoytville clay loam, 0 to 1 percent slopes	HoA	171.97	172.86	4719
	WOOD	Mermill-Aurand complex, 0 to 1 percent slopes	MfA	172.86	173.21	1842

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	WOOD	Hoytville clay loam, 0 to 1 percent slopes	HoA	173.21	173.86	3447
	WOOD	Mermill-Aurand complex, 0 to 1 percent slopes	MfA	173.86	173.90	227
	WOOD	Hoytville clay loam, 0 to 1 percent slopes	HoA	173.90	174.55	3411
	WOOD	Aurand loam, 0 to 2 percent slopes	AnA	174.55	174.61	296
	WOOD	Nappanee loam, 2 to 6 percent slopes	NnB	174.61	174.66	272
	WOOD	Hoytville clay loam, 0 to 1 percent slopes	HoA	174.66	174.72	342
	WOOD	Aurand loam, 0 to 2 percent slopes	AnA	174.72	174.75	167
	WOOD	Hoytville clay loam, 0 to 1 percent slopes	HoA	174.75	174.79	170
	WOOD	Nappanee silty clay loam, 2 to 6 percent slopes, eroded	NpB2	174.79	174.81	117
	WOOD	Hoytville clay loam, 0 to 1 percent slopes	HoA	174.81	175.30	2567
	WOOD	Aurand loam, 0 to 2 percent slopes	AnA	175.30	175.36	336
	WOOD	St. Clair loam, 6 to 12 percent slopes, eroded	StC2	175.36	175.38	118
	WOOD	Nappanee loam, 0 to 2 percent slopes	NnA	175.38	175.44	313
	WOOD	St. Clair silty clay loam, 12 to 18 percent slopes, eroded	SuD2	175.44	175.51	371
	WOOD	Nappanee loam, 0 to 2 percent slopes	NnA	175.51	175.55	197
	WOOD	Hoytville clay loam, 0 to 1 percent slopes	HoA	175.55	175.64	468
	WOOD	Nappanee loam, 0 to 2 percent slopes	NnA	175.64	175.69	294
	WOOD	Nappanee silty clay loam, 2 to 6 percent slopes	NpB	175.69	175.74	234
	WOOD	Hoytville clay loam, 0 to 1 percent slopes	HoA	175.74	175.81	363
	WOOD	Mermill-Aurand complex, 0 to 1 percent slopes	MfA	175.81	175.94	691

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	WOOD	Aurand loam, 0 to 2 percent slopes	AnA	175.94	175.99	297
	WOOD	Nappanee silty clay loam, 0 to 2 percent slopes	NpA	175.99	176.03	191
	WOOD	St. Clair silty clay loam, 18 to 25 percent slopes, eroded	SuE2	176.03	176.06	143
	WOOD	Water	W	176.06	176.14	420
	LUCAS	Water	W	176.14	176.14	1
	LUCAS	Water	W	176.14	176.18	256
	LUCAS	Shoals loam, occasionally flooded	Sh	176.18	176.21	117
	LUCAS	Eel loam, occasionally flooded	Ee	176.21	176.30	488
	LUCAS	Water	W	176.30	176.42	622
	LUCAS	St. Clair silty clay loam, 4 to 12 percent slopes, eroded	SuC2	176.42	176.44	144
	LUCAS	Digby sandy loam, 0 to 2 percent slopes	DgA	176.44	176.50	316
	LUCAS	Colwood loam	Co	176.50	176.52	103
	LUCAS	St. Clair silty clay loam, 12 to 25 percent slopes, severely eroded	SuE3	176.52	176.54	104
	LUCAS	St. Clair silty clay loam, 4 to 12 percent slopes, eroded	SuC2	176.54	176.57	120
	LUCAS	Seward loamy fine sand, 2 to 6 percent slopes	SdB	176.57	176.61	233
	LUCAS	Ottokee fine sand, 0 to 6 percent slopes	OtB	176.61	176.65	232
	LUCAS	Bixler loamy fine sand, 0 to 2 percent slopes	BxA	176.65	176.72	341
	LUCAS	Lamson fine sandy loam	La	176.72	176.77	247
	LUCAS	Tedrow fine sand, 0 to 3 percent slopes	TdA	176.77	176.84	417
	LUCAS	Lamson fine sandy loam	La	176.84	176.92	415
	LUCAS	Tedrow fine sand, 0 to 3 percent slopes	TdA	176.92	176.97	223
	LUCAS	Lamson fine sandy loam	La	176.97	177.11	746
	LUCAS	Tedrow fine sand, 0 to 3 percent slopes	TdA	177.11	177.16	300
	LUCAS	Lamson fine sandy loam	La	177.16	177.32	825

TABLE 7.2-1

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State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	LUCAS	Colwood loam	Co	177.32	177.42	542
	LUCAS	Bixler loamy fine sand, 0 to 2 percent slopes	BxA	177.42	177.47	226
	LUCAS	Mermill loam	Mf	177.47	177.49	121
	LUCAS	Bixler loamy fine sand, 0 to 2 percent slopes	BxA	177.49	177.56	386
	LUCAS	Mermill loam	Mf	177.56	177.86	1597
	LUCAS	Metamora sandy loam, 0 to 3 percent slopes	MmA	177.86	177.91	244
	LUCAS	Mermill loam	Mf	177.91	177.99	434
	LUCAS	Metamora sandy loam, 0 to 3 percent slopes	MmA	177.99	178.04	270
	LUCAS	Mermill loam	Mf	178.04	178.06	89
	LUCAS	Metamora sandy loam, 0 to 3 percent slopes	MmA	178.06	178.17	583
	LUCAS	Mermill loam	Mf	178.17	178.42	1313
	LUCAS	Haskins loam, 0 to 3 percent slopes	HnA	178.42	178.44	99
	LUCAS	Mermill loam	Mf	178.44	178.45	63
	LUCAS	Haskins loam, 0 to 3 percent slopes	HnA	178.45	178.50	239
	LUCAS	Mermill loam	Mf	178.50	178.54	230
	LUCAS	Hoytville clay loam, 0 to 1 percent slopes	HoA	178.54	178.61	400
	LUCAS	Haskins loam, 0 to 3 percent slopes	HnA	178.61	178.67	317
	LUCAS	Mermill loam	Mf	178.67	178.70	133
	LUCAS	Haskins loam, 0 to 3 percent slopes	HnA	178.70	178.74	200
	LUCAS	Del Rey loam, 0 to 3 percent slopes	DdA	178.74	178.75	56
	LUCAS	Mermill loam	Mf	178.75	178.78	168
	LUCAS	Nappanee loam, 0 to 3 percent slopes	NnA	178.78	178.81	156
	LUCAS	Mermill loam	Mf	178.81	178.83	125
	LUCAS	Haskins loam, 0 to 3 percent slopes	HnA	178.83	178.94	547
	LUCAS	Mermill loam	Mf	178.94	179.02	452

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	LUCAS	Haskins loam, 0 to 3 percent slopes	HnA	179.02	179.09	371
	LUCAS	Mermill loam	Mf	179.09	179.16	365
	LUCAS	Haskins loam, 0 to 3 percent slopes	HnA	179.16	179.19	122
	LUCAS	Mermill loam	Mf	179.19	179.23	211
	LUCAS	Haskins loam, 0 to 3 percent slopes	HnA	179.23	179.24	102
	LUCAS	Mermill loam	Mf	179.24	179.30	303
	LUCAS	Haskins loam, 0 to 3 percent slopes	HnA	179.30	179.33	155
	LUCAS	Mermill loam	Mf	179.33	179.56	1226
	LUCAS	Haskins loam, 0 to 3 percent slopes	HnA	179.56	179.63	376
	LUCAS	Mermill loam	Mf	179.63	179.66	152
	LUCAS	Bixler loamy fine sand, 0 to 2 percent slopes	BxA	179.66	179.76	523
	LUCAS	Colwood loam	Co	179.76	179.80	190
	LUCAS	Bixler loamy fine sand, 0 to 2 percent slopes	BxA	179.80	179.85	266
	LUCAS	Dixboro fine sandy loam, 0 to 2 percent slopes	DsA	179.85	179.88	156
	LUCAS	Sisson loam, 6 to 12 percent slopes	SmC	179.88	179.93	261
	LUCAS	Sloan loam, occasionally flooded	So	179.93	180.01	414
	LUCAS	Del Rey loam, 0 to 3 percent slopes	DdA	180.01	180.31	1579
	LUCAS	Mermill loam	Mf	180.31	180.38	421
	LUCAS	Colwood loam	Co	180.38	180.72	1774
	LUCAS	Digby sandy loam, 0 to 2 percent slopes	DgA	180.72	180.82	510
	LUCAS	Mermill loam	Mf	180.82	181.46	3417
	LUCAS	Rimer loamy fine sand, 0 to 3 percent slopes	RnA	181.46	181.53	359
	LUCAS	Ottokee fine sand, 0 to 6 percent slopes	OtB	181.53	181.67	705
	LUCAS	Granby loamy fine sand	Gr	181.67	181.74	391

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	LUCAS	Ottokee fine sand, 0 to 6 percent slopes	OtB	181.74	181.79	266
	LUCAS	Tedrow fine sand, 0 to 3 percent slopes	TdA	181.79	181.84	282
	LUCAS	Ottokee fine sand, 0 to 6 percent slopes	OtB	181.84	181.91	372
	LUCAS	Bixler loamy fine sand, 2 to 6 percent slopes	BxB	181.91	181.97	289
	LUCAS	Colwood loam	Co	181.97	182.01	195
	LUCAS	Bixler loamy fine sand, 2 to 6 percent slopes	BxB	182.01	182.04	159
	LUCAS	Colwood loam	Co	182.04	182.04	43
	LUCAS	Bixler loamy fine sand, 2 to 6 percent slopes	BxB	182.04	182.08	187
	LUCAS	Colwood loam	Co	182.08	182.18	507
	LUCAS	Bixler loamy fine sand, 2 to 6 percent slopes	BxB	182.18	182.29	600
	LUCAS	Colwood loam	Co	182.29	182.49	1072
	LUCAS	Tedrow fine sand, 0 to 3 percent slopes	TdA	182.49	182.51	99
	LUCAS	Colwood loam	Co	182.51	182.61	520
	LUCAS	Ottokee fine sand, 0 to 6 percent slopes	OtB	182.61	182.71	556
	LUCAS	Colwood loam	Co	182.71	182.80	474
	LUCAS	Ottokee fine sand, 0 to 6 percent slopes	OtB	182.80	182.99	973
	LUCAS	Granby loamy fine sand	Gr	182.99	183.10	586
	LUCAS	Ottokee fine sand, 0 to 6 percent slopes	OtB	183.10	183.16	331
	LUCAS	Granby loamy fine sand	Gr	183.16	183.26	522
	LUCAS	Ottokee fine sand, 0 to 6 percent slopes	OtB	183.26	183.30	203
	LUCAS	Tedrow fine sand, 0 to 3 percent slopes	TdA	183.30	183.33	152
	LUCAS	Granby loamy fine sand	Gr	183.33	183.36	155
	LUCAS	Ottokee fine sand, 0 to 6 percent slopes	OtB	183.36	183.42	342
	LUCAS	Granby loamy fine sand	Gr	183.42	183.49	364

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	LUCAS	Ottokee fine sand, 0 to 6 percent slopes	OtB	183.49	183.55	286
	LUCAS	Tedrow fine sand, 0 to 3 percent slopes	TdA	183.55	183.62	388
	LUCAS	Ottokee fine sand, 0 to 6 percent slopes	OtB	183.62	183.70	426
	LUCAS	Granby loamy fine sand	Gr	183.70	183.76	310
	LUCAS	Ottokee fine sand, 0 to 6 percent slopes	OtB	183.76	183.80	217
	LUCAS	Granby loamy fine sand	Gr	183.80	183.88	447
	LUCAS	Ottokee fine sand, 0 to 6 percent slopes	OtB	183.88	183.90	82
	LUCAS	Granby loamy fine sand	Gr	183.90	183.93	139
	LUCAS	Ottokee fine sand, 0 to 6 percent slopes	OtB	183.93	183.94	56
	LUCAS	Granby loamy fine sand	Gr	183.94	183.97	179
	HENRY	Granby loamy fine sand	Gr	183.97	183.97	20
	HENRY	Granby loamy fine sand	Gr	183.97	183.98	48
	HENRY	Ottokee fine sand, 0 to 6 percent slopes	OuB	183.98	184.00	96
	HENRY	Granby loamy fine sand	Gr	184.00	184.01	20
	HENRY	Tedrow loamy fine sand, 0 to 2 percent slopes	TdA	184.01	184.03	120
	HENRY	Granby loamy fine sand	Gr	184.03	184.06	144
	HENRY	Tedrow loamy fine sand, 0 to 2 percent slopes	TdA	184.06	184.07	88
	HENRY	Granby loamy fine sand	Gr	184.07	184.11	194
	HENRY	Ottokee fine sand, 0 to 6 percent slopes	OuB	184.11	184.13	88
	HENRY	Granby loamy fine sand	Gr	184.13	184.17	253
	HENRY	Ottokee fine sand, 1 to 5 percent slopes	OtB	184.17	184.20	144
	HENRY	Oakville fine sand, 2 to 12 percent slopes	OaC	184.20	184.24	185
	HENRY	Ottokee fine sand, 1 to 5 percent slopes	OtB	184.24	184.31	370
	HENRY	Granby loamy fine sand	Gr	184.31	184.43	658

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	HENRY	Ottokee fine sand, 1 to 5 percent slopes	OtB	184.43	184.52	475
	HENRY	Granby loamy fine sand	Gr	184.52	184.54	80
	HENRY	Ottokee fine sand, 1 to 5 percent slopes	OtB	184.54	184.69	831
	HENRY	Tedrow loamy fine sand, 0 to 2 percent slopes	TdA	184.69	184.71	100
	HENRY	Granby loamy fine sand	Gr	184.71	184.89	955
	FULTON	Granby loamy fine sand	Gr	184.89	184.89	9
	FULTON	Granby loamy fine sand	Gr	184.89	184.92	157
	FULTON	Tedrow loamy fine sand, 0 to 3 percent slopes	TdA	184.92	184.95	126
	FULTON	Granby loamy fine sand	Gr	184.95	184.95	35
	FULTON	Tedrow loamy fine sand, 0 to 3 percent slopes	TdA	184.95	184.99	181
	FULTON	Granby loamy fine sand	Gr	184.99	185.02	151
	FULTON	Tedrow loamy fine sand, 0 to 3 percent slopes	TdA	185.02	185.07	259
	FULTON	Granby loamy fine sand	Gr	185.07	185.09	124
	FULTON	Tedrow loamy fine sand, 0 to 3 percent slopes	TdA	185.09	185.13	221
	FULTON	Granby loamy fine sand	Gr	185.13	185.27	711
	FULTON	Ottokee fine sand, 0 to 6 percent slopes	OtB	185.27	185.28	97
	FULTON	Granby loamy fine sand	Gr	185.28	185.56	1475
	FULTON	Sloan silty clay loam, frequently flooded	So	185.56	185.63	373
	FULTON	Tedrow loamy fine sand, 0 to 3 percent slopes	TdA	185.63	185.65	96
	FULTON	Ottokee fine sand, 0 to 6 percent slopes	OtB	185.65	185.69	169
	FULTON	Tedrow loamy fine sand, 0 to 3 percent slopes	TdA	185.69	185.69	50
	FULTON	Ottokee fine sand, 0 to 6 percent slopes	OtB	185.69	185.72	149
	FULTON	Granby loamy fine sand	Gr	185.72	185.74	100
	FULTON	Tedrow loamy fine sand, 0 to 3 percent slopes	TdA	185.74	185.80	288

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	FULTON	Granby loamy fine sand	Gr	185.80	185.82	103
	FULTON	Tedrow loamy fine sand, 0 to 3 percent slopes	TdA	185.82	185.83	88
	FULTON	Ottokee fine sand, 0 to 6 percent slopes	OtB	185.83	185.85	99
	FULTON	Tedrow loamy fine sand, 0 to 3 percent slopes	TdA	185.85	185.89	195
	FULTON	Ottokee fine sand, 0 to 6 percent slopes	OtB	185.89	185.90	49
	FULTON	Tedrow loamy fine sand, 0 to 3 percent slopes	TdA	185.90	186.06	841
	FULTON	Granby loamy fine sand	Gr	186.06	186.14	454
	FULTON	Tedrow loamy fine sand, 0 to 3 percent slopes	TdA	186.14	186.18	178
	FULTON	Granby loamy fine sand	Gr	186.18	186.21	194
	FULTON	Tedrow loamy fine sand, 0 to 3 percent slopes	TdA	186.21	186.26	247
	FULTON	Granby loamy fine sand	Gr	186.26	186.28	95
	FULTON	Ottokee fine sand, 0 to 6 percent slopes	OtB	186.28	186.40	641
	FULTON	Tedrow loamy fine sand, 0 to 3 percent slopes	TdA	186.40	186.42	102
	FULTON	Ottokee fine sand, 0 to 6 percent slopes	OtB	186.42	186.45	152
	FULTON	Granby loamy fine sand	Gr	186.45	186.51	314
	FULTON	Tedrow loamy fine sand, 0 to 3 percent slopes	TdA	186.51	186.55	203
	FULTON	Granby loamy fine sand	Gr	186.55	186.57	127
	FULTON	Tedrow loamy fine sand, 0 to 3 percent slopes	TdA	186.57	186.60	136
	FULTON	Granby loamy fine sand	Gr	186.60	186.61	97
	FULTON	Tedrow loamy fine sand, 0 to 3 percent slopes	TdA	186.61	186.66	234
	FULTON	Granby loamy fine sand	Gr	186.66	186.68	119
	FULTON	Tedrow loamy fine sand, 0 to 3 percent slopes	TdA	186.68	186.77	454
	FULTON	Granby loamy fine sand	Gr	186.77	186.78	70
	FULTON	Tedrow loamy fine sand, 0 to 3 percent slopes	TdA	186.78	186.80	120

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	FULTON	Granby loamy fine sand	Gr	186.80	186.85	230
	FULTON	Tedrow loamy fine sand, 0 to 3 percent slopes	TdA	186.85	186.94	519
	FULTON	Granby loamy fine sand	Gr	186.94	187.03	429
	FULTON	Ottokee fine sand, 0 to 6 percent slopes	OtB	187.03	187.08	271
	FULTON	Granby loamy fine sand	Gr	187.08	187.13	254
	FULTON	Ottokee fine sand, 0 to 6 percent slopes	OtB	187.13	187.35	1189
	FULTON	Granby loamy fine sand	Gr	187.35	187.37	86
	FULTON	Ottokee fine sand, 0 to 6 percent slopes	OtB	187.37	187.42	300
	FULTON	Granby loamy fine sand	Gr	187.42	187.49	376
	FULTON	Ottokee fine sand, 0 to 6 percent slopes	OtB	187.49	187.53	165
	FULTON	Granby loamy fine sand	Gr	187.53	187.74	1116
	FULTON	Tedrow loamy fine sand, 0 to 3 percent slopes	TdA	187.74	187.81	358
	FULTON	Granby loamy fine sand	Gr	187.81	187.94	720
	FULTON	Tedrow loamy fine sand, 0 to 3 percent slopes	TdA	187.94	187.96	90
	FULTON	Granby loamy fine sand	Gr	187.96	188.04	432
	FULTON	Ottokee fine sand, 0 to 6 percent slopes	OtB	188.04	188.11	363
	FULTON	Granby loamy fine sand	Gr	188.11	188.14	166
	FULTON	Ottokee fine sand, 0 to 6 percent slopes	OtB	188.14	188.39	1306
	FULTON	Granby loamy fine sand	Gr	188.39	188.40	89
	FULTON	Ottokee fine sand, 0 to 6 percent slopes	OtB	188.40	188.47	341
	FULTON	Granby loamy fine sand	Gr	188.47	188.47	14
	FULTON	Ottokee fine sand, 0 to 6 percent slopes	OtB	188.47	188.51	201
	FULTON	Granby loamy fine sand	Gr	188.51	188.64	664
	FULTON	Ottokee fine sand, 0 to 6 percent slopes	OtB	188.64	188.76	676
	FULTON	Tedrow loamy fine sand, 0 to 3 percent slopes	TdA	188.76	188.79	123

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	FULTON	Granby loamy fine sand	Gr	188.79	188.99	1077
	FULTON	Colonie fine sand, 1 to 6 percent slopes	CoB	188.99	189.00	64
	FULTON	Ottokee fine sand, 0 to 6 percent slopes	OtB	189.00	189.14	721
	FULTON	Granby loamy fine sand	Gr	189.14	189.16	84
	FULTON	Colonie fine sand, 1 to 6 percent slopes	CoB	189.16	189.20	243
	FULTON	Granby loamy fine sand	Gr	189.20	189.22	107
	FULTON	Colonie fine sand, 1 to 6 percent slopes	CoB	189.22	189.25	126
	FULTON	Granby loamy fine sand	Gr	189.25	189.27	117
	FULTON	Ottokee fine sand, 0 to 6 percent slopes	OtB	189.27	189.35	431
	FULTON	Granby loamy fine sand	Gr	189.35	189.40	246
	FULTON	Ottokee fine sand, 0 to 6 percent slopes	OtB	189.40	189.49	506
	FULTON	Granby loamy fine sand	Gr	189.49	189.54	263
	FULTON	Ottokee fine sand, 0 to 6 percent slopes	OtB	189.54	189.57	134
	FULTON	Granby loamy fine sand	Gr	189.57	189.58	72
	FULTON	Ottokee fine sand, 0 to 6 percent slopes	OtB	189.58	189.62	200
	FULTON	Granby loamy fine sand	Gr	189.62	189.63	81
	FULTON	Ottokee fine sand, 0 to 6 percent slopes	OtB	189.63	189.65	79
	FULTON	Granby loamy fine sand	Gr	189.65	189.73	434
	FULTON	Ottokee fine sand, 0 to 6 percent slopes	OtB	189.73	189.81	398
	FULTON	Colonie fine sand, 6 to 12 percent slopes	CoC	189.81	189.87	348
	FULTON	Sloan silty clay loam, frequently flooded	So	189.87	189.98	558
	FULTON	Colonie fine sand, 1 to 6 percent slopes	CoB	189.98	190.05	389
	FULTON	Ottokee fine sand, 0 to 6 percent slopes	OtB	190.05	190.12	350
	FULTON	Granby loamy fine sand	Gr	190.12	190.19	371

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	FULTON	Ottokee fine sand, 0 to 6 percent slopes	OtB	190.19	190.27	448
	FULTON	Granby loamy fine sand	Gr	190.27	190.29	92
	FULTON	Ottokee fine sand, 0 to 6 percent slopes	OtB	190.29	190.31	111
	FULTON	Tedrow loamy fine sand, 0 to 3 percent slopes	TdA	190.31	190.33	71
	FULTON	Ottokee fine sand, 0 to 6 percent slopes	OtB	190.33	190.36	164
	FULTON	Tedrow loamy fine sand, 0 to 3 percent slopes	TdA	190.36	190.40	212
	FULTON	Ottokee fine sand, 0 to 6 percent slopes	OtB	190.40	190.44	248
	FULTON	Granby loamy fine sand	Gr	190.44	190.47	121
	FULTON	Ottokee fine sand, 0 to 6 percent slopes	OtB	190.47	190.56	494
	FULTON	Granby loamy fine sand	Gr	190.56	190.59	137
	FULTON	Ottokee fine sand, 0 to 6 percent slopes	OtB	190.59	190.60	88
	FULTON	Granby loamy fine sand	Gr	190.60	190.63	159
	FULTON	Ottokee fine sand, 0 to 6 percent slopes	OtB	190.63	190.68	242
	FULTON	Tedrow loamy fine sand, 0 to 3 percent slopes	TdA	190.68	190.79	571
	FULTON	Granby loamy fine sand	Gr	190.79	190.92	712
	FULTON	Ottokee fine sand, 0 to 6 percent slopes	OtB	190.92	190.94	80
	FULTON	Colonie fine sand, 6 to 12 percent slopes	CoC	190.94	190.95	91
	FULTON	Sloan silty clay loam, frequently flooded	So	190.95	191.06	563
	FULTON	Colonie fine sand, 6 to 12 percent slopes	CoC	191.06	191.08	97
	FULTON	Ottokee fine sand, 0 to 6 percent slopes	OtB	191.08	191.16	449
	FULTON	Granby loamy fine sand	Gr	191.16	191.22	293
	FULTON	Ottokee fine sand, 0 to 6 percent slopes	OtB	191.22	191.24	88
	FULTON	Granby loamy fine sand	Gr	191.24	191.30	318

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	FULTON	Tedrow loamy fine sand, 0 to 3 percent slopes	TdA	191.30	191.34	219
	FULTON	Gilford fine sandy loam	Gf	191.34	191.36	101
	FULTON	Tedrow loamy fine sand, 0 to 3 percent slopes	TdA	191.36	191.39	183
	FULTON	Gilford fine sandy loam	Gf	191.39	191.52	666
	FULTON	Tedrow loamy fine sand, 0 to 3 percent slopes	TdA	191.52	191.54	110
	FULTON	Gilford fine sandy loam	Gf	191.54	191.67	707
	FULTON	Granby loamy fine sand	Gr	191.67	191.74	360
	FULTON	Tedrow loamy fine sand, 0 to 3 percent slopes	TdA	191.74	191.84	522
	FULTON	Gilford fine sandy loam	Gf	191.84	191.95	600
	FULTON	Digby loam, 0 to 3 percent slopes	DmA	191.95	192.00	227
	FULTON	Gilford fine sandy loam	Gf	192.00	192.01	91
	FULTON	Digby loam, 0 to 3 percent slopes	DmA	192.01	192.05	199
	FULTON	Gilford fine sandy loam	Gf	192.05	192.12	357
	FULTON	Digby loam, 0 to 3 percent slopes	DmA	192.12	192.13	44
	FULTON	Millgrove loam	Mo	192.13	192.19	356
	FULTON	Digby loam, 0 to 3 percent slopes	DmA	192.19	192.24	229
	FULTON	Millgrove loam	Mo	192.24	192.26	116
	FULTON	Rimer loamy fine sand, 0 to 3 percent slopes	RnA	192.26	192.29	141
	FULTON	Millgrove loam	Mo	192.29	192.30	84
	FULTON	Rimer loamy fine sand, 0 to 3 percent slopes	RnA	192.30	192.32	122
	FULTON	Hoytville clay loam, 0 to 1 percent slopes	HoA	192.32	192.34	106
	FULTON	Haskins loam, 0 to 3 percent slopes	HkA	192.34	192.35	49
	FULTON	Hoytville clay loam, 0 to 1 percent slopes	HoA	192.35	192.37	76
	FULTON	Digby loam, 0 to 3 percent slopes	DmA	192.37	192.40	157

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	FULTON	Gilford fine sandy loam	Gf	192.40	192.43	181
	FULTON	Digby loam, 0 to 3 percent slopes	DmA	192.43	192.51	401
	FULTON	Mermill loam	Mf	192.51	192.53	136
	FULTON	Haskins loam, 0 to 3 percent slopes	HkA	192.53	192.55	109
	FULTON	Mermill loam	Mf	192.55	192.57	94
	FULTON	Haskins loam, 0 to 3 percent slopes	HkA	192.57	192.66	453
	FULTON	Mermill loam	Mf	192.66	192.72	327
	FULTON	Haskins loam, 0 to 3 percent slopes	HkA	192.72	192.72	23
	FULTON	Mermill loam	Mf	192.72	192.78	266
	FULTON	Haskins loam, 0 to 3 percent slopes	HkA	192.78	192.86	435
	FULTON	Mermill loam	Mf	192.86	192.89	171
	FULTON	Nappanee loam, 0 to 2 percent slopes	NnA	192.89	192.94	286
	FULTON	Hoytville clay loam, 0 to 1 percent slopes	HoA	192.94	193.11	881
	FULTON	Nappanee loam, 0 to 2 percent slopes	NnA	193.11	193.14	177
	FULTON	Hoytville clay loam, 0 to 1 percent slopes	HoA	193.14	193.18	164
	FULTON	Nappanee loam, 0 to 2 percent slopes	NnA	193.18	193.25	388
	FULTON	Hoytville clay loam, 0 to 1 percent slopes	HoA	193.25	193.30	262
	FULTON	Nappanee loam, 0 to 2 percent slopes	NnA	193.30	193.47	883
	FULTON	Hoytville clay loam, 0 to 1 percent slopes	HoA	193.47	193.52	273
	FULTON	Nappanee loam, 0 to 2 percent slopes	NnA	193.52	193.60	453
	FULTON	Hoytville clay loam, 0 to 1 percent slopes	HoA	193.60	193.64	170
	FULTON	Haskins loam, 0 to 3 percent slopes	HkA	193.64	193.64	7

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	FULTON	Nappanee loam, 0 to 2 percent slopes	NnA	193.64	193.72	463
	FULTON	Millgrove loam	Mo	193.72	193.76	212
	FULTON	Nappanee loam, 0 to 2 percent slopes	NnA	193.76	193.80	189
	FULTON	Hoytville clay loam, 0 to 1 percent slopes	HoA	193.80	193.84	207
	FULTON	Nappanee loam, 0 to 2 percent slopes	NnA	193.84	193.87	184
	FULTON	Hoytville clay loam, 0 to 1 percent slopes	HoA	193.87	193.89	97
	FULTON	Nappanee loam, 0 to 2 percent slopes	NnA	193.89	193.91	109
	FULTON	Hoytville clay loam, 0 to 1 percent slopes	HoA	193.91	193.96	233
	FULTON	Nappanee loam, 0 to 2 percent slopes	NnA	193.96	194.00	239
	FULTON	Hoytville clay loam, 0 to 1 percent slopes	HoA	194.00	194.03	133
	FULTON	Nappanee loam, 0 to 2 percent slopes	NnA	194.03	194.06	181
	FULTON	Hoytville clay loam, 0 to 1 percent slopes	HoA	194.06	194.40	1774
	FULTON	Nappanee loam, 0 to 2 percent slopes	NnA	194.40	194.44	197
	FULTON	Hoytville clay loam, 0 to 1 percent slopes	HoA	194.44	194.59	794
	FULTON	Nappanee loam, 0 to 2 percent slopes	NnA	194.59	194.67	425
	FULTON	Hoytville clay loam, 0 to 1 percent slopes	HoA	194.67	195.35	3627
	FULTON	Nappanee loam, 0 to 2 percent slopes	NnA	195.35	195.40	233
	FULTON	Shoals silt loam, frequently flooded	Sh	195.40	195.48	450
	FULTON	Digby loam, 0 to 3 percent slopes	DmA	195.48	195.50	100
	FULTON	Shoals silt loam, frequently flooded	Sh	195.50	195.53	136
	FULTON	Nappanee loam, 0 to 2 percent slopes	NnA	195.53	195.55	129

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	FULTON	Shoals silt loam, frequently flooded	Sh	195.55	195.57	98
	FULTON	Nappanee loam, 2 to 6 percent slopes	NnB	195.57	195.59	113
	FULTON	Nappanee loam, 0 to 2 percent slopes	NnA	195.59	195.62	140
	FULTON	Hoytville clay loam, 0 to 1 percent slopes	HoA	195.62	195.79	902
	FULTON	Nappanee loam, 0 to 2 percent slopes	NnA	195.79	195.83	238
	FULTON	Hoytville clay loam, 0 to 1 percent slopes	HoA	195.83	196.27	2278
	FULTON	Haskins loam, 0 to 3 percent slopes	HkA	196.27	196.32	303
	FULTON	Hoytville clay loam, 0 to 1 percent slopes	HoA	196.32	196.35	135
	FULTON	Rimer loamy fine sand, 0 to 3 percent slopes	RnA	196.35	196.38	175
	FULTON	Haskins loam, 0 to 3 percent slopes	HkA	196.38	196.41	123
	FULTON	Hoytville clay loam, 0 to 1 percent slopes	HoA	196.41	196.43	125
	FULTON	Nappanee loam, 0 to 2 percent slopes	NnA	196.43	196.46	160
	FULTON	Hoytville clay loam, 0 to 1 percent slopes	HoA	196.46	196.52	344
	FULTON	Nappanee loam, 0 to 2 percent slopes	NnA	196.52	196.55	145
	FULTON	Hoytville clay loam, 0 to 1 percent slopes	HoA	196.55	196.57	80
	FULTON	Nappanee loam, 0 to 2 percent slopes	NnA	196.57	196.61	210
	FULTON	Hoytville clay loam, 0 to 1 percent slopes	HoA	196.61	196.62	59
	FULTON	Rimer loamy fine sand, 0 to 3 percent slopes	RnA	196.62	196.65	160
	FULTON	Nappanee loam, 0 to 2 percent slopes	NnA	196.65	196.67	102
	FULTON	Mermill loam	Mf	196.67	196.70	182
	FULTON	Seward loamy fine sand, 2 to 6 percent slopes	SdB	196.70	196.75	257

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	FULTON	Hoytville clay loam, 0 to 1 percent slopes	HoA	196.75	196.78	160
	FULTON	Seward loamy fine sand, 2 to 6 percent slopes	SdB	196.78	196.82	209
	FULTON	Hoytville clay loam, 0 to 1 percent slopes	HoA	196.82	196.92	499
	FULTON	Haskins loam, 0 to 3 percent slopes	HkA	196.92	196.93	66
	FULTON	Hoytville clay loam, 0 to 1 percent slopes	HoA	196.93	197.37	2333
	FULTON	Nappanee loam, 0 to 2 percent slopes	NnA	197.37	197.59	1184
	FULTON	Hoytville clay loam, 0 to 1 percent slopes	HoA	197.59	197.62	152
	FULTON	Haskins loam, 0 to 3 percent slopes	HkA	197.62	197.69	348
	FULTON	Hoytville clay loam, 0 to 1 percent slopes	HoA	197.69	197.74	249
	FULTON	Haskins loam, 0 to 3 percent slopes	HkA	197.74	197.78	231
	FULTON	Hoytville clay loam, 0 to 1 percent slopes	HoA	197.78	197.83	291
	FULTON	Nappanee loam, 0 to 2 percent slopes	NnA	197.83	197.87	165
	FULTON	Hoytville clay loam, 0 to 1 percent slopes	HoA	197.87	197.92	288
	FULTON	Mermill loam	Mf	197.92	197.96	196
	FULTON	Hoytville clay loam, 0 to 1 percent slopes	HoA	197.96	199.16	6354
	FULTON	Mermill loam	Mf	199.16	199.17	63
	FULTON	Haskins loam, 0 to 3 percent slopes	HkA	199.17	199.22	258
	FULTON	Hoytville clay loam, 0 to 1 percent slopes	HoA	199.22	199.46	1266
	FULTON	Mermill loam	Mf	199.46	199.53	337
	FULTON	Hoytville clay loam, 0 to 1 percent slopes	HoA	199.53	199.78	1347
	FULTON	Mermill loam	Mf	199.78	199.85	369
	FULTON	Hoytville clay loam, 0 to 1 percent slopes	HoA	199.85	199.87	77

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	FULTON	Haskins loam, 0 to 3 percent slopes	HkA	199.87	200.00	729
	FULTON	Mermill loam	Mf	200.00	200.02	100
	FULTON	Hoytville clay loam, 0 to 1 percent slopes	HoA	200.02	200.11	478
	FULTON	Mermill loam	Mf	200.11	200.14	130
	FULTON	Hoytville clay loam, 0 to 1 percent slopes	HoA	200.14	200.28	776
	FULTON	Haskins loam, 0 to 3 percent slopes	HkA	200.28	200.35	369
	FULTON	Hoytville clay loam, 0 to 1 percent slopes	HoA	200.35	200.39	169
	FULTON	Haskins loam, 0 to 3 percent slopes	HkA	200.39	200.40	48
	FULTON	Mermill loam	Mf	200.40	200.51	623
	FULTON	Hoytville clay loam, 0 to 1 percent slopes	HoA	200.51	200.78	1417
	FULTON	Haskins loam, 0 to 3 percent slopes	HkA	200.78	200.83	277
	FULTON	Hoytville clay loam, 0 to 1 percent slopes	HoA	200.83	201.17	1780
	FULTON	Mermill loam	Mf	201.17	201.20	149
	FULTON	Haskins loam, 0 to 3 percent slopes	HkA	201.20	201.25	259
	FULTON	Hoytville clay loam, 0 to 1 percent slopes	HoA	201.25	202.13	4660
	FULTON	Mermill loam	Mf	202.13	202.16	179
	FULTON	Hoytville clay loam, 0 to 1 percent slopes	HoA	202.16	202.31	761
	FULTON	Nappanee loam, 0 to 2 percent slopes	NnA	202.31	202.35	242
	FULTON	Sloan silty clay loam, frequently flooded	So	202.35	202.40	240
	FULTON	Nappanee loam, 2 to 6 percent slopes	NnB	202.40	202.43	141
	FULTON	Mermill loam	Mf	202.43	202.49	309
	FULTON	Ziegenfuss clay loam, 0 to 1 percent slopes	Zie5A	202.49	202.80	1666
Michigan						

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
Mainline						
	LENAWEE	Ziegenfuss clay loam, 0 to 1 percent slopes	ZfsacA	202.81	203.48	3555
	LENAWEE	Wauseon loam, 0 to 3 percent slopes	WcA	203.48	203.54	307
	LENAWEE	Ziegenfuss clay loam, 0 to 1 percent slopes	ZfsacA	203.54	203.64	520
	LENAWEE	Hoytville and Wauseon loams, 0 to 3 percent slopes	HfA	203.64	203.72	442
	LENAWEE	Ziegenfuss clay loam, 0 to 1 percent slopes	ZfsacA	203.72	203.88	865
	LENAWEE	Hoytville and Wauseon loams, 0 to 3 percent slopes	HfA	203.88	203.95	327
	LENAWEE	Ziegenfuss clay loam, 0 to 1 percent slopes	ZfsacA	203.95	209.04	26891
	LENAWEE	Berrien sandy loam, 0 to 3 percent slopes	BcA	209.04	209.05	85
	LENAWEE	Wauseon loam, 0 to 3 percent slopes	WcA	209.05	209.11	288
	LENAWEE	Ziegenfuss clay loam, 0 to 1 percent slopes	ZfsacA	209.11	209.18	377
	LENAWEE	Wauseon loam, 0 to 3 percent slopes	WcA	209.18	209.24	336
	LENAWEE	Ziegenfuss clay loam, 0 to 1 percent slopes	ZfsacA	209.24	209.41	874
	LENAWEE	Wauseon loam, 0 to 3 percent slopes	WcA	209.41	209.41	5
	LENAWEE	St. Clair loam, 12 to 25 percent slopes, moderately eroded	SdD2	209.41	209.56	777
	LENAWEE	Macomb fine sandy loam, 0 to 3 percent slopes	MaA	209.56	209.61	295
	LENAWEE	Genesee loam, 0 to 3 percent slopes	GaA	209.61	209.77	831
	LENAWEE	Water	W	209.77	209.78	56
	LENAWEE	Macomb fine sandy loam, 0 to 3 percent slopes	MaA	209.78	209.82	201
	LENAWEE	Wauseon loam, 0 to 3 percent slopes	WcA	209.82	209.96	725
	LENAWEE	Plainfield and Berrien loamy sands, 0 to 3 percent slopes	PdA	209.96	209.98	131

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	LENAWEE	Wauseon loam, 0 to 3 percent slopes	WcA	209.98	210.00	102
	LENAWEE	Macomb fine sandy loam, 0 to 3 percent slopes	MaA	210.00	210.02	103
	LENAWEE	Wauseon loam, 0 to 3 percent slopes	WcA	210.02	210.06	187
	LENAWEE	Macomb fine sandy loam, 0 to 3 percent slopes	MaA	210.06	210.08	109
	LENAWEE	Wauseon loam, 0 to 3 percent slopes	WcA	210.08	210.27	1007
	LENAWEE	Brady and Macomb loams, 0 to 3 percent slopes	BkA	210.27	210.49	1170
	LENAWEE	Brady sandy loam, 0 to 3 percent slopes	BhA	210.49	210.51	137
	LENAWEE	Wauseon loam, 0 to 3 percent slopes	WcA	210.51	211.10	3099
	LENAWEE	Plainfield and Berrien loamy sands, 0 to 3 percent slopes	PdA	211.10	211.13	166
	LENAWEE	Brady and Macomb loams, 0 to 3 percent slopes	BkA	211.13	211.17	207
	LENAWEE	Plainfield and Berrien loamy sands, 0 to 3 percent slopes	PdA	211.17	211.20	163
	LENAWEE	Brady and Macomb loams, 0 to 3 percent slopes	BkA	211.20	211.54	1791
	LENAWEE	Brady sandy loam, 0 to 3 percent slopes	BhA	211.54	211.58	174
	LENAWEE	Brady and Macomb loams, 0 to 3 percent slopes	BkA	211.58	214.92	17662
	LENAWEE	Brady sandy loam, 0 to 3 percent slopes	BhA	214.92	214.96	220
	LENAWEE	Brady and Macomb loams, 0 to 3 percent slopes	BkA	214.96	214.99	171
	LENAWEE	Brady sandy loam, 0 to 3 percent slopes	BhA	214.99	215.03	199
	LENAWEE	Brady and Macomb loams, 0 to 3 percent slopes	BkA	215.03	215.11	429
	LENAWEE	Brady sandy loam, 0 to 3 percent slopes	BhA	215.11	215.16	246
	LENAWEE	Brady and Macomb loams, 0 to 3 percent slopes	BkA	215.16	215.23	386

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	LENAWEE	Brady sandy loam, 0 to 3 percent slopes	BhA	215.23	215.29	324
	LENAWEE	Brady and Macomb loams, 0 to 3 percent slopes	BkA	215.29	216.43	6023
	LENAWEE	Wauseon loam, 0 to 3 percent slopes	WcA	216.43	217.15	3787
	LENAWEE	Sebewa sandy loam, 0 to 3 percent slopes	SbA	217.15	217.23	427
	LENAWEE	Berrien sandy loam, 0 to 3 percent slopes	BcA	217.23	217.26	148
	LENAWEE	Hoytville and Wauseon loams, 0 to 3 percent slopes	HfA	217.26	217.36	523
	LENAWEE	Ziegenfuss clay loam, 0 to 1 percent slopes	ZfsacA	217.36	217.39	156
	LENAWEE	Macomb fine sandy loam, 0 to 3 percent slopes	MaA	217.39	217.43	200
	LENAWEE	Ziegenfuss clay loam, 0 to 1 percent slopes	ZfsacA	217.43	217.94	2726
	LENAWEE	Lenawee silty clay loam	Le	217.94	218.65	3734
	LENAWEE	Ziegenfuss clay loam, 0 to 1 percent slopes	ZfsacA	218.65	224.06	28574
	LENAWEE	Hoytville and Wauseon loams, 0 to 3 percent slopes	HfA	224.06	224.18	644
	LENAWEE	Nappanee silt loam, 0 to 3 percent slopes	NaA	224.18	224.44	1367
	LENAWEE	Ziegenfuss clay loam, 0 to 1 percent slopes	ZfsacA	224.44	224.49	249
	LENAWEE	Wauseon loam, 0 to 3 percent slopes	WcA	224.49	224.57	400
	LENAWEE	Hoytville and Wauseon loams, 0 to 3 percent slopes	HfA	224.57	224.64	370
	LENAWEE	Ziegenfuss clay loam, 0 to 1 percent slopes	ZfsacA	224.64	224.69	275
	MONROE	Ziegenfuss clay loam, 0 to 1 percent slopes	ZfsacA	224.69	224.69	3
	MONROE	Ziegenfuss clay loam, 0 to 1 percent slopes	ZfsacA	224.69	225.05	1932
	MONROE	Blount loam, 0 to 3 percent slopes	13A	225.05	225.19	708
	MONROE	Ziegenfuss clay loam, 0 to 1 percent slopes	ZfsacA	225.19	225.62	2262

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	MONROE	Nappanee loam, 0 to 3 percent slopes	43A	225.62	225.69	381
	MONROE	Ziegenfuss clay loam, 0 to 1 percent slopes	ZfsacA	225.69	225.83	758
	MONROE	Nappanee loam, 0 to 3 percent slopes	43A	225.83	226.23	2095
	MONROE	Ziegenfuss clay loam, 0 to 1 percent slopes	ZfsacA	226.23	226.25	122
	MONROE	Nappanee loam, 0 to 3 percent slopes	43A	226.25	226.39	715
	MONROE	Ziegenfuss clay loam, 0 to 1 percent slopes	ZfsacA	226.39	226.57	958
	MONROE	Nappanee loam, 0 to 3 percent slopes	43A	226.57	226.64	372
	MONROE	Ziegenfuss clay loam, 0 to 1 percent slopes	ZfsacA	226.64	226.73	448
	MONROE	Nappanee loam, 0 to 3 percent slopes	43A	226.73	226.80	414
	MONROE	Ziegenfuss clay loam, 0 to 1 percent slopes	ZfsacA	226.80	227.29	2580
	MONROE	Nappanee loam, 0 to 3 percent slopes	43A	227.29	227.34	257
	MONROE	Ziegenfuss clay loam, 0 to 1 percent slopes	ZfsacA	227.34	227.41	359
	MONROE	Nappanee loam, 0 to 3 percent slopes	43A	227.41	227.55	742
	MONROE	Pewamo clay loam	22	227.55	227.71	853
	MONROE	Blount loam, 0 to 3 percent slopes	13A	227.71	227.84	690
	MONROE	Pewamo clay loam	22	227.84	227.89	246
	MONROE	Blount loam, 0 to 3 percent slopes	13A	227.89	227.90	77
	MONROE	Pewamo clay loam	22	227.90	228.08	912
	MONROE	Nappanee loam, 0 to 3 percent slopes	43A	228.08	228.12	256
	MONROE	Pewamo clay loam	22	228.12	228.22	508
	MONROE	Nappanee loam, 0 to 3 percent slopes	43A	228.22	228.39	912
	MONROE	Hoytville and Wauseon loams, 0 to 3 percent slopes	100A	228.39	228.45	305

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	MONROE	Nappanee loam, 0 to 3 percent slopes	43A	228.45	228.69	1247
	MONROE	Hoytville and Wauseon loams, 0 to 3 percent slopes	100A	228.69	228.73	233
	MONROE	Oakville fine sand, loamy substratum, 0 to 6 percent slopes	49B	228.73	228.83	514
	MONROE	Nappanee loam, 0 to 3 percent slopes	43A	228.83	229.07	1275
	MONROE	Hoytville and Wauseon loams, 0 to 3 percent slopes	100A	229.07	229.79	3820
	MONROE	Nappanee loam, 0 to 3 percent slopes	43A	229.79	229.84	252
	MONROE	Hoytville and Wauseon loams, 0 to 3 percent slopes	100A	229.84	229.87	143
	MONROE	Nappanee loam, 0 to 3 percent slopes	43A	229.87	230.11	1271
	MONROE	Hoytville and Wauseon loams, 0 to 3 percent slopes	100A	230.11	230.18	352
	MONROE	Nappanee loam, 0 to 3 percent slopes	43A	230.18	230.20	145
	MONROE	Hoytville and Wauseon loams, 0 to 3 percent slopes	100A	230.20	230.22	91
	MONROE	Nappanee loam, 0 to 3 percent slopes	43A	230.22	230.27	277
	MONROE	Sloan loam	30	230.27	230.33	292
	MONROE	Metamora sandy loam, 0 to 3 percent slopes	23A	230.33	230.37	206
	MONROE	Pewamo clay loam	22	230.37	230.46	480
	MONROE	Metamora sandy loam, 0 to 3 percent slopes	23A	230.46	230.50	235
	MONROE	Corunna sandy loam	24	230.50	230.57	368
	MONROE	Metamora sandy loam, 0 to 3 percent slopes	23A	230.57	230.79	1141
	MONROE	Pewamo clay loam	22	230.79	230.88	493
	MONROE	Ypsi sandy loam, 0 to 4 percent slopes	103A	230.88	231.03	799
	MONROE	Thetford loamy sand, 0 to 3 percent slopes	40A	231.03	231.06	160

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	MONROE	Ypsi sandy loam, 0 to 4 percent slopes	103A	231.06	231.14	409
	MONROE	Ypsi sandy loam, 0 to 4 percent slopes	YpA	231.14	231.14	14
	WASHTENAW	Ypsi sandy loam, 0 to 4 percent slopes	YpA	231.14	231.25	573
	WASHTENAW	Ziegenfuss clay loam, 0 to 1 percent slopes	ZfsacA	231.25	231.31	295
	WASHTENAW	Ypsi sandy loam, 0 to 4 percent slopes	YpA	231.31	231.63	1715
	WASHTENAW	Seward sandy loam, loamy subsoil variant, 2 to 6 percent slopes	SfB	231.63	231.65	107
	WASHTENAW	Ypsi sandy loam, 0 to 4 percent slopes	YpA	231.65	231.74	482
	WASHTENAW	Sloan loam	Sc	231.74	231.89	789
	WASHTENAW	Ypsi sandy loam, 0 to 4 percent slopes	YpA	231.89	232.22	1717
	WASHTENAW	Wauseon fine sandy loam	Ws	232.22	232.24	89
	WASHTENAW	Wasepi sandy loam, 0 to 4 percent slopes	WaA	232.24	232.27	190
	WASHTENAW	Wauseon fine sandy loam	Ws	232.27	232.30	129
	WASHTENAW	Wasepi sandy loam, 0 to 4 percent slopes	WaA	232.30	232.59	1541
	WASHTENAW	Wauseon fine sandy loam	Ws	232.59	232.66	398
	WASHTENAW	Wasepi sandy loam, 0 to 4 percent slopes	WaA	232.66	232.93	1429
	WASHTENAW	Gilford sandy loam	Gf	232.93	232.97	169
	WASHTENAW	Wasepi sandy loam, 0 to 4 percent slopes	WaA	232.97	233.01	235
	WASHTENAW	Gilford sandy loam	Gf	233.01	233.05	211
	WASHTENAW	Ziegenfuss clay loam, 0 to 1 percent slopes	ZfsacA	233.05	233.15	551
	WASHTENAW	Ypsi sandy loam, 0 to 4 percent slopes	YpA	233.15	233.59	2321
	WASHTENAW	Ziegenfuss clay loam, 0 to 1 percent slopes	ZfsacA	233.59	233.66	349
	WASHTENAW	Ypsi sandy loam, 0 to 4 percent slopes	YpA	233.66	233.70	202

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	WASHTENAW	Ziegenfuss clay loam, 0 to 1 percent slopes	ZfsacA	233.70	233.75	295
	WASHTENAW	Ypsi sandy loam, 0 to 4 percent slopes	YpA	233.75	233.89	721
	WASHTENAW	Ziegenfuss clay loam, 0 to 1 percent slopes	ZfsacA	233.89	234.01	617
	WASHTENAW	Wauseon fine sandy loam	Ws	234.01	234.07	337
	WASHTENAW	Ziegenfuss clay loam, 0 to 1 percent slopes	ZfsacA	234.07	234.10	138
	WASHTENAW	Ypsi sandy loam, 0 to 4 percent slopes	YpA	234.10	234.34	1258
	WASHTENAW	Nappanee silty clay loam, 0 to 2 percent slopes	NaA	234.34	234.37	176
	WASHTENAW	Ziegenfuss clay loam, 0 to 1 percent slopes	ZfsacA	234.37	234.43	334
	WASHTENAW	Ypsi sandy loam, 0 to 4 percent slopes	YpA	234.43	234.54	568
	WASHTENAW	Ziegenfuss clay loam, 0 to 1 percent slopes	ZfsacA	234.54	234.65	580
	WASHTENAW	Nappanee silty clay loam, 0 to 2 percent slopes	NaA	234.65	234.97	1671
	WASHTENAW	Wauseon fine sandy loam	Ws	234.97	235.01	248
	WASHTENAW	Ziegenfuss clay loam, 0 to 1 percent slopes	ZfsacA	235.01	235.08	356
	WASHTENAW	Nappanee silty clay loam, 0 to 2 percent slopes	NaA	235.08	235.12	217
	WASHTENAW	Ypsi sandy loam, 0 to 4 percent slopes	YpA	235.12	235.25	675
	WASHTENAW	Wauseon fine sandy loam	Ws	235.25	235.31	295
	WASHTENAW	Kibbie fine sandy loam, 0 to 4 percent slopes	KnA	235.31	235.40	488
	WASHTENAW	Wauseon fine sandy loam	Ws	235.40	235.45	278
	WASHTENAW	Ypsi sandy loam, 0 to 4 percent slopes	YpA	235.45	235.50	281
	WASHTENAW	Boyer loamy sand, 0 to 6 percent slopes	BnB	235.50	235.57	351
	WASHTENAW	Ypsi sandy loam, 0 to 4 percent slopes	YpA	235.57	235.69	612
	WASHTENAW	Wauseon fine sandy loam	Ws	235.69	235.73	208

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	WASHTENAW	Ziegenfuss clay loam, 0 to 1 percent slopes	ZfsacA	235.73	235.76	203
	WASHTENAW	Ypsi sandy loam, 0 to 4 percent slopes	YpA	235.76	235.80	184
	WASHTENAW	Ziegenfuss clay loam, 0 to 1 percent slopes	ZfsacA	235.80	235.85	261
	WASHTENAW	Nappanee silty clay loam, 2 to 6 percent slopes	NaB	235.85	235.86	85
	WASHTENAW	Ziegenfuss clay loam, 0 to 1 percent slopes	ZfsacA	235.86	235.95	445
	WASHTENAW	Dixboro-Kibbie fine sandy loams, 0 to 4 percent slopes	DoA	235.95	235.99	216
	WASHTENAW	Nappanee silty clay loam, 0 to 2 percent slopes	NaA	235.99	236.06	363
	WASHTENAW	Ziegenfuss clay loam, 0 to 1 percent slopes	ZfsacA	236.06	236.17	591
	WASHTENAW	Pella silt loam	Pc	236.17	236.21	208
	WASHTENAW	Nappanee silty clay loam, 0 to 2 percent slopes	NaA	236.21	236.34	695
	WASHTENAW	Ziegenfuss clay loam, 0 to 1 percent slopes	ZfsacA	236.34	236.39	272
	WASHTENAW	Nappanee silty clay loam, 2 to 6 percent slopes	NaB	236.39	236.48	446
	WASHTENAW	Ziegenfuss clay loam, 0 to 1 percent slopes	ZfsacA	236.48	236.50	115
	WASHTENAW	Pella silt loam	Pc	236.50	236.63	686
	WASHTENAW	Ypsi sandy loam, 0 to 4 percent slopes	YpA	236.63	236.70	372
	WASHTENAW	Pella silt loam	Pc	236.70	236.73	136
	WASHTENAW	Nappanee silty clay loam, 2 to 6 percent slopes	NaB	236.73	236.78	297
	WASHTENAW	Pella silt loam	Pc	236.78	236.84	292
	WASHTENAW	Ypsi sandy loam, 0 to 4 percent slopes	YpA	236.84	236.87	158
	WASHTENAW	Kendallville loam, 2 to 6 percent slopes	KeB	236.87	236.89	148
	WASHTENAW	Pella silt loam	Pc	236.89	236.94	240
	WASHTENAW	Seward sandy loam, loamy subsoil variant, 2 to 6 percent slopes	SfB	236.94	237.15	1111

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	WASHTENAW	Pella silt loam	Pc	237.15	237.20	255
	WASHTENAW	Seward sandy loam, loamy subsoil variant, 2 to 6 percent slopes	SfB	237.20	237.25	256
	WASHTENAW	Kibbie fine sandy loam, 0 to 4 percent slopes	KnA	237.25	237.41	884
	WASHTENAW	Sisson fine sandy loam, 2 to 6 percent slopes	SnB	237.41	237.52	579
	WASHTENAW	Kibbie fine sandy loam, 0 to 4 percent slopes	KnA	237.52	237.61	465
	WASHTENAW	Pella silt loam	Pc	237.61	237.65	216
	WASHTENAW	Kibbie fine sandy loam, 0 to 4 percent slopes	KnA	237.65	237.71	303
	WASHTENAW	Pella silt loam	Pc	237.71	238.03	1661
	WASHTENAW	Wauseon fine sandy loam	Ws	238.03	238.37	1835
	WASHTENAW	Gilford sandy loam	Gf	238.37	238.45	412
	WASHTENAW	Wasepi sandy loam, 0 to 4 percent slopes	WaA	238.45	238.95	2648
	WASHTENAW	Gilford sandy loam	Gf	238.95	239.05	492
	WASHTENAW	Wasepi sandy loam, 0 to 4 percent slopes	WaA	239.05	239.30	1322
	WASHTENAW	Gilford sandy loam	Gf	239.30	239.57	1438
	WASHTENAW	Wasepi sandy loam, 0 to 4 percent slopes	WaA	239.57	239.63	316
	WASHTENAW	Gilford sandy loam	Gf	239.63	239.64	72
	WASHTENAW	Wasepi sandy loam, 0 to 4 percent slopes	WaA	239.64	240.09	2366
	WASHTENAW	Gilford sandy loam	Gf	240.09	240.18	483
	WASHTENAW	Wasepi sandy loam, 0 to 4 percent slopes	WaA	240.18	240.19	57
	WASHTENAW	Gilford sandy loam	Gf	240.19	240.38	1014
	WASHTENAW	Cohoctah fine sandy loam, frequently flooded	Cc	240.38	240.48	484
	WASHTENAW	Wasepi sandy loam, 0 to 4 percent slopes	WaA	240.48	240.83	1884
	WASHTENAW	Oshtemo loamy sand, 0 to 6 percent slopes	OsB	240.83	240.88	266
	WASHTENAW	Wasepi sandy loam, 0 to 4 percent slopes	WaA	240.88	240.91	161

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	WASHTENAW	Oshtemo loamy sand, 0 to 6 percent slopes	OsB	240.91	241.01	530
	WASHTENAW	Wasepi sandy loam, 0 to 4 percent slopes	WaA	241.01	241.77	3996
	WASHTENAW	Boyer loamy sand, 0 to 6 percent slopes	BnB	241.77	241.81	183
	WASHTENAW	Wasepi sandy loam, 0 to 4 percent slopes	WaA	241.81	242.02	1116
	WASHTENAW	Boyer loamy sand, 0 to 6 percent slopes	BnB	242.02	242.06	235
	WASHTENAW	Wasepi sandy loam, 0 to 4 percent slopes	WaA	242.06	242.10	200
	WASHTENAW	Boyer loamy sand, 0 to 6 percent slopes	BnB	242.10	242.18	445
	WASHTENAW	Wasepi sandy loam, 0 to 4 percent slopes	WaA	242.18	242.25	357
	WASHTENAW	Fox sandy loam, 0 to 2 percent slopes	FoA	242.25	242.28	166
	WASHTENAW	Wasepi sandy loam, 0 to 4 percent slopes	WaA	242.28	242.30	67
	WASHTENAW	Fox sandy loam, 0 to 2 percent slopes	FoA	242.30	242.36	355
	WASHTENAW	Wasepi sandy loam, 0 to 4 percent slopes	WaA	242.36	242.45	465
	WASHTENAW	Boyer loamy sand, 0 to 6 percent slopes	BnB	242.45	242.48	167
	WASHTENAW	Gilford sandy loam	Gf	242.48	242.64	831
	WASHTENAW	Wasepi sandy loam, 0 to 4 percent slopes	WaA	242.64	242.70	342
	WASHTENAW	Boyer loamy sand, 0 to 6 percent slopes	BnB	242.70	242.74	190
	WASHTENAW	Wasepi sandy loam, 0 to 4 percent slopes	WaA	242.74	242.82	439
	WASHTENAW	Boyer loamy sand, 0 to 6 percent slopes	BnB	242.82	242.89	351
	WASHTENAW	Gilford sandy loam	Gf	242.89	242.94	246
	WASHTENAW	Boyer loamy sand, 0 to 6 percent slopes	BnB	242.94	242.95	70
	WASHTENAW	Gilford sandy loam	Gf	242.95	242.99	207

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	WASHTENAW	Wasepi sandy loam, 0 to 4 percent slopes	WaA	242.99	243.07	410
	WASHTENAW	Gilford sandy loam	Gf	243.07	243.09	141
	WASHTENAW	Wasepi sandy loam, 0 to 4 percent slopes	WaA	243.09	243.17	429
	WASHTENAW	Boyer loamy sand, 0 to 6 percent slopes	BnB	243.17	243.24	368
	WASHTENAW	Wasepi sandy loam, 0 to 4 percent slopes	WaA	243.24	243.29	226
	WASHTENAW	Boyer loamy sand, 0 to 6 percent slopes	BnB	243.29	243.32	150
	WASHTENAW	Wasepi sandy loam, 0 to 4 percent slopes	WaA	243.32	243.36	260
	WASHTENAW	Gilford sandy loam	Gf	243.36	243.43	363
	WASHTENAW	Wasepi sandy loam, 0 to 4 percent slopes	WaA	243.43	243.56	672
	WASHTENAW	Boyer loamy sand, 0 to 6 percent slopes	BnB	243.56	243.85	1531
	WASHTENAW	Wasepi sandy loam, 0 to 4 percent slopes	WaA	243.85	243.92	366
	WASHTENAW	Gilford sandy loam	Gf	243.92	244.08	832
	WASHTENAW	Wasepi sandy loam, 0 to 4 percent slopes	WaA	244.08	244.15	388
	WASHTENAW	Boyer loamy sand, 0 to 6 percent slopes	BnB	244.15	244.58	2239
	WASHTENAW	Owosso-Miami complex, 2 to 6 percent slopes	OwB	244.58	244.63	277
	WASHTENAW	Macomb loam, 0 to 4 percent slopes	MaA	244.63	244.83	1091
	WASHTENAW	Boyer loamy sand, 0 to 6 percent slopes	BnB	244.83	244.84	21
	WASHTENAW	Cohoctah fine sandy loam, frequently flooded	Cc	244.84	245.02	936
	WASHTENAW	Water	W	245.02	245.06	239
	WASHTENAW	Boyer loamy sand, 0 to 6 percent slopes	BnB	245.06	245.31	1323
	WASHTENAW	Gilford sandy loam	Gf	245.31	245.41	508
	WASHTENAW	Boyer loamy sand, 0 to 6 percent slopes	BnB	245.41	245.58	908

TABLE 7.2-1

Summary of Soil Types by County and State and Milepost Affected by the NEXUS Project Pipeline Facilities

State/ Facility	County	Soil Association/ Series/Complex	Map Unit Symbol	Mileposts Crossed Through Soil Type		Approximate Crossing Length (ft) a/
				Milepost Start	Milepost End	
	WASHTENAW	Wasepi sandy loam, 0 to 4 percent slopes	WaA	245.58	246.01	2284
	WASHTENAW	Boyer loamy sand, 0 to 6 percent slopes	BnB	246.01	246.06	230
	WASHTENAW	Wasepi sandy loam, 0 to 4 percent slopes	WaA	246.06	246.34	1518
	WASHTENAW	Gilford sandy loam	Gf	246.34	246.42	389
	WASHTENAW	Wasepi sandy loam, 0 to 4 percent slopes	WaA	246.42	247.08	3479
	WASHTENAW	Spinks loamy sand, 0 to 6 percent slopes	SpB	247.08	247.65	3038
	WASHTENAW	Wasepi sandy loam, 0 to 4 percent slopes	WaA	247.65	247.67	119
	WASHTENAW	Gilford sandy loam	Gf	247.67	247.80	688
	WASHTENAW	Spinks loamy sand, 0 to 6 percent slopes	SpB	247.80	247.96	844
	WASHTENAW	Wasepi sandy loam, 0 to 4 percent slopes	WaA	247.96	248.04	414
	WASHTENAW	Gilford sandy loam	Gf	248.04	248.15	561
	WASHTENAW	Spinks loamy sand, 0 to 6 percent slopes	SpB	248.15	248.31	861
	WASHTENAW	Wasepi sandy loam, 0 to 4 percent slopes	WaA	248.31	248.44	681
	WASHTENAW	Gilford sandy loam	Gf	248.44	248.57	697
	WASHTENAW	Wasepi sandy loam, 0 to 4 percent slopes	WaA	248.57	248.91	1756
	WASHTENAW	Gilford sandy loam	Gf	248.91	248.94	206
	WASHTENAW	Wasepi sandy loam, 0 to 4 percent slopes	WaA	248.94	249.03	467
	WASHTENAW	Wasepi sandy loam, 0 to 4 percent slopes	WaA	248.94	249.03	467

a/ Soil crossing lengths are rounded to the nearest whole number

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility		Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
						Water (K Factor) c/	Wind (WEG) d/								
Ohio															
TGP Interconnect															
	COLUMBIANA	BkB	Berks channery silt loam, 2 to 6 percent slopes	1.3	0.6	0.17	6	4	All areas are prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	20-40	Fair
	COLUMBIANA	BkC	Berks channery silt loam, 6 to 15 percent slopes	3.4	1.3	0.17	6	10.5	Not prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	20-40	Fair
	COLUMBIANA	BkD	Berks channery silt loam, 15 to 25 percent slopes	4.1	1.8		6	20	Not prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	20-40	Fair
	COLUMBIANA	BkE	Berks channery silt loam, 25 to 40 percent slopes	0.1	0.0		6	32.5	Not prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	20-40	Fair
	COLUMBIANA	CoC	Coshocton silt loam, 6 to 15 percent slopes	1.2	1.1		5	10.5	Not prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	40-84	Good
	COLUMBIANA	GnB	Gilpin silt loam, 2 to 6 percent slopes	0.3	0.2	0.32	6	4	All areas are prime farmland	Well drained	C	Non-Hydric	Low potential for compaction	20-40	Good
	COLUMBIANA	OrA	Orrville silt loam, 0 to 2 percent slopes, occasionally flooded	0.7	0.3	0.37	6	1	Prime farmland if drained	Somewha t poorly drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Good

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility		Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
						Water (K Factor) c/	Wind (WEG) d/								
Mainline															
	COLUMBIANA	Am F	Amanda loam, 35 to 70 percent slopes	1.1	0.5	0.37	5	52.5	Not prime farmland	Well drained	C	Non-Hydric	Low potential for compaction	>60	Fair
	COLUMBIANA	BkC	Berks channery silt loam, 6 to 15 percent slopes	1.2	0.5	0.17	6	10.5	Not prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	20-40	Fair
	COLUMBIANA	BkD	Berks channery silt loam, 15 to 25 percent slopes	3.9	1.5		6	20	Not prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	20-40	Fair
	COLUMBIANA	BkE	Berks channery silt loam, 25 to 40 percent slopes	2.3	1.0		6	32.5	Not prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	20-40	Fair
	COLUMBIANA	BtB	Bogart silt loam, 2 to 6 percent slopes	1.3	0.4	0.32	5	4	All areas are prime farmland	Moderately well drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Good
	COLUMBIANA	BtF 4F1	Bethesda and Fairpoint channery silt loams, 25 to 70 percent slopes	1.1	0.5	0.17	5	45	Not prime farmland	Well drained	D	Non-Hydric	Low potential for compaction	>80	Fair
	COLUMBIANA	CcB	Canfield silt loam, 2 to 6 percent slopes	17.8	7.1	0.37	5	4	All areas are prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>80	Good

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility		Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
						Water (K Factor) c/	Wind (WEG) d/								
	COLUMBIANA	CcC	Canfield silt loam, 6 to 12 percent slopes	27.9	11.6	0.37	5	9	Not prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>80	Good
	COLUMBIANA	CcD	Canfield silt loam, 12 to 20 percent slopes	4.6	1.7	0.37	5	16	Not prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>80	Fair
	COLUMBIANA	CcE	Canfield silt loam, 20 to 35 percent slopes	11.4	4.9	0.37	5	27.5	Not prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>80	Fair
	COLUMBIANA	CdC	Canfield silt loam, 6 to 12 percent slopes	0.0	0.0	0.37	5	9	Not prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>80	Good
	COLUMBIANA	ChC	Chili silt loam, 6 to 12 percent slopes	0.1	0.0	0.32	5	9	Not prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>60	Good
	COLUMBIANA	CoC	Coshocton silt loam, 6 to 15 percent slopes	0.9	0.7		5	10.5	Not prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	40-84	Good
	COLUMBIANA	FcD	Fairpoint silty clay loam, 8 to 25 percent slopes	0.7	0.7	0.43	6	16.5	Not prime farmland	Well drained	C	Non-Hydric	Low potential for compaction	>60	Poor
	COLUMBIANA	FdA	Fitchville silt loam, 0 to 2 percent slopes	4.6	1.8	0.37	6	1	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	>80	Good
	COLUMBIANA	FdB	Fitchville silt loam, 2 to 6 percent slopes	1.5	0.5	0.37	6	4	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	>80	Good

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility		Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
						Water (K Factor) c/	Wind (WEG) d/								
	COLUMBIANA	FeA	Fluvaquents, silty, 0 to 1 percent slopes, frequently flooded	0.3	0.2			0.5	Not prime farmland	Very poorly drained	D	Hydric	High potential for compaction	>80	Very poor
	COLUMBIANA	FnC 2	Fredericktown gravelly loam, 6 to 15 percent slopes, eroded	5.1	1.7	0.24	5	10.5	Not prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>80	Good
	COLUMBIANA	FoB	Fredericktown silt loam, 2 to 6 percent slopes	0.2	0.1	0.32	5	4	All areas are prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>80	Good
	COLUMBIANA	Gn C	Gilpin silt loam, 6 to 15 percent slopes	7.9	3.5		6	10.5	Not prime farmland	Well drained	C	Non-Hydric	Low potential for compaction	20-40	Good
	COLUMBIANA	Gn D	Gilpin silt loam, 15 to 25 percent slopes	9.2	4.0	0.24	6	20	Not prime farmland	Well drained	C	Non-Hydric	Low potential for compaction	20-40	Fair
	COLUMBIANA	GrC	Glenford silt loam, 6 to 12 percent slopes	2.2	0.9	0.37	6	10.5	Not prime farmland	Moderately well drained	C/D	Non-Hydric	Moderate potential for compaction	>60	Good
	COLUMBIANA	HeC	Hazleton channery loam, 6 to 15 percent slopes	3.8	1.5		5	10.5	Not prime farmland	Well drained	A	Non-Hydric	Low potential for compaction	40-80	Good
	COLUMBIANA	HeE	Hazleton channery loam, 25 to 40 percent slopes	1.8	0.8		5	32.5	Not prime farmland	Well drained	A	Non-Hydric	Low potential for compaction	40-80	Fair

NEXUS GAS TRANSMISSION

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility		Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
						Water (K Factor) c/	Wind (WEG) d/								
	COLUMBIANA	JwB	Jimtown silt loam, 2 to 6 percent slopes	2.3	0.7	0.32	5	4	Prime farmland if drained	Somewhat poorly drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Good
	COLUMBIANA	KnC	Kensington silt loam, 6 to 15 percent slopes	8.0	3.4		6	10.5	Not prime farmland	Moderately well drained	B	Non-Hydric	Moderate potential for compaction	>60	Good
	COLUMBIANA	KnD	Kensington silt loam, 15 to 25 percent slopes	13.6	6.1		6	20	Not prime farmland	Moderately well drained	B	Non-Hydric	Moderate potential for compaction	>60	Fair
	COLUMBIANA	McB	Mechanicsburg silt loam, 2 to 6 percent slopes	5.5	2.2	0.37	6	4	All areas are prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	40-72	Good
	COLUMBIANA	Mc C	Mechanicsburg silt loam, 6 to 15 percent slopes	1.2	0.4	0.1	6	10.5	Not prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	40-72	Good
	COLUMBIANA	ReB	Ravenna silt loam, 2 to 6 percent slopes	0.1	0.1	0.37	6	4	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>80	Good
	COLUMBIANA	ReB	Ravenna silt loam, 2 to 6 percent slopes	1.8	0.7	0.37	5	4	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>80	Good
	COLUMBIANA	RsB	Rittman silt loam, 2 to 6 percent slopes	5.2	2.0	0.43	6	4	All areas are prime farmland	Moderately well drained	D	Non-Hydric	Moderate potential for compaction	40-60	Good
	COLUMBIANA	RsC	Rittman silt loam, 6 to 12 percent slopes	5.4	2.2	0.43	6	9	Not prime farmland	Moderately well drained	D	Non-Hydric	Moderate potential for compaction	40-60	Good

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility		Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
						Water (K Factor) c/	Wind (WEG) d/								
	COLUMBIANA	RsD 2	Rittman silt loam, 12 to 20 percent slopes, eroded	1.6	0.5	0.43	6	16	Not prime farmland	Moderately well drained	D	Non-Hydric	Moderate potential for compaction	40-60	Fair
	COLUMBIANA	TeC	Teegarden silt loam, 6 to 15 percent slopes	5.3	2.2	0.37	6	10.5	Not prime farmland	Moderately well drained	C/D	Non-Hydric	Moderate potential for compaction	>60	Good
	COLUMBIANA	TeC 2	Teegarden silt loam, 6 to 15 percent slopes, eroded	4.4	1.8	0.37	6	10.5	Not prime farmland	Moderately well drained	C/D	Non-Hydric	Moderate potential for compaction	>60	Good
	COLUMBIANA	Ub	Udorthents, refuse substratum, 2 to 25 percent slopes	0.4	0.2	0.24	5	13.5	Not prime farmland	Moderately well drained	A	Non-Hydric	Moderate potential for compaction	>80	
	COLUMBIANA	Wa B	Wadsworth silt loam, 2 to 6 percent slopes	0.4	0.2	0.43	6	4	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>60	Good
	COLUMBIANA	Wo A	Wick silt loam, 0 to 2 percent slopes, frequently flooded	3.8	2.0	0.43	5	0.5	Prime farmland if drained and either protected from flooding or not frequently flooded during the growing season	Very poorly drained	B/D	Hydric	High potential for compaction	>80	Poor

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility		Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
						Water (K Factor) c/	Wind (WEG) d/								
	COLUMBIANA	ZeA	Zepernick silt loam, 0 to 2 percent slopes, occasionally flooded	6.4	3.2	0.37	6	0.5	Prime farmland if drained	Somewhat poorly drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Poor
	STARK	BoA	Bogart silt loam, 0 to 2 percent slopes	2.0	0.7	0.32	5	1	All areas are prime farmland	Moderately well drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Good
	STARK	BoB	Bogart silt loam, 2 to 6 percent slopes	3.8	1.5	0.32	5	4	All areas are prime farmland	Moderately well drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Good
	STARK	CdB	Canfield silt loam, 2 to 6 percent slopes	29.6	11.6	0.37	5	4	All areas are prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>80	Good
	STARK	CdC	Canfield silt loam, 6 to 12 percent slopes	10.9	3.9	0.37	5	9	Not prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>80	Good
	STARK	CdC 2	Canfield silt loam, 6 to 12 percent slopes, moderately eroded	13.2	5.3	0.37	5	9	Not prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>80	Good
	STARK	CdD 2	Canfield silt loam, 12 to 18 percent slopes, moderately eroded	2.8	1.3	0.37	5	15	Not prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>80	Fair
	STARK	Cg	Carlisle muck	0.3	0.1		2	1	Not prime farmland	Very poorly drained	A/D	Hydric	High potential for compaction	>60	Poor

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility		Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
						Water (K Factor) c/	Wind (WEG) d/								
	STARK	Ch	Carlisle muck	3.5	1.7		2	1	Not prime farmland	Very poorly drained	A/D	Hydric	High potential for compaction	>60	Poor
	STARK	CnB	Chili loam, 2 to 6 percent slopes	3.6	1.5	0.32	5	4	All areas are prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>60	Good
	STARK	CoC	Chili gravelly loam, 6 to 12 percent slopes	4.9	2.1	0.24	5	9	Not prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>60	Good
	STARK	CoC 2	Chili gravelly loam, 6 to 12 percent slopes, moderately eroded	1.4	0.6	0.24	5	9	Not prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>60	Good
	STARK	CoD 2	Chili gravelly loam, 12 to 18 percent slopes, moderately eroded	2.0	0.8	0.1	5	15	Not prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>60	Fair
	STARK	CoE 2	Chili gravelly loam, 18 to 25 percent slopes, moderately eroded	0.5	0.0	0.24	5	22	Not prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>60	Fair
	STARK	CpA	Chili silt loam, 0 to 2 percent slopes	1.3	0.6	0.32	5	1	All areas are prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>60	Good
	STARK	CpB	Chili silt loam, 2 to 6 percent slopes	20.7	8.8	0.32	5	4	All areas are prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>60	Good

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility		Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
						Water (K Factor) c/	Wind (WEG) d/								
	STARK	CpC	Chili silt loam, 6 to 12 percent slopes	7.6	3.3	0.32	5	9	Not prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>60	Good
	STARK	CpC 2	Chili silt loam, 6 to 12 percent slopes, moderately eroded	11.9	5.1	0.32	5	9	Not prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>60	Good
	STARK	CyB	Conotton gravelly loam, 2 to 6 percent slopes	2.2	0.9	0.24	5	4	Not prime farmland	Well drained	A	Non-Hydric	Low potential for compaction	>80	Fair
	STARK	CyD 2	Conotton gravelly loam, 12 to 18 percent slopes, moderately eroded	1.2	0.4	0.24	5	15	Not prime farmland	Well drained	A	Non-Hydric	Low potential for compaction	>80	Fair
	STARK	CyE 2	Conotton gravelly loam, 18 to 25 percent slopes, moderately eroded	0.7	0.5	0.24	5	22	Not prime farmland	Well drained	A	Non-Hydric	Low potential for compaction	>80	Fair
	STARK	Da	Damascus loam	3.5	0.9	0.24	6	1	Prime farmland if drained	Poorly drained	B/D	Hydric	High potential for compaction	>75	Fair
	STARK	Da	Damascus loam	0.0	0.0	0.32	6	1	Prime farmland if drained	Poorly drained	B/D	Hydric	High potential for compaction	>75	Fair

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility		Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
						Water (K Factor) c/	Wind (WEG) d/								
	STARK	FcA	Fitchville silt loam, 0 to 2 percent slopes	16.8	7.1	0.37	6	1	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	>80	Good
	STARK	FcB	Fitchville silt loam, 2 to 6 percent slopes	0.7	0.3	0.37	6	4	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	>80	Good
	STARK	GfB	Glenford silt loam, 2 to 6 percent slopes	1.0	0.4	0.37	6	4	All areas are prime farmland	Moderately well drained	C/D	Non-Hydric	Moderate potential for compaction	>60	Good
	STARK	GfC	Glenford silt loam, 6 to 12 percent slopes	0.6	0.3	0.37	6	9	Not prime farmland	Moderately well drained	C/D	Non-Hydric	Moderate potential for compaction	>60	Good
	STARK	LaD	Latham silt loam, 12 to 18 percent slopes	0.5	0.3	0.43	6	15	Not prime farmland	Moderately well drained	D	Non-Hydric	Moderate potential for compaction	20-40	Fair
	STARK	Ly	Luray silt loam	7.8	3.2	0.32	6	1	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>60	Fair
	STARK	Lz	Luray silt loam, gravelly subsoil variant	4.2	1.7	0.32	6	1	Prime farmland if drained	Very poorly drained	B/D	Hydric	High potential for compaction	>60	Fair
	STARK	Me B	Mentor silt loam, 2 to 6 percent slopes	0.5	0.2	0.37	5	4	All areas are prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>60	Good
	STARK	ReA	Ravenna silt loam, 0 to 2 percent slopes	9.3	3.7	0.37	6	1	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>80	Good

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility		Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
						Water (K Factor) c/	Wind (WEG) d/								
	STARK	ReB	Ravenna silt loam, 2 to 6 percent slopes	33.8	13.5	0.37	6	4	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>80	Good
	STARK	RsB	Rittman silt loam, 2 to 6 percent slopes	3.0	1.1	0.43	6	4	All areas are prime farmland	Moderately well drained	D	Non-Hydric	Moderate potential for compaction	40-60	Good
	STARK	RsC 2	Rittman silt loam, 6 to 12 percent slopes, moderately eroded	5.8	2.3	0.43	6	9	Not prime farmland	Moderately well drained	D	Non-Hydric	Moderate potential for compaction	40-60	Good
	STARK	RsD 2	Rittman silt loam, 12 to 18 percent slopes, moderately eroded	0.7	0.2	0.43	6	15	Not prime farmland	Moderately well drained	D	Non-Hydric	Moderate potential for compaction	40-60	Fair
	STARK	Sb	Sebring silt loam	13.2	5.2	0.37	6	1	Prime farmland if drained	Poorly drained	C/D	Hydric	High potential for compaction	>60	Fair
	STARK	Se	Sebring silt loam, till substratum	2.6	1.0	0.37	6	1	Prime farmland if drained	Poorly drained	C/D	Hydric	High potential for compaction	>60	Fair
	STARK	Sh	Shoals silt loam	4.7	2.1	0.24	6	1	Prime farmland if drained	Somewhat poorly drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Fair

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility: Water (K Factor) c/	Erodibility: Wind (WEG) d/	Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
	STARK	Sl	Sloan silt loam	1.0	0.6	0.28	6	1	Prime farmland if drained and either protected from flooding or not frequently flooded during the growing season	Very poorly drained	B/D	Hydric	High potential for compaction	>60	Fair
	STARK	Wa A	Wadsworth silt loam, 0 to 2 percent slopes	9.8	3.9	0.43	6	1	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>60	Good
	STARK	Wa B	Wadsworth silt loam, 2 to 6 percent slopes	31.0	11.8	0.43	6	4	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>60	Good
	STARK	Wa C	Wadsworth silt loam, 6 to 12 percent slopes	1.4	0.5	0.43	6	9	Not prime farmland	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>60	Good
	STARK	Wa C2	Wadsworth silt loam, 6 to 12 percent slopes, moderately eroded	3.9	1.6	0.43	6	9	Not prime farmland	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>60	Good
	STARK	Wh A	Weinbach silt loam, 0 to 2 percent slopes	6.2	2.4	0.43	6	1	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>60	Good
	STARK	Wh B	Weinbach silt loam, 2 to 6 percent slopes	5.3	1.7	0.43	6	4	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>60	Good

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility		Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
						Water (K Factor) c/	Wind (WEG) d/								
	STARK	WrB	Wheeling silt loam, 2 to 6 percent slopes	3.1	1.2	0.37	5	4	All areas are prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	40-60	Good
	STARK	WrC	Wheeling silt loam, 6 to 12 percent slopes	0.9	0.4	0.37	5	9	Not prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	40-60	Good
	STARK	Wt	Willette muck	2.6	1.2		2	1	Not prime farmland	Very poorly drained	C/D	Hydric	High potential for compaction	>60	Poor
	STARK	Wu B	Wooster silt loam, 2 to 6 percent slopes	0.3	0.0	0.37	5	4	All areas are prime farmland	Well drained	C	Non-Hydric	Low potential for compaction	>85	Good
	STARK	Wu C	Wooster silt loam, 6 to 12 percent slopes	1.0	0.4	0.37	5	9	Not prime farmland	Well drained	C	Non-Hydric	Low potential for compaction	>85	Good
	STARK	Wu C2	Wooster silt loam, 6 to 12 percent slopes, moderately eroded	8.5	3.5	0.37	5	9	Not prime farmland	Well drained	C	Non-Hydric	Low potential for compaction	>85	Good
	STARK	Wu D2	Wooster silt loam, 12 to 18 percent slopes, moderately eroded	1.6	0.6	0.37	5	15	Not prime farmland	Well drained	C	Non-Hydric	Low potential for compaction	>85	Fair
	SUMMIT	BgA	Bogart loam, 0 to 2 percent slopes	2.0	0.9	0.32	5	1	All areas are prime farmland	Moderately well drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Good

NEXUS GAS TRANSMISSION

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility		Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
						Water (K Factor) c/	Wind (WEG) d/								
	SUMMIT	BgB	Bogart loam, 2 to 6 percent slopes	1.7	0.7	0.32	5	4	All areas are prime farmland	Moderately well drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Good
	SUMMIT	Ca	Canadice silty clay loam	0.8	0.4	0.49	6	1	Not prime farmland	Poorly drained	D	Hydric	High potential for compaction	>60	Poor
	SUMMIT	CdA	Canfield silt loam, 0 to 2 percent slopes	0.7	0.2	0.37	5	1	All areas are prime farmland	Moderately well drained	D	Non-Hydric	Moderate potential for compaction	>80	Good
	SUMMIT	CdB	Canfield silt loam, 2 to 6 percent slopes	0.3	0.1	0.37	5	4	All areas are prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>80	Good
	SUMMIT	CdB	Canfield silt loam, 2 to 6 percent slopes	39.3	14.4	0.37	5	4	All areas are prime farmland	Moderately well drained	D	Non-Hydric	Moderate potential for compaction	>80	Good
	SUMMIT	CdC	Canfield silt loam, 6 to 12 percent slopes	0.8	0.5	0.37	5	9	Not prime farmland	Moderately well drained	D	Non-Hydric	Moderate potential for compaction	>80	Good
	SUMMIT	CdC 2	Canfield silt loam, 6 to 12 percent slopes, moderately eroded	1.6	0.8	0.37	5	9	Not prime farmland	Moderately well drained	D	Non-Hydric	Moderate potential for compaction	>80	Good
	SUMMIT	CeB	Canfield silt loam, sandstone substratum, 2 to 6 percent slopes	0.6	0.3	0.37	5	4	All areas are prime farmland	Moderately well drained	D	Non-Hydric	Moderate potential for compaction	40-60	Good

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility		Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
						Water (K Factor) c/	Wind (WEG) d/								
	SUMMIT	Cg	Carlisle muck	10.5	6.0		2	1	Not prime farmland	Very poorly drained	A/D	Hydric	High potential for compaction	>60	Poor
	SUMMIT	Ck	Chagrin silt loam, alkaline	0.1	0.1	0.32	5	1	Prime farmland if protected from flooding or not frequently flooded during the growing season	Well drained	B	Non-Hydric	Low potential for compaction	>60	Good
	SUMMIT	CnA	Chili loam, 0 to 2 percent slopes	0.4	0.2	0.32	5	1	All areas are prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>60	Fair
	SUMMIT	CnB	Chili loam, 2 to 6 percent slopes	5.8	2.6	0.1	5	4	All areas are prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>60	Fair
	SUMMIT	CnC	Chili loam, 6 to 12 percent slopes	0.2	0.1	0.1	5	9	Not prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>60	Fair
	SUMMIT	CoC 2	Chili gravelly loam, 6 to 12 percent slopes, moderately eroded	1.0	0.4	0.24	8	9	Not prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>60	Fair
	SUMMIT	CoD 2	Chili gravelly loam, 12 to 18 percent slopes, moderately eroded	0.6	0.3	0.24	8	15	Not prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>60	Fair

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility: Water (K Factor) c/	Erodibility: Wind (WEG) d/	Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
	SUMMIT	CpA	Chili silt loam, 0 to 2 percent slopes	2.1	0.8	0.32	5	1	All areas are prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>60	Fair
	SUMMIT	CpB	Chili silt loam, 2 to 6 percent slopes	10.7	4.1	0.1	5	4	All areas are prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>60	Fair
	SUMMIT	CpC	Chili silt loam, 6 to 12 percent slopes	7.6	3.4	0.1	5	9	Not prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>60	Fair
	SUMMIT	Cw C2	Chili-Wooster complex, 6 to 12 percent slopes, moderately eroded	7.9	3.1	0.1	5	9	Not prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>60	Fair
	SUMMIT	CyD	Conotton-Oshtemo complex, 12 to 18 percent slopes	3.8	1.5	0.24	8	15	Not prime farmland	Well drained	A	Non-Hydric	Low potential for compaction	>80	Fair
	SUMMIT	CyE	Conotton-Oshtemo complex, 18 to 25 percent slopes	0.3	0.2	0.1	8	21	Not prime farmland	Well drained	A	Non-Hydric	Low potential for compaction	>80	Fair
	SUMMIT	CyF	Conotton-Oshtemo complex, 25 to 50 percent slopes	0.5	0.3	0.1	8	38	Not prime farmland	Well drained	A	Non-Hydric	Low potential for compaction	>80	Fair

TABLE 7.2-2

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	SUMMIT	Da	Damascus loam	1.0	0.5	0.32	6	1	Prime farmland if drained	Poorly drained	B/D	Hydric	High potential for compaction	>75	Fair
	SUMMIT	DkF	Dekalb sandy loam, 25 to 70 percent slopes	0.6	0.2	0.24	3	50	Not prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	36	Poor
	SUMMIT	FcA	Fitchville silt loam, 0 to 2 percent slopes	6.3	3.0	0.37	6	1	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	>80	Fair
	SUMMIT	FcB	Fitchville silt loam, 2 to 6 percent slopes	0.5	0.2	0.37	6	4	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	>80	Fair
	SUMMIT	Fr	Frenchtown silt loam	0.0	0.0	0.37	6	1	Prime farmland if drained	Poorly drained	D	Hydric	High potential for compaction	>80	Poor
	SUMMIT	GfA	Glenford silt loam, 0 to 2 percent slopes	1.1	0.6	0.37	6	1	All areas are prime farmland	Moderately well drained	C/D	Non-Hydric	Moderate potential for compaction	>60	Good
	SUMMIT	GfB	Glenford silt loam, 2 to 6 percent slopes	3.8	1.6	0.37	6	4	All areas are prime farmland	Moderately well drained	C/D	Non-Hydric	Moderate potential for compaction	>60	Good

TABLE 7.2-2

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						Water (K Factor) c/	Wind (WEG) d/								
	SUMMIT	Ho	Holly silt loam	1.3	0.6	0.28	6	1	Prime farmland if drained and either protected from flooding or not frequently flooded during the growing season	Poorly drained	B/D	Hydric	High potential for compaction	>60	Fair
	SUMMIT	Hy	Holly silt loam, alkaline	0.4	0.2	0.28	6	1	Prime farmland if drained and either protected from flooding or not frequently flooded during the growing season	Poorly drained	B/D	Hydric	High potential for compaction	>60	Fair
	SUMMIT	JtA	Jimtown loam, 0 to 2 percent slopes	4.0	1.9	0.32	5	1	Prime farmland if drained	Somewhat poorly drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Fair
	SUMMIT	Ld	Linwood muck	3.0	1.4		2	1	Not prime farmland	Very poorly drained	B/D	Hydric	High potential for compaction	>60	Poor
	SUMMIT	Ln	Lorain silty clay loam	0.3	0.1	0.32	7	1	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	20-40	Poor

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility Water (K Factor) c/	Erodibility Wind (WEG) d/	Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
	SUMMIT	LoB	Loudonville silt loam, 2 to 6 percent slopes	0.2	0.2	0.32	5	4	All areas are prime farmland	Well drained	C	Non-Hydric	Low potential for compaction	20-40	Fair
	SUMMIT	LoD	Loudonville silt loam, 12 to 18 percent slopes	2.4	0.6	0.32	5	15	Not prime farmland	Well drained	C	Non-Hydric	Low potential for compaction	20-40	Fair
	SUMMIT	Ly	Luray silt loam	0.0	0.0	0.32	6	1	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>60	Poor
	SUMMIT	Od	Olmsted loam	0.1	0.0	0.24	5	1	Prime farmland if drained	Very poorly drained	B/D	Hydric	High potential for compaction	>60	Poor
	SUMMIT	Or	Orrville silt loam	0.5	0.3	0.37	5	1	Prime farmland if drained and either protected from flooding or not frequently flooded during the growing season	Somewhat poorly drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Fair
	SUMMIT	OsB	Oshtemo sandy loam, 2 to 6 percent slopes	2.1	0.6	0.24	3	4	All areas are prime farmland	Well drained	A	Non-Hydric	Low potential for compaction	>80	Fair
	SUMMIT	OsC	Oshtemo sandy loam, 6 to 12 percent slopes	1.4	0.7	0.24	3	9	Not prime farmland	Well drained	A	Non-Hydric	Low potential for compaction	>80	Fair

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility		Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
						Water (K Factor) c/	Wind (WEG) d/								
	SUMMIT	ReA	Ravenna silt loam, 0 to 2 percent slopes	6.2	2.5	0.37	5	1	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>80	Fair
	SUMMIT	ReB	Ravenna silt loam, 2 to 6 percent slopes	5.2	2.5	0.37	5	4	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>80	Fair
	SUMMIT	Sb	Sebring silt loam	10.6	5.1	0.37	6	1	Prime farmland if drained	Poorly drained	C/D	Hydric	High potential for compaction	>60	Poor
	SUMMIT	So	Sloan silt loam	0.0	0.0	0.28	6	1	Prime farmland if drained and either protected from flooding or not frequently flooded during the growing season	Very poorly drained	B/D	Hydric	High potential for compaction	>60	Poor
	SUMMIT	Ua	Udorthents	1.1	0.5			0	Not prime farmland					N/A	
	SUMMIT	Uf	Udorthents, sanitary landfill	1.7	0.9			0	Not prime farmland					N/A	
	SUMMIT	W	Water	0.1	0.1			0	Not prime farmland					N/A	
	SUMMIT	WrA	Wheeling silt loam, 0 to 2 percent slopes	0.5	0.2	0.37	5	1	All areas are prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	40-60	Good

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility		Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
						Water (K Factor) c/	Wind (WEG) d/								
	SUMMIT	WrB	Wheeling silt loam, 2 to 6 percent slopes	1.5	0.5	0.2	5	4	All areas are prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	40-60	Good
	SUMMIT	Wu B	Wooster silt loam, 2 to 6 percent slopes	25.5	8.1	0.37	5	4	All areas are prime farmland	Well drained	C	Non-Hydric	Low potential for compaction	>85	Good
	SUMMIT	Wu C	Wooster silt loam, 6 to 12 percent slopes	1.3	0.3	0.37	5	9	Not prime farmland	Well drained	C	Non-Hydric	Low potential for compaction	>85	Good
	SUMMIT	Wu C2	Wooster silt loam, 6 to 12 percent slopes, moderately eroded	30.7	13.0	0.37	5	9	Not prime farmland	Well drained	C	Non-Hydric	Low potential for compaction	>85	Good
	SUMMIT	Wu D	Wooster silt loam, 12 to 18 percent slopes	2.4	0.9	0.37	5	15	Not prime farmland	Well drained	C	Non-Hydric	Low potential for compaction	>85	Good
	SUMMIT	Wu D2	Wooster silt loam, 12 to 18 percent, moderately eroded	6.8	3.4	0.37	5	15	Not prime farmland	Well drained	C	Non-Hydric	Low potential for compaction	>85	Good
	SUMMIT	Wu E2	Wooster silt loam, 18 to 25 percent slopes, moderately eroded	1.5	0.6	0.37	5	22	Not prime farmland	Well drained	C	Non-Hydric	Low potential for compaction	>85	Good

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility		Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
						Water (K Factor) c/	Wind (WEG) d/								
	SUMMIT	Wu F2	Wooster silt loam, 25 to 50 percent slopes, moderately eroded	0.5	0.3	0.37	5	38	Not prime farmland	Well drained	C	Non-Hydric	Low potential for compaction	>85	Good
	WAYNE	BtB	Bogart loam, 2 to 6 percent slopes	1.3	0.6	0.32	5	4	All areas are prime farmland	Moderately well drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Good
	WAYNE	CdB	Canfield silt loam, 2 to 6 percent slopes	33.7	11.7	0.37	5	4	All areas are prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>80	Good
	WAYNE	CdB 2	Canfield silt loam, 2 to 6 percent slopes, eroded	3.2	1.2	0.37	5	4	All areas are prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>80	Good
	WAYNE	CdC	Canfield silt loam, 6 to 12 percent slopes	9.5	4.0	0.37	5	9	Farmland of local importance	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>80	Good
	WAYNE	CdC 2	Canfield silt loam, 6 to 12 percent slopes, eroded	5.7	2.1	0.37	5	9	Farmland of local importance	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>80	Good
	WAYNE	CnC	Chili loam, 6 to 12 percent slopes	0.1	0.0	0.32	5	9	Farmland of local importance	Well drained	B	Non-Hydric	Low potential for compaction	>60	Good
	WAYNE	GfB	Glenford silt loam, 2 to 6 percent slopes	11.9	4.4	0.37	6	4	All areas are prime farmland	Moderately well drained	C/D	Non-Hydric	Moderate potential for compaction	>60	Good

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility: Water (K Factor) c/	Erodibility: Wind (WEG) d/	Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
	WAYNE	GfC	Glenford silt loam, 6 to 12 percent slopes	4.3	0.8	0.37	6	9	Farmland of local importance	Moderately well drained	C/D	Non-Hydric	Moderate potential for compaction	>60	Good
	WAYNE	GfC 2	Glenford silt loam, 6 to 12 percent slopes, eroded	0.0	0.0	0.37	6	9	Farmland of local importance	Moderately well drained	C/D	Non-Hydric	Moderate potential for compaction	>60	Good
	WAYNE	LnD	Loudonville silt loam, 12 to 18 percent slopes	0.1	0.0	0.32	5	15	Not prime farmland	Well drained	C	Non-Hydric	Low potential for compaction	20-40	Fair
	WAYNE	Or	Orrville silt loam, occasionally flooded	3.1	1.4	0.37	6	1	Prime farmland if drained	Somewhat poorly drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Good
	WAYNE	ReA	Ravenna silt loam, 0 to 2 percent slopes	9.5	4.3	0.37	6	1	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>80	Good
	WAYNE	ReB	Ravenna silt loam, 2 to 6 percent slopes	5.3	2.0	0.37	6	4	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>80	Good
	WAYNE	Wu C2	Wooster-Riddles silt loams, 6 to 12 percent slopes, eroded	7.6	3.0	0.32	5	9	Farmland of local importance	Well drained	C	Non-Hydric	Low potential for compaction	40-60	Good
	WAYNE	Wu D2	Wooster-Riddles silt loams, 12 to 18 percent slopes, eroded	2.6	1.3	0.37	5	15	Farmland of local importance	Well drained	C	Non-Hydric	Low potential for compaction	40-60	Fair

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility		Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
						Water (K Factor) c/	Wind (WEG) d/								
	MEDINA	BnA	Bennington silt loam, 0 to 2 percent slopes	4.4	2.1	0.43	6	1	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	>80	Good
	MEDINA	BnB	Bennington silt loam, 2 to 6 percent slopes	14.1	5.3	0.43	6	3	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	>80	Good
	MEDINA	BtB	Bogart loam, 2 to 6 percent slopes	5.3	2.0	0.32	5	3	All areas are prime farmland	Moderately well drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Good
	MEDINA	Ca	Canadice silty clay loam	3.1	1.4	0.49	6	0.8	Farmland of local importance	Poorly drained	D	Hydric	High potential for compaction	>60	Fair
	MEDINA	CcA	Caneadea silt loam, 0 to 2 percent slopes	1.6	0.8	0.43	6	1	Farmland of local importance	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>60	Good
	MEDINA	CdB	Canfield silt loam, 2 to 6 percent slopes	1.9	0.5	0.37	5	3	All areas are prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>80	Good
	MEDINA	CgB	Cardington silt loam, 2 to 6 percent slopes	2.9	1.1	0.37	5	3	All areas are prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	78	Good
	MEDINA	CgC2	Cardington silt loam, 6 to 12 percent slopes, moderately eroded	5.1	1.8	0.37	5	8	Farmland of local importance	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	78	Good

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility: Water (K Factor) c/	Erodibility: Wind (WEG) d/	Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
	MEDINA	CgE 2	Cardington silt loam, 12 to 25 percent slopes, moderately eroded	0.9	0.4	0.37	5	14	Not prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	78	Fair
	MEDINA	Ch	Carlisle muck	0.0			2	0.2	Farmland of local importance	Very poorly drained	A/D	Hydric	High potential for compaction	>60	Poor
	MEDINA	CnB	Chili loam, 2 to 6 percent slopes	2.3	0.8	0.17	5	5	All areas are prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>60	Good
	MEDINA	CnC	Chili loam, 6 to 12 percent slopes	0.6	0.2	0.17	5	8	Farmland of local importance	Well drained	B	Non-Hydric	Low potential for compaction	>60	Good
	MEDINA	CoC 2	Chili gravelly loam, 6 to 12 percent slopes, moderately eroded	1.3	0.5	0.17	8	10	Farmland of local importance	Well drained	B	Non-Hydric	Low potential for compaction	>60	Good
	MEDINA	CoE 2	Chili gravelly loam, 12 to 25 percent slopes, moderately eroded	0.9	0.2	0.17	8	14	Not prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>60	Fair
	MEDINA	CpB	Chili silt loam, 2 to 6 percent slopes	2.2	0.9	0.17	5	4	All areas are prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>60	Good
	MEDINA	CpC	Chili silt loam, 6 to 12 percent slopes	2.1	0.8	0.17	5	8	Farmland of local importance	Well drained	B	Non-Hydric	Low potential for compaction	>60	Good

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility		Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
						Water (K Factor) c/	Wind (WEG) d/								
	MEDINA	Cy	Condit silt loam, 0 to 1 percent slopes	2.1	0.8	0.37	6	0.5	Prime farmland if drained	Poorly drained	C/D	Hydric	High potential for compaction	>80	
	MEDINA	ElB	Ellsworth silt loam, 2 to 6 percent slopes	2.1	1.0	0.43	6	3	All areas are prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>60	Good
	MEDINA	ElB 2	Ellsworth silt loam, 2 to 6 percent slopes, moderately eroded	13.8	5.1	0.43	6	4	All areas are prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>60	Good
	MEDINA	ElC 2	Ellsworth silt loam, 6 to 12 percent slopes, moderately eroded	4.1	1.7	0.43	6	10	Farmland of local importance	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>60	Good
	MEDINA	ElE 2	Ellsworth silt loam, 12 to 25 percent slopes, moderately eroded	9.9	4.3	0.43	6	16	Not prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>60	Fair
	MEDINA	ElF	Ellsworth silt loam, 25 to 70 percent slopes	1.5	0.7	0.43	6	25	Not prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>60	Poor
	MEDINA	EvA	Euclid silt loam, occasionally flooded	3.1	1.3	0.37	5	1	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	>74	Good
	MEDINA	FcA	Fitchville silt loam, 0 to 2 percent slopes	2.8	1.4	0.37	6	1	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	>80	Good

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility		Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
						Water (K Factor) c/	Wind (WEG) d/								
	MEDINA	FcB	Fitchville silt loam, 2 to 6 percent slopes	2.2	0.8	0.37	6	3	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	>80	Good
	MEDINA	GfB	Glenford silt loam, 2 to 6 percent slopes	3.1	1.2	0.37	6	3	All areas are prime farmland	Moderately well drained	C/D	Non-Hydric	Moderate potential for compaction	>60	Good
	MEDINA	GfC 2	Glenford silt loam, 6 to 12 percent slopes, moderately eroded	0.1	0.0	0.37	6	8	Farmland of local importance	Moderately well drained	C/D	Non-Hydric	Moderate potential for compaction	>60	Good
	MEDINA	Hy	Holly silt loam	5.6	1.9	0.28	6	0.8	Prime farmland if drained and either protected from flooding or not frequently flooded during the growing season	Poorly drained	B/D	Hydric	High potential for compaction	>60	Fair
	MEDINA	JtA	Jimtown loam, 0 to 2 percent slopes	6.1	2.0	0.32	5	1	Prime farmland if drained	Somewhat poorly drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Good

NEXUS GAS TRANSMISSION

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility		Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
						Water (K Factor) c/	Wind (WEG) d/								
	MEDINA	Le	Lobdell silt loam	4.4	2.1	0.37	6	1	Prime farmland if protected from flooding or not frequently flooded during the growing season	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>60	Fair
	MEDINA	Ly	Luray silt loam	4.6	1.6	0.32	6	1	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>60	Poor
	MEDINA	Mg A	Mahoning silt loam, 0 to 2 percent slopes	29.3	11.2	0.43	6	2	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	40-60	Good
	MEDINA	Mg B	Mahoning silt loam, 2 to 6 percent slopes	37.9	15.3	0.43	6	3	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	40-60	Good
	MEDINA	MlA	Mahoning silt loam, sandstone substratum, 0 to 2 percent slopes	0.2	0.1	0.43	6	1	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	40-60	Good
	MEDINA	Mr	Miner silty clay loam	3.2	1.5	0.32	6	0.5	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>60	Poor
	MEDINA	Od	Olmsted loam	0.7	0.3	0.24	5	0.5	Prime farmland if drained	Very poorly drained	B/D	Hydric	High potential for compaction	>60	Poor

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility		Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
						Water (K Factor) c/	Wind (WEG) d/								
	MEDINA	Or	Orrville silt loam	9.2	4.6	0.37	5	0.5	Prime farmland if drained and either protected from flooding or not frequently flooded during the growing season	Somewhat poorly drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Fair
	MEDINA	OtB	Oshtemo sandy loam, 2 to 6 percent slopes	1.4	0.5	0.24	3	4	All areas are prime farmland	Well drained	A	Non-Hydric	Low potential for compaction	>80	Good
	MEDINA	ReB	Ravenna silt loam, 2 to 6 percent slopes	1.2	0.2	0.37	5	3	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>80	Good
	MEDINA	RsB	Rittman silt loam, 2 to 6 percent slopes	32.7	12.3	0.43	5	3	All areas are prime farmland	Moderately well drained	D	Non-Hydric	Moderate potential for compaction	40-60	Good
	MEDINA	RsB 2	Rittman silt loam, 2 to 6 percent slopes, moderately eroded	12.0	4.6	0.43	5	5	All areas are prime farmland	Moderately well drained	D	Non-Hydric	Moderate potential for compaction	40-60	Good
	MEDINA	RsC 2	Rittman silt loam, 6 to 12 percent slopes, moderately eroded	23.1	9.0	0.43	5	10	Farmland of local importance	Moderately well drained	D	Non-Hydric	Moderate potential for compaction	40-60	Good

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility Water (K Factor) c/	Erodibility Wind (WEG) d/	Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
	MEDINA	RsE 2	Rittman silt loam, 12 to 25 percent slopes, moderately eroded	4.3	2.1	0.43	5	14	Not prime farmland	Moderately well drained	D	Non-Hydric	Moderate potential for compaction	40-60	Fair
	MEDINA	RsF	Rittman silt loam, 25 to 70 percent slopes	1.7	0.8	0.43	5	25	Not prime farmland	Moderately well drained	D	Non-Hydric	Moderate potential for compaction	40-60	Fair
	MEDINA	Sg	Sebring silt loam	3.5	1.3	0.37	6	0.5	Prime farmland if drained	Poorly drained	C/D	Hydric	High potential for compaction	>60	Fair
	MEDINA	St	Sebring silt loam, till substratum	4.0	1.7	0.37	6	0.5	Prime farmland if drained	Poorly drained	C/D	Hydric	High potential for compaction	>60	Fair
	MEDINA	Ud	Udorthents, loamy	5.4	1.7			3	Not prime farmland					N/A	
	MEDINA	Wa A	Wadsworth silt loam, 0 to 2 percent slopes	28.6	10.7	0.43	6	2	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>60	Good
	MEDINA	Wa B	Wadsworth silt loam, 2 to 6 percent slopes	29.7	11.9	0.43	6	3	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>60	Good
	MEDINA	Wc	Wallkill silt loam	2.2	1.0	0.37	5	1	Farmland of local importance	Poorly drained	B/D	Hydric	High potential for compaction	>59	Poor
	MEDINA	Wu B	Wooster silt loam, 2 to 6 percent slopes	1.4	0.6	0.37	5	3	All areas are prime farmland	Well drained	C	Non-Hydric	Low potential for compaction	>85	Good

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

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						Water (K Factor) c/	Wind (WEG) d/								
	MEDINA	Wu C2	Wooster-Riddles silt loams, 6 to 12 percent slopes, eroded	0.2	0.0	0.32	5	9	Farmland of local importance	Well drained	C	Non-Hydric	Low potential for compaction	40-60	Good
	MEDINA	Wu C2	Wooster silt loam, 6 to 12 percent slopes, moderately eroded	0.9	0.3	0.37	5	8	Farmland of local importance	Well drained	C	Non-Hydric	Low potential for compaction	>85	Good
	MEDINA	Wu E2	Wooster silt loam, 12 to 25 percent slopes, moderately eroded	1.8	0.8	0.37	5	14	Not prime farmland	Well drained	C	Non-Hydric	Low potential for compaction	>85	Fair
	MEDINA	Wv B	Wooster-Riddles silt loams, 2 to 6 percent slopes	2.8	0.7	0.32	5	4	All areas are prime farmland	Well drained	C	Non-Hydric	Low potential for compaction	40-60	Good
	MEDINA	Wv C2	Wooster-Riddles silt loams, 6 to 12 percent slopes, eroded	1.5	0.5	0.32	5	9	Farmland of local importance	Well drained	C	Non-Hydric	Low potential for compaction	40-60	Good
	LORAIN	AgF	Alexandria silt loam, 25 to 50 percent slopes	0.0	0.0	0.37	5	30	Not prime farmland	Well drained	C	Non-Hydric	Low potential for compaction	>80	Poor
	LORAIN	BtA	Bogart loam, 0 to 2 percent slopes	1.3	0.7	0.32	5	1	All areas are prime farmland	Moderately well drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Good

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility Water (K Factor) c/	Erodibility Wind (WEG) d/	Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
	LORAIN	BtB	Bogart loam, 2 to 6 percent slopes	2.2	0.8	0.32	5	4	All areas are prime farmland	Moderately well drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Good
	LORAIN	CaB	Cardington silt loam, 2 to 6 percent slopes	0.0	0.0	0.37	6	4	All areas are prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	78	Good
	LORAIN	ClA	Chili loam, 0 to 2 percent slopes	3.4	1.0	0.32	5	1	All areas are prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>60	Good
	LORAIN	ElB	Ellsworth silt loam, 2 to 6 percent slopes	0.5	0.2	0.43	6	4	All areas are prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>60	Good
	LORAIN	ElB 2	Ellsworth silt loam, 2 to 6 percent slopes, moderately eroded	1.2	0.3	0.43	6	4	All areas are prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>60	Good
	LORAIN	ElC 2	Ellsworth silt loam, 6 to 12 percent slopes, moderately eroded	3.9	1.7	0.43	6	9	Not prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>60	Good
	LORAIN	ElD 2	Ellsworth silt loam, 12 to 18 percent slopes, moderately eroded	0.8	0.4	0.43	6	15	Not prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>60	Fair

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility		Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
						Water (K Factor) c/	Wind (WEG) d/								
	LORAIN	ElF 2	Ellsworth silt loam, 18 to 50 percent slopes, moderately eroded	1.7	0.7	0.43	6	34	Not prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>60	Fair
	LORAIN	FdA	Fitchville silt loam, low terrace, 0 to 2 percent slopes	5.5	2.5	0.37	5	1	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	>80	Good
	LORAIN	HsA	Haskins loam, 0 to 2 percent slopes	13.9	4.7	0.37	5	1	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	>60	Good
	LORAIN	HsB	Haskins loam, 2 to 6 percent slopes	0.4	0.2	0.37	5	4	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	>60	Good
	LORAIN	JtA	Jimtown loam, 0 to 2 percent slopes	0.5	0.2	0.32	5	1	Prime farmland if drained	Somewhat poorly drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Good
	LORAIN	Lb	Lobdell silt loam	5.0	1.1	0.37	6	1	Prime farmland if protected from flooding or not frequently flooded during the growing season	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>60	Good
	LORAIN	Mg A	Mahoning silt loam, 0 to 2 percent slopes	154.5	61.4	0.43	6	1	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	40-60	Good

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility		Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
						Water (K Factor) c/	Wind (WEG) d/								
	LORAIN	Mg B	Mahoning silt loam, 2 to 6 percent slopes	32.5	12.8	0.43	6	4	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	40-60	Good
	LORAIN	Mg B	Mahoning silt loam, 2 to 6 percent slopes	0.1	0.0	0.43	6	3	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	40-60	Good
	LORAIN	Mg B2	Mahoning silt loam, 2 to 6 percent slopes, moderately eroded	0.5	0.2	0.43	6	4	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	40-60	Good
	LORAIN	MkA	Mahoning-Tiro silt loams, 0 to 2 percent slopes	36.4	14.5	0.43	6	1	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	40-60	Good
	LORAIN	MkB	Mahoning-Tiro silt loams, 2 to 6 percent slopes	2.7	1.0	0.43	6	4	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	40-60	Good
	LORAIN	Mr	Miner silty clay loam	8.6	3.5	0.32	7	1	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>60	Fair
	LORAIN	MtB	Mitiwanga silt loam, 2 to 6 percent slopes	7.5	3.2	0.32	6	4	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	20-40	Good

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility		Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
						Water (K Factor) c/	Wind (WEG) d/								
	LORAIN	Or	Orrville silt loam	4.6	1.9	0.37	5	1	Prime farmland if drained and either protected from flooding or not frequently flooded during the growing season	Somewhat poorly drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Good
	LORAIN	RdA	Rawson loam, 0 to 2 percent slopes	0.9	0.4	0.32	5	1	All areas are prime farmland	Moderately well drained	D	Non-Hydric	Moderate potential for compaction	>60	Good
	LORAIN	RdB	Rawson loam, 2 to 6 percent slopes	0.0	0.0	0.32	5	4	All areas are prime farmland	Moderately well drained	D	Non-Hydric	Moderate potential for compaction	>60	Good
	LORAIN	Sb	Sebring silt loam	1.0	0.4	0.37	6	1	Prime farmland if drained	Poorly drained	C/D	Hydric	High potential for compaction	>60	Fair
	LORAIN	Tg	Tioga fine sandy loam	0.7	0.7	0.37	3	1	Prime farmland if protected from flooding or not frequently flooded during the growing season	Well drained	A	Non-Hydric	Low potential for compaction	>50	Good

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility		Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
						Water (K Factor) c/	Wind (WEG) d/								
	LORAIN	TrA	Trumbull silty clay loam, 0 to 2 percent slopes	30.8	12.4	0.37	7	1	Not prime farmland	Poorly drained	D	Hydric	High potential for compaction	>60	Fair
	LORAIN	W	Water	0.4	0.4			0	Not prime farmland					N/A	
	ERIE	AgF	Alexandria silt loam, 25 to 50 percent slopes	0.1	0.1	0.37	5	30	Not prime farmland	Well drained	C	Non-Hydric	Low potential for compaction	>80	Poor
	ERIE	AkA	Allis clay loam, 0 to 2 percent slopes	1.9	0.6	0.43	6	1	Not prime farmland	Poorly drained	D	Hydric	High potential for compaction	36	Fair
	ERIE	AnG	Amanda-Dekalb-Rock outcrop association, 40 to 70 percent slopes	1.5	1.2	0.37	6	55	Not prime farmland	Well drained	C	Non-Hydric	Low potential for compaction	20-40	Poor
	ERIE	BgA	Bennington silt loam, 0 to 2 percent slopes	32.7	12.9	0.43	6	1	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	>80	Good
	ERIE	BgB	Bennington silt loam, 2 to 6 percent slopes	11.5	4.2	0.43	6	4	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	>80	Good
	ERIE	BkA	Bixler loamy fine sand, 0 to 2 percent slopes	11.9	4.5	0.17	2	1	Prime farmland if drained	Somewhat poorly drained	B	Non-Hydric	Moderate potential for compaction	>80	Fair

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility		Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
						Water (K Factor) c/	Wind (WEG) d/								
	ERIE	BkB	Bixler loamy fine sand, 2 to 6 percent slopes	0.7	0.2	0.17	2	4	Prime farmland if drained	Somewhat poorly drained	B	Non-Hydric	Moderate potential for compaction	>80	Fair
	ERIE	CaB	Cardington silt loam, 2 to 6 percent slopes	13.8	5.2	0.37	6	4	All areas are prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	78	Good
	ERIE	CbC 2	Cardington silty clay loam, 6 to 12 percent slopes, eroded	3.8	1.4	0.37	7	9	Not prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	78	Good
	ERIE	CcA	Castalia very channery loam, 0 to 2 percent slopes	7.7	3.6	0.2	8	1	Not prime farmland	Well drained	A	Non-Hydric	Low potential for compaction	20-40	Poor
	ERIE	CcB	Castalia very channery loam, 2 to 6 percent slopes	3.5	1.3	0.2	8	4	Not prime farmland	Well drained	A	Non-Hydric	Low potential for compaction	20-40	Poor
	ERIE	ChB	Chili loam, loamy substratum, 2 to 6 percent slopes	6.2	1.9	0.32	5	4	All areas are prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>60	Good
	ERIE	Cm A	Colwood loam, 0 to 1 percent slopes	15.7	6.0	0.28	5	0.5	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>60	Poor

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility		Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
						Water (K Factor) c/	Wind (WEG) d/								
	ERIE	CnA	Colwood silt loam, bedrock substratum, 0 to 1 percent slopes	4.6	1.7	0.43	5	0.5	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>60	Poor
	ERIE	CoA	Condit silt loam, 0 to 1 percent slopes	11.9	4.6	0.37	6	0.5	Prime farmland if drained	Poorly drained	C/D	Hydric	High potential for compaction	>80	
	ERIE	CtB	Conotton loam, 2 to 6 percent slopes	0.9	0.4	0.24	5	4	All areas are prime farmland	Well drained	A	Non-Hydric	Low potential for compaction	>80	Fair
	ERIE	CuC	Conotton gravelly loam, 6 to 12 percent slopes	0.4	0.2	0.24	8	9	Not prime farmland	Well drained	A	Non-Hydric	Low potential for compaction	>80	Fair
	ERIE	DeA	Del Rey silt loam, 0 to 2 percent slopes	3.1	1.0	0.43	6	1	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	>60	Good
	ERIE	DuA	Dunbridge loamy sand, 0 to 2 percent slopes	2.5	0.9	0.24	2	1	All areas are prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	20-40	Fair
	ERIE	DuB	Dunbridge loamy sand, 2 to 6 percent slopes	1.4	0.5	0.17	2	4	All areas are prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	20-40	Fair
	ERIE	EcA	Elliott silt loam, bedrock substratum, 0 to 2 percent slopes	1.2	0.4	0.28	6	1	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	65-67	Good

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility		Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
						Water (K Factor) c/	Wind (WEG) d/								
	ERIE	EnA	Elnora loamy fine sand, 0 to 4 percent slopes	2.4	1.0	0.17	2	2	Not prime farmland	Moderately well drained	A/D	Non-Hydric	Moderate potential for compaction	>80	Good
	ERIE	FrA	Fries silty clay loam, 0 to 1 percent slopes	9.4	3.8	0.28	7	0.5	Prime farmland if drained	Very poorly drained	D	Hydric	High potential for compaction	28-30	Fair
	ERIE	GtB	Glenford silt loam, 2 to 6 percent slopes	0.1	0.0	0.37	6	3	All areas are prime farmland	Moderately well drained	C/D	Non-Hydric	Moderate potential for compaction	>60	Good
	ERIE	HkA	Haskins loam, 0 to 2 percent slopes	7.6	3.2	0.37	5	1	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	>60	Good
	ERIE	HoA	Holly silt loam, 0 to 1 percent slopes, occasionally flooded	8.0	4.2	0.28	6	0.5	Prime farmland if drained	Poorly drained	B/D	Hydric	High potential for compaction	>60	Fair
	ERIE	HrB	Hornell silt loam, 2 to 6 percent slopes	0.5	0.2	0.43	6	4	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	20-40	Good
	ERIE	HsA	Hornell silty clay loam, 0 to 2 percent slopes	13.7	5.3	0.43	7	1	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	20-40	Good
	ERIE	JtA	Jimtown loam, 0 to 2 percent slopes	15.2	6.4	0.32	5	1	Prime farmland if drained	Somewhat poorly drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Good

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility: Water (K Factor) c/	Erodibility: Wind (WEG) d/	Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
	ERIE	JuA	Joliet silt loam, 0 to 1 percent slopes	3.2	1.2	0.28	6	0.5	Prime farmland if drained	Poorly drained	D	Hydric	High potential for compaction	19	Poor
	ERIE	KbA	Kibbie fine sandy loam, 0 to 2 percent slopes	0.0		0.43	3	0.5	Prime farmland if drained	Somewhat poorly drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Good
	ERIE	KbA	Kibbie fine sandy loam, 0 to 2 percent slopes	50.7	20.0	0.2	3	1	Prime farmland if drained	Somewhat poorly drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Good
	ERIE	MeA	Mermill silty clay loam, 0 to 1 percent slopes	8.0	3.1	0.37	7	0.5	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>80	Good
	ERIE	MfA	Milford silty clay loam, 0 to 1 percent slopes	6.5	2.5	0.28	4	0.5	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>60	Fair
	ERIE	MgA	Millgrove loam, 0 to 1 percent slopes	19.5	7.0	0.24	6	0.5	Prime farmland if drained	Very poorly drained	B/D	Hydric	High potential for compaction	60-80	Fair
	ERIE	MmA	Millsdale silty clay loam, 0 to 1 percent slopes	13.9	5.4	0.28	7	0.5	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	20-40	Fair
	ERIE	MnA	Milton silt loam, 0 to 2 percent slopes	10.3	4.0	0.37	6	1	All areas are prime farmland	Well drained	C	Non-Hydric	Low potential for compaction	40-60	Good

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

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						Water (K Factor) c/	Wind (WEG) d/								
	ERIE	Mn B	Milton silt loam, 2 to 6 percent slopes	1.3	0.6	0.37	6	4	All areas are prime farmland	Well drained	C	Non-Hydric	Low potential for compaction	40-60	Good
	ERIE	MrA	Miner silty clay loam, 0 to 1 percent slopes	2.5	0.9	0.32	7	0.5	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>60	Fair
	ERIE	MsA	Miner silt loam, bedrock substratum, 0 to 1 percent slopes	6.5	2.5	0.32	6	0.5	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>60	Fair
	ERIE	MxA	Mitiwanga silt loam, 0 to 2 percent slopes	5.8	2.3	0.32	6	1	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	20-40	Good
	ERIE	NoA	Nolin silt loam, 0 to 2 percent slopes, occasionally flooded	0.7	0.7	0.43	5	1	All areas are prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>60	Good
	ERIE	OgA	Ogontz fine sandy loam, 0 to 2 percent slopes	3.9	1.4	0.37	3	1	All areas are prime farmland	Moderately well drained	B	Non-Hydric	Moderate potential for compaction	>80	Good
	ERIE	OhB	Ogontz silt loam, 2 to 6 percent slopes	10.1	4.1	0.37	6	4	All areas are prime farmland	Moderately well drained	B	Non-Hydric	Moderate potential for compaction	>80	Good

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

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						Water (K Factor) c/	Wind (WEG) d/								
	ERIE	OpA	Orrville silt loam, bedrock substratum, 0 to 2 percent slopes, occasionally flooded	6.6	2.5	0.37	6	1	Prime farmland if drained	Somewhat poorly drained	B/D	Non-Hydric	Moderate potential for compaction	60-80	Good
	ERIE	OsB	Oshtemo loamy sand, 0 to 6 percent slopes	5.9	2.6	0.17	2	3	All areas are prime farmland	Well drained	A	Non-Hydric	Low potential for compaction	>80	Good
	ERIE	PcA	Pewamo silty clay loam, 0 to 1 percent slopes	21.4	8.1	0.28	7	0.5	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>60	Poor
	ERIE	Pm A	Plumbrook fine sandy loam, 0 to 2 percent slopes	2.0	0.9	0.2	3	1	Prime farmland if drained	Somewhat poorly drained	A/D	Non-Hydric	Moderate potential for compaction	>80	Good
	ERIE	RaA	Randolph silt loam, 0 to 2 percent slopes	2.1	0.7	0.37	6	1	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	20-40	Good
	ERIE	RcA	Rawson sandy loam, 0 to 2 percent slopes	4.0	1.9	0.24	3	1	All areas are prime farmland	Moderately well drained	D	Non-Hydric	Moderate potential for compaction	>60	Good
	ERIE	RcB	Rawson sandy loam, 2 to 6 percent slopes	1.3	0.5	0.24	3	4	All areas are prime farmland	Moderately well drained	D	Non-Hydric	Moderate potential for compaction	>60	Good

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility		Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
						Water (K Factor) c/	Wind (WEG) d/								
	ERIE	RgA	Rimer loamy fine sand, 0 to 2 percent slopes	1.4	0.5	0.32	2	1	Prime farmland if drained	Somewhat poorly drained	A/D	Non-Hydric	Moderate potential for compaction	>80	Fair
	ERIE	RhA	Ritchey loam, 0 to 2 percent slopes	5.9	2.4	0.37	6	1	Not prime farmland	Well drained	D	Non-Hydric	Low potential for compaction	10 to 20	Poor
	ERIE	RhB	Ritchey loam, 2 to 6 percent slopes	0.5	0.0	0.37	6	4	Not prime farmland	Well drained	D	Non-Hydric	Low potential for compaction	10 to 20	Poor
	ERIE	RhC	Ritchey loam, 6 to 12 percent slopes	0.3	0.1		6	9	Not prime farmland	Well drained	D	Non-Hydric	Low potential for compaction	10 to 20	Poor
	ERIE	SbF	Saylesville silt loam, 25 to 40 percent slopes	5.6	3.0	0.37	5	33	Not prime farmland	Well drained	C	Non-Hydric	Low potential for compaction	>60	Fair
	ERIE	ShB	Shinrock silt loam, 2 to 6 percent slopes	4.6	1.8	0.37	6	4	All areas are prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>60	Good
	ERIE	SkC 2	Shinrock silty clay loam, 6 to 12 percent slopes, eroded	5.3	1.9	0.37	7	9	Not prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>60	Good
	ERIE	SkD 2	Shinrock silty clay loam, 12 to 18 percent slopes, eroded	6.0	3.0	0.37	7	15	Not prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>60	Fair

NEXUS GAS TRANSMISSION

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility		Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
						Water (K Factor) c/	Wind (WEG) d/								
	ERIE	SpB	Spinks loamy fine sand, 0 to 6 percent slopes	1.0	0.5	0.17	2	3	Not prime farmland	Well drained	A	Non-Hydric	Low potential for compaction	>100	Fair
	ERIE	TuA	Tuscola fine sandy loam, 0 to 2 percent slopes	8.6	3.0	0.24	3	1	All areas are prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>80	Good
	ERIE	TuB	Tuscola fine sandy loam, 2 to 6 percent slopes	3.3	1.0	0.24	3	4	All areas are prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>80	Good
	ERIE	UcB	Udipsamments -Spinks complex, 0 to 6 percent slopes	5.5	2.4			3	Not prime farmland	Excessively drained		Non-Hydric	Low potential for compaction	>80	
	ERIE	UdB	Udorthents, loamy, 0 to 6 percent slopes	1.7	0.7			3	Not prime farmland					N/A	
	ERIE	W	Water	0.5	0.5			0	Not prime farmland					N/A	
	ERIE	Wa B	Wakeman sandy loam, 2 to 6 percent slopes	2.6	1.0	0.28	3	4	All areas are prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	20-40	Good
	ERIE	Wa C	Wakeman sandy loam, 6 to 12 percent slopes	0.3	0.1	0.28	3	9	Not prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	20-40	Good

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility		Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
						Water (K Factor) c/	Wind (WEG) d/								
	ERIE	ZuC 2	Zurich silt loam, 6 to 12 percent slopes, eroded	0.4	0.2	0.37	6	9	Not prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>80	Good
	ERIE	ZuD 2	Zurich silt loam, 12 to 18 percent slopes, eroded	5.7	2.3	0.37	6	15	Not prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>80	Fair
	ERIE	ZuE 2	Zurich silt loam, 18 to 25 percent slopes, eroded	0.8	0.4	0.37	6	22	Not prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>80	Fair
	ERIE	ZuF	Zurich silt loam, 25 to 40 percent slopes	2.5	1.1	0.37	6	32.5	Not prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>80	Fair
	SANDUSKY	An	Aquents, nearly level	1.2	0.6			1	Not prime farmland	Very poorly drained		Hydric	High potential for compaction	N/A	
	SANDUSKY	BaB	Belmore loam, 2 to 6 percent slopes	7.5	2.3	0.32	5	2	All areas are prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>77	Good
	SANDUSKY	ChB	Castalia very stony loam, 1 to 6 percent slopes	5.6	2.9		8	1	Not prime farmland	Well drained	A	Non-Hydric	Low potential for compaction	20-40	Poor
	SANDUSKY	Co	Colwood fine sandy loam	7.6	3.0	0.43	3	0.5	Prime farmland if drained	Very poorly drained	B/D	Hydric	High potential for compaction	>60	Fair

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility		Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
						Water (K Factor) c/	Wind (WEG) d/								
	SANDUSKY	DeA	Del Rey silt loam, 0 to 2 percent slopes	53.7	21.4	0.43	6	0.2	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	>60	Good
	SANDUSKY	DkA	Dixboro-Kibbie complex, 0 to 2 percent slopes	7.5	2.8	0.2	3	0.2	All areas are prime farmland	Somewhat poorly drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Good
	SANDUSKY	DuB	Dunbridge sandy loam, 1 to 4 percent slopes	4.6	1.8		3	1	All areas are prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	18-42	Fair
	SANDUSKY	GtB	Glenford silt loam, 2 to 6 percent slopes	13.4	4.6	0.37	6	3	All areas are prime farmland	Moderately well drained	C/D	Non-Hydric	Moderate potential for compaction	>60	Good
	SANDUSKY	Gw B	Glynwood silt loam, 2 to 6 percent slopes	8.3	2.9	0.32	6	3	All areas are prime farmland	Moderately well drained	D	Non-Hydric	Moderate potential for compaction	>80	Good
	SANDUSKY	HaB	Haskins sandy loam, 1 to 4 percent slopes	36.9	12.7	0.37	3	1	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	>60	Good
	SANDUSKY	HoA	Hoytville clay loam, 0 to 1 percent slopes	143.6	54.0	0.24	4	0	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>80	Poor
	SANDUSKY	KbA	Kibbie fine sandy loam, 0 to 2 percent slopes	24.0	8.1	0.43	3	0.5	Prime farmland if drained	Somewhat poorly drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Good
	SANDUSKY	Le	Lenawee silty clay loam	83.4	32.3	0.28	6	0.2	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>60	Fair

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility		Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
						Water (K Factor) c/	Wind (WEG) d/								
	SANDUSKY	Me B	Mentor silt loam, 1 to 4 percent slopes	7.6	3.4	0.37	5	3	All areas are prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>60	Good
	SANDUSKY	Mo	Mermill loam	8.4	3.6	0.28	5	0.5	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>80	Good
	SANDUSKY	Ms	Millsdale silty clay loam	18.1	6.9		6	0.5	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	20-40	Fair
	SANDUSKY	NpA	Nappanee silt loam, 0 to 3 percent slopes	42.9	15.4	0.37	6	0.2	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>60	Good
	SANDUSKY	RoB	Rimer loamy fine sand, 1 to 4 percent slopes	6.5	2.6	0.32	2	3	Prime farmland if drained	Somewhat poorly drained	A/D	Non-Hydric	Moderate potential for compaction	>80	Fair
	SANDUSKY	Rs	Rossburg silt loam, occasionally flooded	0.6	0.4	0.24	6	0.5	All areas are prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>60	Good
	SANDUSKY	SbC 2	Saylesville silty clay loam, 6 to 12 percent slopes, eroded	1.2	0.5	0.37	6	6	Not prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>60	Good
	SANDUSKY	Sh	Shoals silt loam, frequently flooded	7.5	2.8	0.24	6	0.2	Not prime farmland	Somewhat poorly drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Fair

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility		Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
						Water (K Factor) c/	Wind (WEG) d/								
	SANDUSKY	SoB	Spinks fine sand, 2 to 6 percent slopes	6.4	1.2	0.1	1	3	Not prime farmland	Well drained	A	Non-Hydric	Low potential for compaction	>100	Fair
	SANDUSKY	To	Toledo silty clay	6.2	2.3	0.28	4	0.2	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>80	Fair
	SANDUSKY	Tp	Toledo silty clay loam, ponded	0.3	0.3	0.28	4	0.2	Not prime farmland	Very poorly drained	C/D	Hydric	High potential for compaction	>80	Poor
	SANDUSKY	W	Water	0.6	0.6			0	Not prime farmland					N/A	
	WOOD	Am A	Aurand fine sandy loam, 0 to 2 percent slopes	1.6	0.7	0.24	3	1	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	>80	Good
	WOOD	AnA	Aurand loam, 0 to 2 percent slopes	5.4	1.9	0.32	5	1	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	>80	Good
	WOOD	CbB	Castalia-Marblehead complex, very stony, 0 to 6 percent slopes	11.5	5.1		8	3	Not prime farmland	Well drained	A	Non-Hydric	Low potential for compaction	20-40	Poor
	WOOD	DsB	Dunbridge-Spinks, deep to limestone, loamy fine sands, 2 to 6 percent slopes	3.0	1.5	0.2	2	3	Not prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	18-42	Fair

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility		Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
						Water (K Factor) c/	Wind (WEG) d/								
	WOOD	HoA	Hoytville clay loam, 0 to 1 percent slopes	0.0	0.0	0.24	4	0	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>80	Poor
	WOOD	HoA	Hoytville clay loam, 0 to 1 percent slopes	199.0	75.1	0.24	4	0	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>80	Poor
	WOOD	JoA	Joliet silty clay loam, 0 to 1 percent slopes	0.8	0.5		6	0.2	Not prime farmland	Poorly drained	D	Hydric	High potential for compaction	19	Poor
	WOOD	MfA	Mermill-Aurand complex, 0 to 1 percent slopes	23.5	8.0	0.28	6	0.5	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>80	Poor
	WOOD	Mh A	Millsdale silty clay loam, 0 to 1 percent slopes	4.7	2.0		6	0.5	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	20-40	Poor
	WOOD	Nm A	Nappanee sandy loam, 0 to 2 percent slopes	2.9	1.2	0.37	3	0.5	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>60	Good
	WOOD	NnA	Nappanee loam, 0 to 2 percent slopes	8.8	3.2	0.37	6	0.5	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>60	Good
	WOOD	NnB	Nappanee loam, 2 to 6 percent slopes	2.1	0.7	0.37	6	2	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>60	Good
	WOOD	NpA	Nappanee silty clay loam, 0 to 2 percent slopes	0.2	0.2	0.37	6	0.5	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>60	Good

TABLE 7.2-2

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						Water (K Factor) c/	Wind (WEG) d/								
	WOOD	NpA	Nappanee silt loam, 0 to 3 percent slopes	0.0	0.0	0.37	6	0.2	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>60	Good
	WOOD	NpB	Nappanee silty clay loam, 2 to 6 percent slopes	0.9	0.3	0.43	6	2	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>60	Good
	WOOD	NpB 2	Nappanee silty clay loam, 2 to 6 percent slopes, eroded	0.5	0.1	0.37	6	2	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>60	Good
	WOOD	RbA	Randolph loam, 0 to 2 percent slopes	5.6	2.5		6	0.5	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	20-40	Good
	WOOD	SdA	Seward and Ottokee, till substratum, loamy fine sands, 0 to 2 percent slopes	1.9	0.9	0.32	2	0.5	Not prime farmland	Moderately well drained	A	Non-Hydric	Moderate potential for compaction	>80	Fair
	WOOD	SnA	Sloan silt loam, 0 to 1 percent slopes, frequently flooded	0.5	0.2	0.32	6	0.2	Prime farmland if drained and either protected from flooding or not frequently flooded during the growing season	Very poorly drained	B/D	Hydric	High potential for compaction	>60	Poor

TABLE 7.2-2

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	WOOD	SpA	Sloan silty clay loam, 0 to 1 percent slopes, frequently flooded	1.3	0.5	0.28	6	0.2	Prime farmland if drained and either protected from flooding or not frequently flooded during the growing season	Very poorly drained	B/D	Hydric	High potential for compaction	>60	Poor
	WOOD	StC 2	St. Clair loam, 6 to 12 percent slopes, eroded	0.2	0.1	0.32	6	8	Not prime farmland	Moderately well drained	D	Non-Hydric	Moderate potential for compaction	>48	Good
	WOOD	SuD 2	St. Clair silty clay loam, 12 to 18 percent slopes, eroded	1.0	0.4	0.43	6	14	Not prime farmland	Moderately well drained	D	Non-Hydric	Moderate potential for compaction	>48	Fair
	WOOD	SuE 2	St. Clair silty clay loam, 18 to 25 percent slopes, eroded	0.4	0.2	0.43	6	20	Not prime farmland	Moderately well drained	D	Non-Hydric	Moderate potential for compaction	>48	Fair
	WOOD	W	Water	0.0	0.0			0	Not prime farmland					N/A	
	WOOD	W	Water	0.5	0.5			0	Not prime farmland					N/A	
	LUCAS	BxA	Bixler loamy fine sand, 0 to 2 percent slopes	8.2	2.0	0.17	2	1	Prime farmland if drained	Somewhat poorly drained	B	Non-Hydric	Moderate potential for compaction	>80	Fair

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						Water (K Factor) c/	Wind (WEG) d/								
	LUCAS	BxB	Bixler loamy fine sand, 2 to 6 percent slopes	3.5	1.4	0.17	2	4	Prime farmland if drained	Somewhat poorly drained	B	Non-Hydric	Moderate potential for compaction	>80	Fair
	LUCAS	Co	Colwood loam	15.4	6.3	0.28	5	1	Prime farmland if drained	Very poorly drained	B/D	Hydric	High potential for compaction	>60	Fair
	LUCAS	DdA	Del Rey loam, 0 to 3 percent slopes	4.7	1.9	0.43	6	2	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	>60	Good
	LUCAS	DgA	Digby sandy loam, 0 to 2 percent slopes	2.1	1.0	0.24	3	1	Prime farmland if drained	Somewhat poorly drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Good
	LUCAS	DsA	Dixboro fine sandy loam, 0 to 2 percent slopes	0.5	0.2	0.2	3	1	All areas are prime farmland	Somewhat poorly drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Good
	LUCAS	Ee	Eel loam, occasionally flooded	0.6	0.6	0.37	6	1	All areas are prime farmland	Moderately well drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Good
	LUCAS	Gr	Granby loamy fine sand	9.4	3.6	0.17	2	1	Not prime farmland	Very poorly drained	A/D	Hydric	High potential for compaction	>80	Poor
	LUCAS	HnA	Haskins loam, 0 to 3 percent slopes	7.6	2.9	0.37	5	2	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	>60	Good
	LUCAS	HoA	Hoytville clay loam, 0 to 1 percent slopes	1.2	0.5	0.24	4	0	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>80	Poor

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						Water (K Factor) c/	Wind (WEG) d/								
	LUCAS	La	Lamson fine sandy loam	9.0	2.6	0.28	3	1	Prime farmland if drained	Very poorly drained	A/D	Hydric	High potential for compaction	>60	Poor
	LUCAS	Mf	Mermill loam	31.9	12.0	0.32	6	1	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>80	Fair
	LUCAS	Mm A	Metamora sandy loam, 0 to 3 percent slopes	1.9	1.0	0.2	3	2	Prime farmland if drained	Somewhat poorly drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Good
	LUCAS	NnA	Nappanee loam, 0 to 3 percent slopes	0.5	0.2	0.37	6	2	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>60	Good
	LUCAS	OtB	Ottokee fine sand, 0 to 6 percent slopes	16.2	5.8	0.15	1	3	Not prime farmland	Moderately well drained	A	Non-Hydric	Moderate potential for compaction	>80	Fair
	LUCAS	RnA	Rimer loamy fine sand, 0 to 3 percent slopes	1.1	0.4	0.17	2	2	Prime farmland if drained	Somewhat poorly drained	A/D	Non-Hydric	Moderate potential for compaction	>80	Fair
	LUCAS	SdB	Seward loamy fine sand, 2 to 6 percent slopes	0.9	0.3	0.17	2	4	All areas are prime farmland	Moderately well drained	A	Non-Hydric	Moderate potential for compaction	>80	Good
	LUCAS	Sh	Shoals loam, occasionally flooded	0.1	0.1	0.24	6	1	Prime farmland if drained	Somewhat poorly drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Fair
	LUCAS	Sm C	Sisson loam, 6 to 12 percent slopes	0.7	0.3	0.32	5	9	Not prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>60	Good

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						Water (K Factor) c/	Wind (WEG) d/								
	LUCAS	So	Sloan loam, occasionally flooded	1.5	0.5	0.28	6	1	Prime farmland if drained	Very poorly drained	B/D	Hydric	High potential for compaction	>60	Poor
	LUCAS	SuC 2	St. Clair silty clay loam, 4 to 12 percent slopes, eroded	0.3	0.3	0.43	6	8	Not prime farmland	Moderately well drained	D	Non-Hydric	Moderate potential for compaction	>48	Good
	LUCAS	SuE 3	St. Clair silty clay loam, 12 to 25 percent slopes, severely eroded	0.1	0.1	0.43	6	18	Not prime farmland	Moderately well drained	D	Non-Hydric	Moderate potential for compaction	>48	Fair
	LUCAS	TdA	Tedrow fine sand, 0 to 3 percent slopes	6.6	2.1	0.15	1	2	Not prime farmland	Somewhat poorly drained	A/D	Non-Hydric	Moderate potential for compaction	>60	Fair
	LUCAS	W	Water	1.0	1.0			0	Not prime farmland					N/A	
	LUCAS	W	Water	0.0	0.0			0	Not prime farmland					N/A	
	HENRY	Gr	Granby loamy fine sand	6.1	2.6	0.17	2	1	Not prime farmland	Very poorly drained	A/D	Hydric	High potential for compaction	>80	Poor
	HENRY	Gr	Granby loamy fine sand	0.0	0.0	0.17	2	1	Not prime farmland	Very poorly drained	A/D	Hydric	High potential for compaction	>80	Poor
	HENRY	Oa C	Oakville fine sand, 2 to 12 percent slopes	0.4	0.2	0.15	1	7	Not prime farmland	Well drained	A	Non-Hydric	Low potential for compaction	>80	Poor

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	HENRY	OtB	Ottokee fine sand, 1 to 5 percent slopes	5.2	2.1	0.15	1	3	Not prime farmland	Moderately well drained	A	Non-Hydric	Moderate potential for compaction	>80	Fair
	HENRY	OuB	Ottokee fine sand, 0 to 6 percent slopes	0.3	0.2	0.15	1	3	Not prime farmland	Moderately well drained	A	Non-Hydric	Moderate potential for compaction	>80	Fair
	HENRY	TdA	Tedrow loamy fine sand, 0 to 2 percent slopes	1.2	0.4	0.17	2	1	Not prime farmland	Somewhat poorly drained	A/D	Non-Hydric	Moderate potential for compaction	>60	Fair
	FULTON	CoB	Colonie fine sand, 1 to 6 percent slopes	2.8	1.0	0.15	1	4	Not prime farmland	Well drained	A	Non-Hydric	Low potential for compaction	>80	Fair
	FULTON	CoC	Colonie fine sand, 6 to 12 percent slopes	1.3	0.5	0.1	1	9	Not prime farmland	Somewhat excessively drained	A	Non-Hydric	Low potential for compaction	>80	Fair
	FULTON	Dm A	Digby loam, 0 to 3 percent slopes	5.2	1.5	0.32	5	2	Prime farmland if drained	Somewhat poorly drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Good
	FULTON	Gf	Gilford fine sandy loam	8.2	3.0	0.1	3	1	Prime farmland if drained	Very poorly drained	A/D	Hydric	High potential for compaction	>80	Poor
	FULTON	Gr	Granby loamy fine sand	0.0	0.0	0.17	2	1	Not prime farmland	Very poorly drained	A/D	Hydric	High potential for compaction	>80	Poor
	FULTON	Gr	Granby loamy fine sand	40.3	15.7	0.17	2	1	Farmland of local importance	Very poorly drained	A/D	Hydric	High potential for compaction	>80	Poor

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility		Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
						Water (K Factor) c/	Wind (WEG) d/								
	FULTON	HkA	Haskins loam, 0 to 3 percent slopes	12.6	4.7	0.37	5	2	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	>60	Good
	FULTON	HoA	Hoytville clay loam, 0 to 1 percent slopes	108.8	41.2	0.24	4	0	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>80	Poor
	FULTON	Mf	Mermill loam	11.3	4.2	0.32	5	1	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>80	Good
	FULTON	Mo	Millgrove loam	3.2	0.9	0.28	6	1	Prime farmland if drained	Very poorly drained	B/D	Hydric	High potential for compaction	60-80	Poor
	FULTON	NnA	Nappanee loam, 0 to 2 percent slopes	22.6	8.0	0.37	6	1	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>60	Good
	FULTON	NnB	Nappanee loam, 2 to 6 percent slopes	0.7	0.3	0.37	6	4	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>60	Good
	FULTON	OaB	Oakville fine sand, 0 to 6 percent slopes	0.0	0.0	0.15	1	3	Not prime farmland	Well drained	A	Non-Hydric	Low potential for compaction	>80	Poor
	FULTON	OtB	Ottokee fine sand, 0 to 6 percent slopes	33.1	13.2	0.15	1	3	Farmland of local importance	Moderately well drained	A	Non-Hydric	Moderate potential for compaction	>80	Fair
	FULTON	RnA	Rimer loamy fine sand, 0 to 3 percent slopes	1.8	0.7	0.32	2	2	Prime farmland if drained	Somewhat poorly drained	A/D	Non-Hydric	Moderate potential for compaction	>80	Fair

NEXUS GAS TRANSMISSION

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility		Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
						Water (K Factor) c/	Wind (WEG) d/								
	FULTON	SdB	Seward loamy fine sand, 2 to 6 percent slopes	1.4	0.5	0.17	2	4	Farmland of local importance	Moderately well drained	A	Non-Hydric	Moderate potential for compaction	>80	Fair
	FULTON	Sh	Shoals silt loam, frequently flooded	2.4	0.8	0.24	6	1	Prime farmland if drained and either protected from flooding or not frequently flooded during the growing season	Somewhat poorly drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Fair
	FULTON	So	Sloan silty clay loam, frequently flooded	6.0	2.1	0.28	6	1	Prime farmland if drained and either protected from flooding or not frequently flooded during the growing season	Very poorly drained	B/D	Hydric	High potential for compaction	>60	Fair
	FULTON	TdA	Tedrow loamy fine sand, 0 to 3 percent slopes	21.4	8.3	0.17	2	2	Farmland of local importance	Somewhat poorly drained	A/D	Non-Hydric	Moderate potential for compaction	>60	Fair

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility		Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
						Water (K Factor) c/	Wind (WEG) d/								
	FULTON	Zie5 A	Ziegenfuss clay loam, 0 to 1 percent slopes	8.2	1.9	0.24	6	0.3	Prime farmland if drained	Poorly drained	C/D	Hydric	High potential for compaction	>80	Fair
Michigan															
Mainline															
	LENAWEE	BcA	Berrien sandy loam, 0 to 3 percent slopes	0.6	0.3	0.17	2	2	Farmland of local importance	Moderately well drained	A	Non-Hydric	Moderate potential for compaction	>60	Poor
	LENAWEE	BhA	Brady sandy loam, 0 to 3 percent slopes	3.7	1.5	0.2	3	2	All areas are prime farmland	Somewhat poorly drained	B	Non-Hydric	Moderate potential for compaction	>80	Good
	LENAWEE	BkA	Brady and Macomb loams, 0 to 3 percent slopes	84.6	32.0	0.28	5	2	All areas are prime farmland	Somewhat poorly drained	B	Non-Hydric	Moderate potential for compaction	>60	Good
	LENAWEE	GaA	Genesee loam, 0 to 3 percent slopes	2.7	0.9	0.37	5	1	All areas are prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>60	Good
	LENAWEE	HfA	Hoytville and Wauseon loams, 0 to 3 percent slopes	6.9	2.6	0.28	6	1	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>60	Fair
	LENAWEE	Le	Lenawee silty clay loam	10.6	4.3	0.28	7	1	Prime farmland if drained	Poorly drained	B/D	Hydric	High potential for compaction	>60	Poor

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility		Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
						Water (K Factor) c/	Wind (WEG) d/								
	LENAWEE	Ma A	Macomb fine sandy loam, 0 to 3 percent slopes	3.3	1.0	0.2	3	2	Prime farmland if drained	Somewhat poorly drained	B	Non-Hydric	Moderate potential for compaction	>60	Good
	LENAWEE	NaA	Nappanee silt loam, 0 to 3 percent slopes	4.3	1.6	0.37	6	2	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>60	Good
	LENAWEE	PdA	Plainfield and Berrien loamy sands, 0 to 3 percent slopes	1.7	0.5	0.17	2	2	Not prime farmland	Moderately well drained	A	Non-Hydric	Moderate potential for compaction	>60	Poor
	LENAWEE	SbA	Sebewa sandy loam, 0 to 3 percent slopes	1.2	0.5	0.2	3	2	Prime farmland if drained	Poorly drained	B/D	Hydric	High potential for compaction	>80	Poor
	LENAWEE	SdD 2	St. Clair loam, 12 to 25 percent slopes, moderately eroded	1.6	0.8	0.37	6	19	Not prime farmland	Moderately well drained	D	Non-Hydric	Moderate potential for compaction	>48	Fair
	LENAWEE	W	Water	0.1	0.1			0	Not prime farmland					N/A	
	LENAWEE	Wc A	Wauseon loam, 0 to 3 percent slopes	31.1	11.8	0.28	5	1	Prime farmland if drained	Poorly drained	B/D	Hydric	High potential for compaction	>60	Fair
	LENAWEE	Zfsa cA	Ziegenfuss clay loam, 0 to 1 percent slopes	199.0	74.6	0.24	6	0.3	Prime farmland if drained	Poorly drained	C/D	Hydric	High potential for compaction	>80	Fair

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility		Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
						Water (K Factor) c/	Wind (WEG) d/								
	MONROE	100 A	Hoytville and Wauseon loams, 0 to 3 percent slopes	15.0	5.7	0.28	5	1	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>60	Fair
	MONROE	103 A	Ypsi sandy loam, 0 to 4 percent slopes	3.5	1.4	0.2	3	2	Prime farmland if drained	Somewhat poorly drained	C	Non-Hydric	Moderate potential for compaction	>60	Good
	MONROE	13A	Blount loam, 0 to 3 percent slopes	3.9	1.7	0.43	6	2	Prime farmland if drained	Somewhat poorly drained	C	Non-Hydric	Moderate potential for compaction	>79	Good
	MONROE	22	Pewamo clay loam	10.4	4.0	0.24	6	1	Prime farmland if drained	Poorly drained	C/D	Hydric	High potential for compaction	>60	Poor
	MONROE	23A	Metamora sandy loam, 0 to 3 percent slopes	5.3	1.8	0.2	3	2	Prime farmland if drained	Somewhat poorly drained	B	Non-Hydric	Moderate potential for compaction	>60	Good
	MONROE	24	Corunna sandy loam	1.0	0.4	0.24	3	1	Prime farmland if drained	Poorly drained	B/D	Hydric	High potential for compaction	>60	Poor
	MONROE	30	Sloan loam	0.6	0.3	0.28	6	1	Not prime farmland	Very poorly drained	B/D	Hydric	High potential for compaction	>60	Fair
	MONROE	40A	Thetford loamy sand, 0 to 3 percent slopes	0.5	0.2	0.17	2	2	Farmland of local importance	Somewhat poorly drained	A	Non-Hydric	Moderate potential for compaction	>66	Fair
	MONROE	43A	Nappanee loam, 0 to 3 percent slopes	33.3	12.2	0.37	6	2	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>60	Good

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility: Water (K Factor) c/	Erodibility: Wind (WEG) d/	Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
	MONROE	49B	Oakville fine sand, loamy substratum, 0 to 6 percent slopes	1.6	0.6	0.15	1	3	Not prime farmland	Moderately well drained	A	Non-Hydric	Moderate potential for compaction	>80	Poor
	MONROE	YpA	Ypsi sandy loam, 0 to 4 percent slopes	0.0	0.0	0.2	3	2	Prime farmland if drained	Somewhat poorly drained	C	Non-Hydric	Moderate potential for compaction	>60	Good
	MONROE	Zfsa cA	Ziegenfuss clay loam, 0 to 1 percent slopes	0.0	0.0	0.24	6	0.3	Prime farmland if drained	Poorly drained	C/D	Hydric	High potential for compaction	>80	Fair
	MONROE	Zfsa cA	Ziegenfuss clay loam, 0 to 1 percent slopes	28.9	10.8	0.24	6	0.3	Prime farmland if drained	Poorly drained	C/D	Hydric	High potential for compaction	>80	Fair
	WASHTENAW	BnB	Boyer loamy sand, 0 to 6 percent slopes	33.4	10.2	0.17	2	3	Farmland of local importance	Well drained	B	Non-Hydric	Low potential for compaction	>60	Fair
	WASHTENAW	Cc	Cohoctah fine sandy loam, frequently flooded	2.5	1.6	0.24	3	1	Not prime farmland	Poorly drained	B/D	Hydric	High potential for compaction	>80	Poor
	WASHTENAW	CoB	Conover loam, 0 to 4 percent slopes	0.3	0.0	0.28	5	2	Prime farmland if drained	Somewhat poorly drained	C	Non-Hydric	Moderate potential for compaction	>60	Good
	WASHTENAW	DoA	Dixboro-Kibbie fine sandy loams, 0 to 4 percent slopes	0.5	0.3	0.2	3	2	Prime farmland if drained	Somewhat poorly drained	B	Non-Hydric	Moderate potential for compaction	>60	Good

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility: Water (K Factor) c/	Erodibility: Wind (WEG) d/	Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
	WASHTENAW	FoA	Fox sandy loam, 0 to 2 percent slopes	1.3	0.6	0.24	3	1	All areas are prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>80	Good
	WASHTENAW	Gf	Gilford sandy loam	27.2	11.4	0.2	3	1	Not prime farmland	Very poorly drained	B/D	Hydric	High potential for compaction	>80	Fair
	WASHTENAW	KeB	Kendallville loam, 2 to 6 percent slopes	0.5	0.2	0.37	6	4	All areas are prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>60	Good
	WASHTENAW	KnA	Kibbie fine sandy loam, 0 to 4 percent slopes	6.2	2.4	0.2	3	2	Prime farmland if drained	Somewhat poorly drained	B	Non-Hydric	Moderate potential for compaction	>60	Good
	WASHTENAW	MaA	Macomb loam, 0 to 4 percent slopes	2.6	1.3	0.28	5	2	Prime farmland if drained	Somewhat poorly drained	B	Non-Hydric	Moderate potential for compaction	>60	Good
	WASHTENAW	MoB	Morley loam, 2 to 6 percent slopes	0.1	0.0	0.37	6	4	All areas are prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>80	Good
	WASHTENAW	NaA	Nappanee silty clay loam, 0 to 2 percent slopes	9.5	3.6	0.37	7	1	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>60	Good
	WASHTENAW	NaB	Nappanee silty clay loam, 2 to 6 percent slopes	2.5	1.0	0.43	7	4	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>60	Good

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility		Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
						Water (K Factor) c/	Wind (WEG) d/								
	WASHTENAW	OsB	Oshtemo loamy sand, 0 to 6 percent slopes	2.2	0.9	0.17	2	3	All areas are prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>80	Fair
	WASHTENAW	Ow B	Owosso-Miami complex, 2 to 6 percent slopes	0.6	0.3	0.24	3	4	All areas are prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>60	Good
	WASHTENAW	Pc	Pella silt loam	11.3	4.3	0.28	6	1	Prime farmland if drained	Poorly drained	B/D	Hydric	High potential for compaction	>60	Good
	WASHTENAW	Sc	Sloan loam	1.7	0.9	0.28	6	1	Not prime farmland	Very poorly drained	B/D	Hydric	High potential for compaction	>60	Fair
	WASHTENAW	SfB	Seward sandy loam, loamy subsoil variant, 2 to 6 percent slopes	3.9	1.7	0.24	3	4	Farmland of local importance	Moderately well drained	B	Non-Hydric	Moderate potential for compaction	>80	Fair
	WASHTENAW	SnB	Sisson fine sandy loam, 2 to 6 percent slopes	1.8	0.7	0.37	3	4	All areas are prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>60	Good
	WASHTENAW	SpB	Spinks loamy sand, 0 to 6 percent slopes	14.2	5.5	0.15	2	3	Farmland of local importance	Well drained	A	Non-Hydric	Low potential for compaction	>100	Fair
	WASHTENAW	W	Water	0.5	0.3			0	Not prime farmland					N/A	
	WASHTENAW	Wa A	Wasepi sandy loam, 0 to 4 percent slopes	101.2	37.2	0.2	3	2	Farmland of local importance	Somewhat poorly drained	B	Non-Hydric	Moderate potential for compaction	>60	Good

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	**County**	**Map Unit**	**Soil Association/ Series/ Complex**	**Project Work Area (acres) a/**	**Permanent ROW Area (acres) b/**	**Erodibility**		**Slope Percent e/' f/**	**Prime Farmland Soils Designation g/**	**Drainage Class**	**Dominant Hydrologic Group**	**Hydric h/**	**Compaction Potential i/**	**Average Approximate Depth to Bedrock (inches) j/**	**Re-vegetation Potential k/**
						Water (K Factor) c/	**Wind (WEG) d/**								
	WASHTENAW	Wb A	Wasepi sandy loam, loamy substratum, 0 to 3 percent slopes	0.0	0.0	0.2	3	2	Farmland of local importance	Somewhat poorly drained	B	Non-Hydric	Moderate potential for compaction	>60	Fair
	WASHTENAW	Ws	Wauseon fine sandy loam	12.0	4.5	0.2	3	1	Prime farmland if drained	Very poorly drained	B/D	Hydric	High potential for compaction	>60	Fair
	WASHTENAW	YpA	Ypsi sandy loam, 0 to 4 percent slopes	35.5	13.5	0.2	3	2	Prime farmland if drained	Somewhat poorly drained	C	Non-Hydric	Moderate potential for compaction	>60	Good
	WASHTENAW	Zfsa cA	Ziegenfuss clay loam, 0 to 1 percent slopes	15.7	6.2	0.24	6	0.3	Prime farmland if drained	Poorly drained	C/D	Hydric	High potential for compaction	>80	Fair
			TGP Subtotal:	*11.2*	*5.4*										
			NEXUS Subtotal:	*3877.9*	*1505.5*										
Ohio															
Hanoverton Compressor Station (CS-1)															
	COLUMBIANA	BkE	Berks channery silt loam, 25 to 40 percent slopes	0.0			6	32.5	Not prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	20-40	Fair
	COLUMBIANA	FcD	Fairpoint silty clay loam, 8 to 25 percent slopes	18.2		0.43	6	16.5	Not prime farmland	Well drained	C	Non-Hydric	Low potential for compaction	>60	Poor

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility		Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
						Water (K Factor) c/	Wind (WEG) d/								
	COLUMBIANA	FoB	Fredericktown silt loam, 2 to 6 percent slopes	23.3	9.5	0.32	5	4	All areas are prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>80	Good
	COLUMBIANA	Gn C	Gilpin silt loam, 6 to 15 percent slopes	3.5	0.1		6	10.5	Not prime farmland	Well drained	C	Non-Hydric	Low potential for compaction	20-40	Good
	COLUMBIANA	Gn D	Gilpin silt loam, 15 to 25 percent slopes	7.9	0.5	0.24	6	20	Not prime farmland	Well drained	C	Non-Hydric	Low potential for compaction	20-40	Fair
	COLUMBIANA	KnC	Kensington silt loam, 6 to 15 percent slopes	9.7	2.1		6	10.5	Not prime farmland	Moderately well drained	B	Non-Hydric	Moderate potential for compaction	>60	Good
	COLUMBIANA	KnD	Kensington silt loam, 15 to 25 percent slopes	16.0	4.8		6	20	Not prime farmland	Moderately well drained	B	Non-Hydric	Moderate potential for compaction	>60	Fair
	COLUMBIANA	TeC	Teegarden silt loam, 6 to 15 percent slopes	20.0	11.5	0.37	6	10.5	Not prime farmland	Moderately well drained	C/D	Non-Hydric	Moderate potential for compaction	>60	Good
	COLUMBIANA	TeC 2	Teegarden silt loam, 6 to 15 percent slopes, eroded	1.0		0.37	6	10.5	Not prime farmland	Moderately well drained	C/D	Non-Hydric	Moderate potential for compaction	>60	Good
Wadsworth Compressor Station (CS-2)															
	MEDINA	RsB	Rittman silt loam, 2 to 6 percent slopes	40.7	15.1	0.43	5	3	All areas are prime farmland	Moderately well drained	D	Non-Hydric	Moderate potential for compaction	40-60	Good

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility		Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
						Water (K Factor) c/	Wind (WEG) d/								
	MEDINA	RsC 2	Rittman silt loam, 6 to 12 percent slopes, moderately eroded	2.9		0.43	5	10	Farmland of local importance	Moderately well drained	D	Non-Hydric	Moderate potential for compaction	40-60	Good
	MEDINA	Ud	Udorthents, loamy	0.2				3	Not prime farmland					N/A	
	MEDINA	Wa A	Wadsworth silt loam, 0 to 2 percent slopes	15.5	4.4	0.43	6	2	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>60	Good
	MEDINA	Wa B	Wadsworth silt loam, 2 to 6 percent slopes	4.4	0.4	0.43	6	3	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>60	Good
Clyde Compressor Station (CS-3)															
	SANDUSKY	BaB	Belmore loam, 2 to 6 percent slopes	0.3	0.2	0.32	5	2	All areas are prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>77	Good
	SANDUSKY	HaB	Haskins sandy loam, 1 to 4 percent slopes	3.6	1.1	0.37	3	1	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	>60	Good
	SANDUSKY	KbA	Kibbie fine sandy loam, 0 to 2 percent slopes	27.0	24.1	0.43	3	0.5	Prime farmland if drained	Somewhat poorly drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Good
	SANDUSKY	Le	Lenawee silty clay loam	29.8	23.2	0.28	6	0.2	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>60	Fair
Waterville Compressor Station (CS-4)															

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility: Water (K Factor) c/	Erodibility: Wind (WEG) d/	Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
	LUCAS	Mf	Mermill loam	20.3	18.5	0.32	6	1	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>80	Fair
	LUCAS	Mm A	Metamora sandy loam, 0 to 3 percent slopes	14.6	14.1	0.2	3	2	Prime farmland if drained	Somewhat poorly drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Good
	LUCAS	RnA	Rimer loamy fine sand, 0 to 3 percent slopes	2.6	2.4	0.17	2	2	Prime farmland if drained	Somewhat poorly drained	A/D	Non-Hydric	Moderate potential for compaction	>80	Fair
Ohio															
MR01 (TGP)															
	COLUMBIANA	BkB	Berks channery silt loam, 2 to 6 percent slopes	3.1	0.7	0.17	6	4	All areas are prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	20-40	Fair
	COLUMBIANA	BkD	Berks channery silt loam, 15 to 25 percent slopes	5.3	1.4		6	20	Not prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	20-40	Fair
	COLUMBIANA	CoC	Coshocton silt loam, 6 to 15 percent slopes	0.6			5	10.5	Not prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	40-84	Good
MR02&3 (Kensington/OPEN)															
	COLUMBIANA	BkB	Berks channery silt loam, 2 to 6 percent slopes	3.1	0.7	0.17	6	4	All areas are prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	20-40	Fair

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility		Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
						Water (K Factor) c/	Wind (WEG) d/								
	COLUMBIANA	BkD	Berks channery silt loam, 15 to 25 percent slopes	5.3	1.4		6	20	Not prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	20-40	Fair
	COLUMBIANA	CoC	Coshocton silt loam, 6 to 15 percent slopes	0.6			5	10.5	Not prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	40-84	Good
	COLUMBIANA	OrA	Orrville silt loam, 0 to 2 percent slopes, occasionally flooded	0.7		0.37	6	1	Prime farmland if drained	Somewhat poorly drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Good
Michigan															
MR04 (DTE / WillowRun)															
	WASHTENAW	Wa A	Wasepi sandy loam, 0 to 4 percent slopes	2.6	2.1	0.2	3	2	Farmland of local importance	Somewhat poorly drained	B	Non-Hydric	Moderate potential for compaction	>60	Good
			MR01	9.0	2.1										
			MR02&3	9.7	2.1										
			MR04	2.6	2.1										
Ohio															
Yard 1-1															
	STARK	Wa B	Wadsworth silt loam, 2 to 6 percent slopes	22.7	0	0.43	6	4	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>60	Good

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility		Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
						Water (K Factor) c/	Wind (WEG) d/								
	STARK	Se	Sebring silt loam, till substratum	3.6	0	0.37	6	1	Prime farmland if drained	Poorly drained	C/D	Hydric	High potential for compaction	>60	Fair
	STARK	Wa A	Wadsworth silt loam, 0 to 2 percent slopes	2.0	0	0.43	6	1	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>60	Good
	STARK	Wa C2	Wadsworth silt loam, 6 to 12 percent slopes, moderately eroded	10.9	0	0.43	6	9	Not prime farmland	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>60	Good
Yard 2-1															
	ERIE	CoA	Condit silt loam, 0 to 1 percent slopes	2.5	0	0.37	6	0.5	Prime farmland if drained	Poorly drained	C/D	Hydric	High potential for compaction	>80	
	ERIE	JtA	Jimtown loam, 0 to 2 percent slopes	3.3	0	0.32	5	1	Prime farmland if drained	Somewhat poorly drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Good
	ERIE	Mg A	Millgrove loam, 0 to 1 percent slopes	0.1	0	0.24	6	0.5	Prime farmland if drained	Very poorly drained	B/D	Hydric	High potential for compaction	60-80	Fair
	ERIE	BgA	Bennington silt loam, 0 to 2 percent slopes	40.6	0	0.43	6	1	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	>80	Good
	ERIE	CaB	Cardington silt loam, 2 to 6 percent slopes	8.0	0	0.37	6	4	All areas are prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	78	Good
Yard 3-1															

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility		Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
						Water (K Factor) c/	Wind (WEG) d/								
	WOOD	AnA	Aurand loam, 0 to 2 percent slopes	0.6	0	0.32	5	1	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	>80	Good
	WOOD	HoA	Hoytville clay loam, 0 to 1 percent slopes	61.6	0	0.24	4	0	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>80	Poor
	WOOD	MfA	Mermill-Aurand complex, 0 to 1 percent slopes	16.6	0	0.28	6	0.5	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>80	Poor
Yard 3-2															
	LUCAS	HnA	Haskins loam, 0 to 3 percent slopes	4.5	0	0.37	5	2	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	>60	Good
	LUCAS	Co	Colwood loam	3.9	0	0.28	5	1	Prime farmland if drained	Very poorly drained	B/D	Hydric	High potential for compaction	>60	Fair
	LUCAS	DdA	Del Rey loam, 0 to 3 percent slopes	5.5	0	0.43	6	2	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	>60	Good
	LUCAS	DsA	Dixboro fine sandy loam, 0 to 2 percent slopes	4.8	0	0.2	3	1	All areas are prime farmland	Somewhat poorly drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Good
	LUCAS	FuA	Fulton silty clay loam, 0 to 2 percent slopes	8.5	0	0.32	6	1	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction		Good
	LUCAS	Lf	Lenawee silty clay loam	0.2	0	0.28	6	1	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction		Fair

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility		Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
						Water (K Factor) c/	Wind (WEG) d/								
	LUCAS	To	Toledo silty clay	42.9	0	0.28	4	1	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction		Poor
Michigan															
Yard 4-1															
	LENAWEE	112 A	Wauseon loam, 0 to 3 percent slopes	0.1	0	0.28	5	1	Prime farmland if drained	Poorly drained	B/D	Hydric	High potential for compaction		Fair
	LENAWEE	22	Pewamo clay loam	0.1	0	0.24	6	1	Prime farmland if drained	Poorly drained	C/D	Hydric	High potential for compaction	>60	Poor
	LENAWEE	Pm	Pewamo clay loam	42.2	0	0.24	6	1	Prime farmland if drained	Poorly drained	C/D	Hydric	High potential for compaction	>60	Poor
	LENAWEE	Wc A	Wauseon loam, 0 to 3 percent slopes	2.0	0	0.28	5	1	Prime farmland if drained	Poorly drained	B/D	Hydric	High potential for compaction	>60	Fair
Yard 4-2															
	WASHTENAW	Wa A	Wasepi sandy loam, 0 to 4 percent slopes	6.3	0	0.2	3	2	Farmland of local importance	Somewhat poorly drained	B	Non-Hydric	Moderate potential for compaction	>60	Good
	WASHTENAW	BnB	Boyer loamy sand, 0 to 6 percent slopes	1.0	0	0.17	2	3	Farmland of local importance	Well drained	B	Non-Hydric	Low potential for compaction	>60	Fair

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	**County**	**Map Unit**	**Soil Association/ Series/ Complex**	**Project Work Area (acres) a/**	**Permanent ROW Area (acres) b/**	**Erodibility**		**Slope Percent e/' f/**	**Prime Farmland Soils Designation g/**	**Drainage Class**	**Dominant Hydrologic Group**	**Hydric h/**	**Compaction Potential i/**	**Average Approximate Depth to Bedrock (inches) j/**	**Re-vegetation Potential k/**
						Water (K Factor) c/	**Wind (WEG) d/**								
Yard 4-3															
	WASHTENAW	Wa A	Wasepi sandy loam, 0 to 4 percent slopes	6.7	0	0.2	3	2	Farmland of local importance	Somewhat poorly drained	B	Non-Hydric	Moderate potential for compaction	>60	Good
	WASHTENAW	BnB	Boyer loamy sand, 0 to 6 percent slopes	9.1	0	0.17	2	3	Farmland of local importance	Well drained	B	Non-Hydric	Low potential for compaction	>60	Fair
	WASHTENAW	Gf	Gilford sandy loam	0.4	0	0.2	3	1	Not prime farmland	Very poorly drained	B/D	Hydric	High potential for compaction	>80	Fair

TABLE 7.2-2

Summary of Soil Characteristics by County and State in Acres Affected by the NEXUS Project Pipeline and Aboveground Facilities

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Project Work Area (acres) a/	Permanent ROW Area (acres) b/	Erodibility		Slope Percent e/' f/	Prime Farmland Soils Designation g/	Drainage Class	Dominant Hydrologic Group	Hydric h/	Compaction Potential i/	Average Approximate Depth to Bedrock (inches) j/	Re-vegetation Potential k/
						Water (K Factor) c/	Wind (WEG) d/								

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a/ "Project Work Areas" = permanent easement of new Project components, temporary work spaces ("TWS") and alternate temporary work spaces ("ATWS").
b/ "Permanent ROW Area" = permanent easement of new Project components.
c/ Average K factor values of horizons of each soil type.
d/ Wind Erosion Group (WEG) status was obtained from the NRCS Soil Data Mart. WEGs range from one to eight, with one being the highest potential for wind erosion, and eight the lowest. Refer to Section 7.3.1.2.
e/ Slope classes assume all slopes are moderately complex and are based on the median slope span described for the series. Classes are defined as follows:

Median Slope (%) for Series	Slope Class
0	Flat
1-3	Nearly Level
4-8	Gently Sloping
9-15	Strongly Sloping
16-30	Moderately Steep
31-45	Steep
>45	Very Steep

f/ For soil map units including areas of Udorthents and Urban Land, NRCS data did not specify a slope range. A slope range of 0 to 8 % was assigned to these developed areas.
g/ Prime Farmland soils designations include: Prime Farmland, Prime Farmland if Drained and Farmland of Local Importance.
h/ All soils with Drainage Classifications of Very Poorly Drained and Poorly Drained are considered "Hydric". "Urban Land" and "Udorthents" map units do not have a NRCS designated drainage class. These map units were considered to be non-hydric soils. Map units comprised of complexes of hydric and non-hydric soil types were considered to be partially hydric.
i/ Compaction potential was determined by drainage class. High compaction potential includes very poorly drained and poorly drained soils, moderate compaction potential includes somewhat poorly drained to moderately well drained soils, and low compaction potential includes well drained soils.
j/ Depths to bedrock were compiled from either the Natural Resources Conservation Service County Soil Surveys or from the NRCS Official Soil Series Descriptions .
k/ The ability of soils within the Project area to support successful revegetation was determined by using the revegetation potential of grasses as recorded in the SSURGO database.

TABLE 7.2-3

Summary of Soil Characteristics by County and State in Miles Affected by Temporary and Permanent Access Roads

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Length (miles) a/	Erodibility		Slope Percent d/, e/	Prime Farmland Soils Designation f/	Drainage Class	Dominant Hydrologic Group	Hydric g/	Compaction Potential h/	Average Approximate Depth to Bedrock (inches) i/	Re-vegetation Potential j/
					Water (K Factor) b/	Wind (WEG) c/								
Ohio														
PAR-0.0a	COLUMBIANA	BkB	Berks channery silt loam, 2 to 6 percent slopes	0.03	0.17	6	4	All areas are prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	20-40	Fair
PAR-0.0a	COLUMBIANA	BkD	Berks channery silt loam, 15 to 25 percent slopes	0.06		6	20	Not prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	20-40	Fair
PAR-0.0b	COLUMBIANA	BkD	Berks channery silt loam, 15 to 25 percent slopes	0.00		6	20	Not prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	20-40	Fair
PAR-1.3	COLUMBIANA	FoB	Fredericktown silt loam, 2 to 6 percent slopes	0.01	0.32	5	4	All areas are prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>80	Good
PAR-3.4	COLUMBIANA	KnD	Kensington silt loam, 15 to 25 percent slopes	0.01		6	20	Not prime farmland	Moderately well drained	B	Non-Hydric	Moderate potential for compaction	>60	Fair
PAR-3.4	COLUMBIANA	TeC	Teegarden silt loam, 6 to 15 percent slopes	0.01	0.37	6	10.5	Not prime farmland	Moderately well drained	C/D	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-10.4	COLUMBIANA	CcE	Canfield silt loam, 20 to 35 percent slopes	0.06	0.37	5	27.5	Not prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>80	Fair
TAR-10.4	COLUMBIANA	RsC	Rittman silt loam, 6 to 12 percent slopes	0.09	0.43	6	9	Not prime farmland	Moderately well drained	D	Non-Hydric	Moderate potential for compaction	40-60	Good

TABLE 7.2-3

Summary of Soil Characteristics by County and State in Miles Affected by Temporary and Permanent Access Roads

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Length (miles) a/	Erodibility		Slope Percent d/, e/	Prime Farmland Soils Designation f/	Drainage Class	Dominant Hydrologic Group	Hydric g/	Compaction Potential h/	Average Approximate Depth to Bedrock (inches) i/	Re-vegetation Potential j/
					Water (K Factor) b/	Wind (WEG) c/								
TAR-11.2	COLUMBIANA	BtB	Bogart silt loam, 2 to 6 percent slopes	0.10	0.32	5	4	All areas are prime farmland	Moderately well drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-11.2	COLUMBIANA	CcC	Canfield silt loam, 6 to 12 percent slopes	0.01	0.37	5	9	Not prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>80	Good
TAR-11.2	COLUMBIANA	CcE	Canfield silt loam, 20 to 35 percent slopes	0.04	0.37	5	27.5	Not prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>80	Fair
TAR-11.2	COLUMBIANA	ZeA	Zepernick silt loam, 0 to 2 percent slopes, occasionally flooded	0.07	0.37	6	0.5	Prime farmland if drained	Somewhat poorly drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Poor
TAR-12.0	COLUMBIANA	CcD	Canfield silt loam, 12 to 20 percent slopes	0.01	0.37	5	16	Not prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>80	Fair
TAR-12.0	COLUMBIANA	ZeA	Zepernick silt loam, 0 to 2 percent slopes, occasionally flooded	0.11	0.37	6	0.5	Prime farmland if drained	Somewhat poorly drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Poor
TAR-2.6	COLUMBIANA	HeE	Hazleton channery loam, 25 to 40 percent slopes	0.08		5	32.5	Not prime farmland	Well drained	A	Non-Hydric	Low potential for compaction	40-80	Fair
TAR-2.6	COLUMBIANA	TeC 2	Teegarden silt loam, 6 to 15 percent slopes, eroded	0.06	0.37	6	10.5	Not prime farmland	Moderately well drained	C/D	Non-Hydric	Moderate potential for compaction	>60	Good

TABLE 7.2-3

Summary of Soil Characteristics by County and State in Miles Affected by Temporary and Permanent Access Roads

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Length (miles) a/	Erodibility Water (K Factor) b/	Erodibility Wind (WEG) c/	Slope Percent d/, e/	Prime Farmland Soils Designation f/	Drainage Class	Dominant Hydrologic Group	Hydric g/	Compaction Potential h/	Average Approximate Depth to Bedrock (inches) i/	Re-vegetation Potential j/
TAR-3.6	COLUMBIANA	KnC	Kensington silt loam, 6 to 15 percent slopes	0.03		6	10.5	Not prime farmland	Moderately well drained	B	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-4.0	COLUMBIANA	GnD	Gilpin silt loam, 15 to 25 percent slopes	0.03	0.24	6	20	Not prime farmland	Well drained	C	Non-Hydric	Low potential for compaction	20-40	Fair
TAR-4.0	COLUMBIANA	HeD	Hazleton channery loam, 15 to 25 percent slopes	0.14		5	20	Not prime farmland	Well drained	A	Non-Hydric	Low potential for compaction	40-80	Fair
TAR-4.0	COLUMBIANA	TeC	Teegarden silt loam, 6 to 15 percent slopes	0.16	0.37	6	10.5	Not prime farmland	Moderately well drained	C/D	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-4.3	COLUMBIANA	GnD	Gilpin silt loam, 15 to 25 percent slopes	0.04	0.24	6	20	Not prime farmland	Well drained	C	Non-Hydric	Low potential for compaction	20-40	Fair
TAR-4.3	COLUMBIANA	KnC	Kensington silt loam, 6 to 15 percent slopes	0.36		6	10.5	Not prime farmland	Moderately well drained	B	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-4.3	COLUMBIANA	KnD	Kensington silt loam, 15 to 25 percent slopes	0.14		6	20	Not prime farmland	Moderately well drained	B	Non-Hydric	Moderate potential for compaction	>60	Fair
TAR-4.8a	COLUMBIANA	FnC2	Fredericktown gravelly loam, 6 to 15 percent slopes, eroded	0.02	0.24	5	10.5	Not prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>80	Good

TABLE 7.2-3

Summary of Soil Characteristics by County and State in Miles Affected by Temporary and Permanent Access Roads

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Length (miles) a/	Erodibility: Water (K Factor) b/	Erodibility: Wind (WEG) c/	Slope Percent d/, e/	Prime Farmland Soils Designation f/	Drainage Class	Dominant Hydrologic Group	Hydric g/	Compaction Potential h/	Average Approximate Depth to Bedrock (inches) i/	Re-vegetation Potential j/
TAR-4.8a	COLUMBIANA	ZeA	Zepernick silt loam, 0 to 2 percent slopes, occasionally flooded	0.03	0.37	6	0.5	Prime farmland if drained	Somewhat poorly drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Poor
TAR-4.8b	COLUMBIANA	FnC 2	Fredericktown gravelly loam, 6 to 15 percent slopes, eroded	0.03	0.24	5	10.5	Not prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>80	Good
TAR-4.8b	COLUMBIANA	JwB	Jimtown silt loam, 2 to 6 percent slopes	0.01	0.32	5	4	Prime farmland if drained	Somewhat poorly drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-4.8b	COLUMBIANA	ZeA	Zepernick silt loam, 0 to 2 percent slopes, occasionally flooded	0.02	0.37	6	0.5	Prime farmland if drained	Somewhat poorly drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Poor
TAR-7.2	COLUMBIANA	CcB	Canfield silt loam, 2 to 6 percent slopes	0.02	0.37	5	4	All areas are prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>80	Good
TAR-7.2	COLUMBIANA	CcC	Canfield silt loam, 6 to 12 percent slopes	0.08	0.37	5	9	Not prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>80	Good
TAR-7.6	COLUMBIANA	CcB	Canfield silt loam, 2 to 6 percent slopes	0.03	0.37	5	4	All areas are prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>80	Good
TAR-7.6	COLUMBIANA	CcC	Canfield silt loam, 6 to 12 percent slopes	0.15	0.37	5	9	Not prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>80	Good

TABLE 7.2-3

Summary of Soil Characteristics by County and State in Miles Affected by Temporary and Permanent Access Roads

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Length (miles) a/	Erodibility		Slope Percent d/, e/	Prime Farmland Soils Designation f/	Drainage Class	Dominant Hydrologic Group	Hydric g/	Compaction Potential h/	Average Approximate Depth to Bedrock (inches) i/	Re-vegetation Potential j/
					Water (K Factor) b/	Wind (WEG) c/								
TAR-7.6	COLUMBIANA	HeE	Hazleton channery loam, 25 to 40 percent slopes	0.04		5	32.5	Not prime farmland	Well drained	A	Non-Hydric	Low potential for compaction	40-80	Fair
TAR-7.9	COLUMBIANA	ChC	Chili silt loam, 6 to 12 percent slopes	0.05	0.32	5	9	Not prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>60	Good
TAR-7.9	COLUMBIANA	FeA	Fluvaquents, silty, 0 to 1 percent slopes, frequently flooded	0.07			0.5	Not prime farmland	Very poorly drained	D	Hydric	High potential for compaction	>80	Very poor
TAR-7.9	COLUMBIANA	KnD	Kensington silt loam, 15 to 25 percent slopes	0.03		6	20	Not prime farmland	Moderately well drained	B	Non-Hydric	Moderate potential for compaction	>60	Fair
PAR-14.3	STARK	FcA	Fitchville silt loam, 0 to 2 percent slopes	0.01	0.37	6	1	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	>80	Good
TAR-13.0	STARK	CdC	Canfield silt loam, 6 to 12 percent slopes	0.06	0.37	5	9	Not prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>80	Good
TAR-15.0	STARK	CdC	Canfield silt loam, 6 to 12 percent slopes	0.30	0.37	5	9	Not prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>80	Good
TAR-15.0	STARK	CoD 2	Chili gravelly loam, 12 to 18 percent slopes, moderately eroded	0.01	0.1	5	15	Not prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>60	Fair

TABLE 7.2-3

Summary of Soil Characteristics by County and State in Miles Affected by Temporary and Permanent Access Roads

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Length (miles) a/	Erodibility Water (K Factor) b/	Erodibility Wind (WEG) c/	Slope Percent d/, e/	Prime Farmland Soils Designation f/	Drainage Class	Dominant Hydrologic Group	Hydric g/	Compaction Potential h/	Average Approximate Depth to Bedrock (inches) i/	Re-vegetation Potential j/
TAR-15.0	STARK	FcA	Fitchville silt loam, 0 to 2 percent slopes	0.01	0.37	6	1	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	>80	Good
TAR-15.0	STARK	GfC	Glenford silt loam, 6 to 12 percent slopes	0.14	0.37	6	9	Not prime farmland	Moderately well drained	C/D	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-15.0	STARK	ReB	Ravenna silt loam, 2 to 6 percent slopes	0.03	0.37	6	4	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>80	Good
TAR-18.1	STARK	CdB	Canfield silt loam, 2 to 6 percent slopes	0.08	0.37	5	4	All areas are prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>80	Good
TAR-18.1	STARK	FcA	Fitchville silt loam, 0 to 2 percent slopes	0.06	0.37	6	1	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	>80	Good
TAR-18.1	STARK	ReB	Ravenna silt loam, 2 to 6 percent slopes	0.11	0.37	6	4	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>80	Good
TAR-19.4	STARK	CdB	Canfield silt loam, 2 to 6 percent slopes	0.17	0.37	5	4	All areas are prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>80	Good
TAR-19.4	STARK	CdC	Canfield silt loam, 6 to 12 percent slopes	0.02	0.37	5	9	Not prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>80	Good
TAR-19.4	STARK	CdC2	Canfield silt loam, 6 to 12 percent slopes, moderately eroded	0.01	0.37	5	9	Not prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>80	Good

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Summary of Soil Characteristics by County and State in Miles Affected by Temporary and Permanent Access Roads

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Length (miles) a/	Erodibility		Slope Percent d/, e/	Prime Farmland Soils Designation f/	Drainage Class	Dominant Hydrologic Group	Hydric g/	Compaction Potential h/	Average Approximate Depth to Bedrock (inches) i/	Re-vegetation Potential j/
					Water (K Factor) b/	Wind (WEG) c/								
TAR-19.4	STARK	ReB	Ravenna silt loam, 2 to 6 percent slopes	0.05	0.37	6	4	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>80	Good
TAR-19.4	STARK	Sh	Shoals silt loam	0.02	0.24	6	1	Prime farmland if drained	Somewhat poorly drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Fair
TAR-19.8	STARK	CdC 2	Canfield silt loam, 6 to 12 percent slopes, moderately eroded	0.02	0.37	5	9	Not prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>80	Good
TAR-19.8	STARK	ReB	Ravenna silt loam, 2 to 6 percent slopes	0.05	0.37	6	4	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>80	Good
TAR-19.8	STARK	RsC 2	Rittman silt loam, 6 to 12 percent slopes, moderately eroded	0.10	0.43	6	9	Not prime farmland	Moderately well drained	D	Non-Hydric	Moderate potential for compaction	40-60	Good
TAR-19.8	STARK	Wa B	Wadsworth silt loam, 2 to 6 percent slopes	0.26	0.43	6	4	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-20.3	STARK	RsC 2	Rittman silt loam, 6 to 12 percent slopes, moderately eroded	0.07	0.43	6	9	Not prime farmland	Moderately well drained	D	Non-Hydric	Moderate potential for compaction	40-60	Good
TAR-20.3	STARK	Wa B	Wadsworth silt loam, 2 to 6 percent slopes	0.14	0.43	6	4	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>60	Good

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State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Length (miles) a/	Erodibility Water (K Factor) b/	Erodibility Wind (WEG) c/	Slope Percent d/, e/	Prime Farmland Soils Designation f/	Drainage Class	Dominant Hydrologic Group	Hydric g/	Compaction Potential h/	Average Approximate Depth to Bedrock (inches) i/	Re-vegetation Potential j/
TAR-24.6	STARK	CdC2	Canfield silt loam, 6 to 12 percent slopes, moderately eroded	0.08	0.37	5	9	Not prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>80	Good
TAR-24.6	STARK	ReB	Ravenna silt loam, 2 to 6 percent slopes	0.03	0.37	6	4	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>80	Good
TAR-24.6	STARK	WuC2	Wooster silt loam, 6 to 12 percent slopes, moderately eroded	0.01	0.37	5	9	Not prime farmland	Well drained	C	Non-Hydric	Low potential for compaction	>85	Good
TAR-27.2	STARK	CdB	Canfield silt loam, 2 to 6 percent slopes	0.04	0.37	5	4	All areas are prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>80	Good
TAR-27.2	STARK	Wt	Willette muck	0.12		2	1	Not prime farmland	Very poorly drained	C/D	Hydric	High potential for compaction	>60	Poor
TAR-27.2	STARK	WuC2	Wooster silt loam, 6 to 12 percent slopes, moderately eroded	0.06	0.37	5	9	Not prime farmland	Well drained	C	Non-Hydric	Low potential for compaction	>85	Good
TAR-28.4	STARK	CpB	Chili silt loam, 2 to 6 percent slopes	0.10	0.32	5	4	All areas are prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>60	Good
PAR-33.4	SUMMIT	CpB	Chili silt loam, 2 to 6 percent slopes	0.08	0.1	5	4	All areas are prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>60	Fair

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Summary of Soil Characteristics by County and State in Miles Affected by Temporary and Permanent Access Roads

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Length (miles) a/	Erodibility		Slope Percent d/, e/	Prime Farmland Soils Designation f/	Drainage Class	Dominant Hydrologic Group	Hydric g/	Compaction Potential h/	Average Approximate Depth to Bedrock (inches) i/	Re-vegetation Potential j/
					Water (K Factor) b/	Wind (WEG) c/								
PAR-42.3	SUMMIT	Wu C2	Wooster silt loam, 6 to 12 percent slopes, moderately eroded	0.02	0.37	5	9	Not prime farmland	Well drained	C	Non-Hydric	Low potential for compaction	>85	Good
TAR-34.0	SUMMIT	CdB	Canfield silt loam, 2 to 6 percent slopes	0.36	0.37	5	4	All areas are prime farmland	Moderately well drained	D	Non-Hydric	Moderate potential for compaction	>80	Good
TAR-34.0	SUMMIT	ReA	Ravenna silt loam, 0 to 2 percent slopes	0.06	0.37	5	1	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>80	Fair
TAR-34.0	SUMMIT	Sb	Sebring silt loam	0.02	0.37	6	1	Prime farmland if drained	Poorly drained	C/D	Hydric	High potential for compaction	>60	Poor
TAR-34.0	SUMMIT	Ua	Udorthents	0.07			0	Not prime farmland					N/A	
TAR-36.1	SUMMIT	CnA	Chili loam, 0 to 2 percent slopes	0.06	0.32	5	1	All areas are prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>60	Fair
TAR-36.1	SUMMIT	CpC	Chili silt loam, 6 to 12 percent slopes	0.00	0.1	5	9	Not prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>60	Fair
TAR-36.8	SUMMIT	CoD 2	Chili gravelly loam, 12 to 18 percent slopes, moderately eroded	0.04	0.24	8	15	Not prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>60	Fair

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Summary of Soil Characteristics by County and State in Miles Affected by Temporary and Permanent Access Roads

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Length (miles) a/	Erodibility Water (K Factor) b/	Erodibility Wind (WEG) c/	Slope Percent d/, e/	Prime Farmland Soils Designation f/	Drainage Class	Dominant Hydrologic Group	Hydric g/	Compaction Potential h/	Average Approximate Depth to Bedrock (inches) i/	Re-vegetation Potential j/
TAR-36.8	SUMMIT	CpC	Chili silt loam, 6 to 12 percent slopes	0.07	0.1	5	9	Not prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>60	Fair
TAR-37.1	SUMMIT	CnC	Chili loam, 6 to 12 percent slopes	0.05	0.1	5	9	Not prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>60	Fair
TAR-37.1	SUMMIT	CyD	Conotton-Oshtemo complex, 12 to 18 percent slopes	0.07	0.24	8	15	Not prime farmland	Well drained	A	Non-Hydric	Low potential for compaction	>80	Fair
TAR-38.5	SUMMIT	GfB	Glenford silt loam, 2 to 6 percent slopes	0.00	0.37	6	4	All areas are prime farmland	Moderately well drained	C/D	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-38.5	SUMMIT	Ln	Lorain silty clay loam	0.06	0.32	7	1	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	20-40	Poor
TAR-38.5	SUMMIT	WrB	Wheeling silt loam, 2 to 6 percent slopes	0.11	0.2	5	4	All areas are prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	40-60	Good
TAR-38.7	SUMMIT	CdB	Canfield silt loam, 2 to 6 percent slopes	0.04	0.37	5	4	All areas are prime farmland	Moderately well drained	D	Non-Hydric	Moderate potential for compaction	>80	Good
TAR-38.7	SUMMIT	CnB	Chili loam, 2 to 6 percent slopes	0.03	0.1	5	4	All areas are prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>60	Fair
TAR-38.7	SUMMIT	CnC	Chili loam, 6 to 12 percent slopes	0.07	0.1	5	9	Not prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>60	Fair

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					Water (K Factor) b/	Wind (WEG) c/								
TAR-38.7	SUMMIT	CyD	Conotton-Oshtemo complex, 12 to 18 percent slopes	0.02	0.24	8	15	Not prime farmland	Well drained	A	Non-Hydric	Low potential for compaction	>80	Fair
TAR-38.7	SUMMIT	Da	Damascus loam	0.03	0.32	6	1	Prime farmland if drained	Poorly drained	B/D	Hydric	High potential for compaction	>75	Fair
TAR-38.7	SUMMIT	FcA	Fitchville silt loam, 0 to 2 percent slopes	0.13	0.37	6	1	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	>80	Fair
TAR-38.7	SUMMIT	Sb	Sebring silt loam	0.04	0.37	6	1	Prime farmland if drained	Poorly drained	C/D	Hydric	High potential for compaction	>60	Poor
TAR-39.1	SUMMIT	CnB	Chili loam, 2 to 6 percent slopes	0.11	0.1	5	4	All areas are prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>60	Fair
TAR-39.1	SUMMIT	CoC2	Chili gravelly loam, 6 to 12 percent slopes, moderately eroded	0.08	0.24	8	9	Not prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>60	Fair
TAR-40.6	SUMMIT	WuC2	Wooster silt loam, 6 to 12 percent slopes, moderately eroded	0.10	0.37	5	9	Not prime farmland	Well drained	C	Non-Hydric	Low potential for compaction	>85	Good
TAR-45.0	SUMMIT	BgB	Bogart loam, 2 to 6 percent slopes	0.04	0.32	5	4	All areas are prime farmland	Moderately well drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Good

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Summary of Soil Characteristics by County and State in Miles Affected by Temporary and Permanent Access Roads

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					Water (K Factor) b/	Wind (WEG) c/								
TAR-45.0	SUMMIT	Wu C2	Wooster silt loam, 6 to 12 percent slopes, moderately eroded	0.02	0.37	5	9	Not prime farmland	Well drained	C	Non-Hydric	Low potential for compaction	>85	Good
TAR-45.0	SUMMIT	Wu D2	Wooster silt loam, 12 to 18 percent, moderately eroded	0.17	0.37	5	15	Not prime farmland	Well drained	C	Non-Hydric	Low potential for compaction	>85	Good
PAR-50.5	WAYNE	GfC	Glenford silt loam, 6 to 12 percent slopes	0.03	0.37	6	9	Farmland of local importance	Moderately well drained	C/D	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-50.5	WAYNE	GfB	Glenford silt loam, 2 to 6 percent slopes	0.08	0.37	6	4	All areas are prime farmland	Moderately well drained	C/D	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-50.7	WAYNE	CdC	Canfield silt loam, 6 to 12 percent slopes	0.05	0.37	5	9	Farmland of local importance	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>80	Good
TAR-50.9	WAYNE	GfB	Glenford silt loam, 2 to 6 percent slopes	0.00	0.37	6	4	All areas are prime farmland	Moderately well drained	C/D	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-50.9	WAYNE	Wu C2	Wooster-Riddles silt loams, 6 to 12 percent slopes, eroded	0.16	0.32	5	9	Farmland of local importance	Well drained	C	Non-Hydric	Low potential for compaction	40-60	Good
TAR-53.9	WAYNE	CdB	Canfield silt loam, 2 to 6 percent slopes	0.15	0.37	5	4	All areas are prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>80	Good

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					Water (K Factor) b/	Wind (WEG) c/								
TAR-53.9	WAYNE	ReA	Ravenna silt loam, 0 to 2 percent slopes	0.05	0.37	6	1	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>80	Good
PAR-60.3	MEDINA	RsB	Rittman silt loam, 2 to 6 percent slopes	0.22	0.43	5	3	All areas are prime farmland	Moderately well drained	D	Non-Hydric	Moderate potential for compaction	40-60	Good
PAR-60.3	MEDINA	WaA	Wadsworth silt loam, 0 to 2 percent slopes	0.16	0.43	6	2	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>60	Good
PAR-63.1	MEDINA	RsB	Rittman silt loam, 2 to 6 percent slopes	0.05	0.43	5	3	All areas are prime farmland	Moderately well drained	D	Non-Hydric	Moderate potential for compaction	40-60	Good
PAR-63.1	MEDINA	RsC2	Rittman silt loam, 6 to 12 percent slopes, moderately eroded	0.06	0.43	5	10	Farmland of local importance	Moderately well drained	D	Non-Hydric	Moderate potential for compaction	40-60	Good
PAR-73.4	MEDINA	MgA	Mahoning silt loam, 0 to 2 percent slopes	0.01	0.43	6	2	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	40-60	Good
PAR-73.4	MEDINA	MgB	Mahoning silt loam, 2 to 6 percent slopes	0.10	0.43	6	3	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	40-60	Good
TAR-53.9	MEDINA	CdB	Canfield silt loam, 2 to 6 percent slopes	0.01	0.37	5	4	All areas are prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>80	Good
TAR-60.8	MEDINA	CnC	Chili loam, 6 to 12 percent slopes	0.06	0.17	5	8	Farmland of local importance	Well drained	B	Non-Hydric	Low potential for compaction	>60	Good

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					Water (K Factor) b/	Wind (WEG) c/								
TAR-60.8	MEDINA	Wa A	Wadsworth silt loam, 0 to 2 percent slopes	0.04	0.43	6	2	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-61.9	MEDINA	Wa A	Wadsworth silt loam, 0 to 2 percent slopes	0.20	0.43	6	2	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-63.4	MEDINA	RsC 2	Rittman silt loam, 6 to 12 percent slopes, moderately eroded	0.11	0.43	5	10	Farmland of local importance	Moderately well drained	D	Non-Hydric	Moderate potential for compaction	40-60	Good
TAR-63.4	MEDINA	St	Sebring silt loam, till substratum	0.02	0.37	6	0.5	Prime farmland if drained	Poorly drained	C/D	Hydric	High potential for compaction	>60	Fair
TAR-63.4	MEDINA	Wa B	Wadsworth silt loam, 2 to 6 percent slopes	0.09	0.43	6	3	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-65.5	MEDINA	RsB 2	Rittman silt loam, 2 to 6 percent slopes, moderately eroded	0.18	0.43	5	5	All areas are prime farmland	Moderately well drained	D	Non-Hydric	Moderate potential for compaction	40-60	Good
TAR-65.5	MEDINA	RsC 2	Rittman silt loam, 6 to 12 percent slopes, moderately eroded	0.02	0.43	5	10	Farmland of local importance	Moderately well drained	D	Non-Hydric	Moderate potential for compaction	40-60	Good
TAR-65.5	MEDINA	Wa A	Wadsworth silt loam, 0 to 2 percent slopes	0.01	0.43	6	2	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>60	Good

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TAR-66.1	MEDINA	BnA	Bennington silt loam, 0 to 2 percent slopes	0.18	0.43	6	1	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	>80	Good
TAR-66.1	MEDINA	BnB	Bennington silt loam, 2 to 6 percent slopes	0.00	0.43	6	3	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	>80	Good
TAR-66.1	MEDINA	BtB	Bogart loam, 2 to 6 percent slopes	0.03	0.32	5	3	All areas are prime farmland	Moderately well drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-66.1	MEDINA	CgB	Cardington silt loam, 2 to 6 percent slopes	0.05	0.37	5	3	All areas are prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	78	Good
TAR-66.1	MEDINA	CgC 2	Cardington silt loam, 6 to 12 percent slopes, moderately eroded	0.04	0.37	5	8	Farmland of local importance	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	78	Good
TAR-66.5	MEDINA	BnA	Bennington silt loam, 0 to 2 percent slopes	0.10	0.43	6	1	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	>80	Good
TAR-66.5	MEDINA	BnB	Bennington silt loam, 2 to 6 percent slopes	0.11	0.43	6	3	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	>80	Good
TAR-69.1	MEDINA	BnB	Bennington silt loam, 2 to 6 percent slopes	0.03	0.43	6	3	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	>80	Good
TAR-69.8	MEDINA	BtB	Bogart loam, 2 to 6 percent slopes	0.07	0.32	5	3	All areas are prime farmland	Moderately well drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Good

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State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Length (miles) a/	Erodibility		Slope Percent d/, e/	Prime Farmland Soils Designation f/	Drainage Class	Dominant Hydrologic Group	Hydric g/	Compaction Potential h/	Average Approximate Depth to Bedrock (inches) i/	Re-vegetation Potential j/
					Water (K Factor) b/	Wind (WEG) c/								
TAR-69.8	MEDINA	Or	Orrville silt loam	0.02	0.37	5	0.5	Prime farmland if drained and either protected from flooding or not frequently flooded during the growing season	Somewhat poorly drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Fair
TAR-70.1	MEDINA	ElB	Ellsworth silt loam, 2 to 6 percent slopes	0.05	0.43	6	3	All areas are prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-70.1	MEDINA	ElC	Ellsworth silt loam, 6 to 12 percent slopes	0.02	0.43	6	8	Farmland of local importance	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>80	Good
TAR-70.1	MEDINA	ElE2	Ellsworth silt loam, 12 to 25 percent slopes, moderately eroded	0.02	0.43	6	16	Not prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>60	Fair
TAR-70.1	MEDINA	ElF	Ellsworth silt loam, 25 to 70 percent slopes	0.00	0.43	6	25	Not prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>60	Poor

TABLE 7.2-3

Summary of Soil Characteristics by County and State in Miles Affected by Temporary and Permanent Access Roads

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Length (miles) a/	Erodibility		Slope Percent d/, e/	Prime Farmland Soils Designation f/	Drainage Class	Dominant Hydrologic Group	Hydric g/	Compaction Potential h/	Average Approximate Depth to Bedrock (inches) i/	Re-vegetation Potential j/
					Water (K Factor) b/	Wind (WEG) c/								
TAR-70.1	MEDINA	Or	Orrville silt loam	0.13	0.37	5	0.5	Prime farmland if drained and either protected from flooding or not frequently flooded during the growing season	Somewhat poorly drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Fair
TAR-70.6	MEDINA	Le	Lobdell silt loam	0.03	0.37	6	1	Prime farmland if protected from flooding or not frequently flooded during the growing season	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>60	Fair
TAR-72.1	MEDINA	ElB 2	Ellsworth silt loam, 2 to 6 percent slopes, moderately eroded	0.04	0.43	6	4	All areas are prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-72.1	MEDINA	ElC 2	Ellsworth silt loam, 6 to 12 percent slopes, moderately eroded	0.02	0.43	6	10	Farmland of local importance	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>60	Good

TABLE 7.2-3

Summary of Soil Characteristics by County and State in Miles Affected by Temporary and Permanent Access Roads

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Length (miles) a/	Erodibility: Water (K Factor) b/	Erodibility: Wind (WEG) c/	Slope Percent d/, e/	Prime Farmland Soils Designation f/	Drainage Class	Dominant Hydrologic Group	Hydric g/	Compaction Potential h/	Average Approximate Depth to Bedrock (inches) i/	Re-vegetation Potential j/
TAR-72.1	MEDINA	Mg B	Mahoning silt loam, 2 to 6 percent slopes	0.05	0.43	6	3	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	40-60	Good
TAR-73.4	MEDINA	Mg A	Mahoning silt loam, 0 to 2 percent slopes	0.08	0.43	6	2	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	40-60	Good
TAR-73.4	MEDINA	Mg B	Mahoning silt loam, 2 to 6 percent slopes	0.02	0.43	6	3	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	40-60	Good
TAR-74.3	MEDINA	ElC 2	Ellsworth silt loam, 6 to 12 percent slopes, moderately eroded	0.04	0.43	6	10	Farmland of local importance	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-74.3	MEDINA	Mg B	Mahoning silt loam, 2 to 6 percent slopes	0.10	0.43	6	3	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	40-60	Good
PAR-91.2	LORAIN	Mg A	Mahoning silt loam, 0 to 2 percent slopes	0.03	0.43	6	1	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	40-60	Good
TAR-82.1	LORAIN	Mg A	Mahoning silt loam, 0 to 2 percent slopes	0.23	0.43	6	1	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	40-60	Good
TAR-82.6	LORAIN	Mg A	Mahoning silt loam, 0 to 2 percent slopes	0.03	0.43	6	1	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	40-60	Good
TAR-83.5	LORAIN	Mg A	Mahoning silt loam, 0 to 2 percent slopes	0.23	0.43	6	1	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	40-60	Good

TABLE 7.2-3

Summary of Soil Characteristics by County and State in Miles Affected by Temporary and Permanent Access Roads

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Length (miles) a/	Erodibility		Slope Percent d/, e/	Prime Farmland Soils Designation f/	Drainage Class	Dominant Hydrologic Group	Hydric g/	Compaction Potential h/	Average Approximate Depth to Bedrock (inches) i/	Re-vegetation Potential j/
					Water (K Factor) b/	Wind (WEG) c/								
TAR-83.6	LORAIN	MgA	Mahoning silt loam, 0 to 2 percent slopes	0.03	0.43	6	1	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	40-60	Good
TAR-88.0	LORAIN	EIB 2	Ellsworth silt loam, 2 to 6 percent slopes, moderately eroded	0.02	0.43	6	4	All areas are prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-88.0	LORAIN	HsA	Haskins loam, 0 to 2 percent slopes	0.25	0.37	5	1	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-88.7	LORAIN	HsA	Haskins loam, 0 to 2 percent slopes	0.13	0.37	5	1	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-89.1	LORAIN	FdA	Fitchville silt loam, low terrace, 0 to 2 percent slopes	0.09	0.37	5	1	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	>80	Good
TAR-90.1	LORAIN	MgA	Mahoning silt loam, 0 to 2 percent slopes	0.04	0.43	6	1	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	40-60	Good
TAR-90.1	LORAIN	TrA	Trumbull silty clay loam, 0 to 2 percent slopes	0.00	0.37	7	1	Not prime farmland	Poorly drained	D	Hydric	High potential for compaction	>60	Fair
TAR-92.0	LORAIN	MgA	Mahoning silt loam, 0 to 2 percent slopes	0.27	0.43	6	1	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	40-60	Good

TABLE 7.2-3

Summary of Soil Characteristics by County and State in Miles Affected by Temporary and Permanent Access Roads

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Length (miles) a/	Erodibility: Water (K Factor) b/	Erodibility: Wind (WEG) c/	Slope Percent d/, e/	Prime Farmland Soils Designation f/	Drainage Class	Dominant Hydrologic Group	Hydric g/	Compaction Potential h/	Average Approximate Depth to Bedrock (inches) i/	Re-vegetation Potential j/
TAR-93.2	LORAIN	MgA	Mahoning silt loam, 0 to 2 percent slopes	0.19	0.43	6	1	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	40-60	Good
TAR-93.2	LORAIN	MkA	Mahoning-Tiro silt loams, 0 to 2 percent slopes	0.15	0.43	6	1	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	40-60	Good
TAR-93.2	LORAIN	TrA	Trumbull silty clay loam, 0 to 2 percent slopes	0.03	0.37	7	1	Not prime farmland	Poorly drained	D	Hydric	High potential for compaction	>60	Fair
TAR-97.7	LORAIN	ElC2	Ellsworth silt loam, 6 to 12 percent slopes, moderately eroded	0.01	0.43	6	9	Not prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-97.7	LORAIN	MgB	Mahoning silt loam, 2 to 6 percent slopes	0.28	0.43	6	4	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	40-60	Good
TAR-97.7	LORAIN	MkA	Mahoning-Tiro silt loams, 0 to 2 percent slopes	0.04	0.43	6	1	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	40-60	Good
PAR-106.4	ERIE	JtA	Jimtown loam, 0 to 2 percent slopes	0.06	0.32	5	1	Prime farmland if drained	Somewhat poorly drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Good
PAR-106.4	ERIE	MgA	Millgrove loam, 0 to 1 percent slopes	0.06	0.24	6	0.5	Prime farmland if drained	Very poorly drained	B/D	Hydric	High potential for compaction	60-80	Fair

TABLE 7.2-3

Summary of Soil Characteristics by County and State in Miles Affected by Temporary and Permanent Access Roads

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Length (miles) a/	Erodibility		Slope Percent d/, e/	Prime Farmland Soils Designation f/	Drainage Class	Dominant Hydrologic Group	Hydric g/	Compaction Potential h/	Average Approximate Depth to Bedrock (inches) i/	Re-vegetation Potential j/
					Water (K Factor) b/	Wind (WEG) c/								
PAR-106.4	ERIE	OsB	Oshtemo loamy sand, 0 to 6 percent slopes	0.04	0.17	2	3	All areas are prime farmland	Well drained	A	Non-Hydric	Low potential for compaction	>80	Good
PAR-106.4	ERIE	TuB	Tuscola fine sandy loam, 2 to 6 percent slopes	0.06	0.24	3	4	All areas are prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>80	Good
PAR-117.9	ERIE	FrA	Fries silty clay loam, 0 to 1 percent slopes	0.01	0.28	7	0.5	Prime farmland if drained	Very poorly drained	D	Hydric	High potential for compaction	28-30	Fair
PAR-117.9	ERIE	MgA	Millgrove loam, 0 to 1 percent slopes	0.02	0.24	6	0.5	Prime farmland if drained	Very poorly drained	B/D	Hydric	High potential for compaction	60-80	Fair
TAR-101.9	ERIE	On	Orrville silt loam, frequently flooded	0.07	0.37	5	1	Prime farmland if drained and either protected from flooding or not frequently flooded during the growing season	Somewhat poorly drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Good

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Summary of Soil Characteristics by County and State in Miles Affected by Temporary and Permanent Access Roads

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Length (miles) a/	Erodibility Water (K Factor) b/	Erodibility Wind (WEG) c/	Slope Percent d/, e/	Prime Farmland Soils Designation f/	Drainage Class	Dominant Hydrologic Group	Hydric g/	Compaction Potential h/	Average Approximate Depth to Bedrock (inches) i/	Re-vegetation Potential j/
TAR-101.9	ERIE	OpA	Orrville silt loam, bedrock substratum, 0 to 2 percent slopes, occasionally flooded	0.01	0.37	6	1	Prime farmland if drained	Somewhat poorly drained	B/D	Non-Hydric	Moderate potential for compaction	60-80	Good
TAR-107.7	ERIE	CtB	Conotton loam, 2 to 6 percent slopes	0.01	0.24	5	4	All areas are prime farmland	Well drained	A	Non-Hydric	Low potential for compaction	>80	Fair
TAR-107.7	ERIE	UcB	Udipsamments-Spinks complex, 0 to 6 percent slopes	0.10			3	Not prime farmland	Excessively drained		Non-Hydric	Low potential for compaction	>80	
TAR-111.8	ERIE	EnA	Elnora loamy fine sand, 0 to 4 percent slopes	0.05	0.17	2	2	Not prime farmland	Moderately well drained	A/D	Non-Hydric	Moderate potential for compaction	>80	Good
TAR-111.8	ERIE	KbA	Kibbie fine sandy loam, 0 to 2 percent slopes	0.36	0.2	3	1	Prime farmland if drained	Somewhat poorly drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-111.8	ERIE	RgA	Rimer loamy fine sand, 0 to 2 percent slopes	0.01	0.32	2	1	Prime farmland if drained	Somewhat poorly drained	A/D	Non-Hydric	Moderate potential for compaction	>80	Fair
TAR-111.8	ERIE	ShB	Shinrock silt loam, 2 to 6 percent slopes	0.08	0.37	6	4	All areas are prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>60	Good

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					Water (K Factor) b/	Wind (WEG) c/								
TAR-111.8	ERIE	SkC 2	Shinrock silty clay loam, 6 to 12 percent slopes, eroded	0.03	0.37	7	9	Not prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-111.9	ERIE	DeA	Del Rey silt loam, 0 to 2 percent slopes	0.25	0.43	6	1	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-111.9	ERIE	EnA	Elnora loamy fine sand, 0 to 4 percent slopes	0.00	0.17	2	2	Not prime farmland	Moderately well drained	A/D	Non-Hydric	Moderate potential for compaction	>80	Good
TAR-111.9	ERIE	ShB	Shinrock silt loam, 2 to 6 percent slopes	0.04	0.37	6	4	All areas are prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-112.5	ERIE	HoA	Holly silt loam, 0 to 1 percent slopes, occasionally flooded	0.12	0.28	6	0.5	Prime farmland if drained	Poorly drained	B/D	Hydric	High potential for compaction	>60	Fair
TAR-112.6	ERIE	ShB	Shinrock silt loam, 2 to 6 percent slopes	0.00	0.37	6	4	All areas are prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-112.6	ERIE	SkC 2	Shinrock silty clay loam, 6 to 12 percent slopes, eroded	0.05	0.37	7	9	Not prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>60	Good

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Summary of Soil Characteristics by County and State in Miles Affected by Temporary and Permanent Access Roads

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Length (miles) a/	Erodibility: Water (K Factor) b/	Erodibility: Wind (WEG) c/	Slope Percent d/, e/	Prime Farmland Soils Designation f/	Drainage Class	Dominant Hydrologic Group	Hydric g/	Compaction Potential h/	Average Approximate Depth to Bedrock (inches) i/	Re-vegetation Potential j/
TAR-112.7	ERIE	OpA	Orrville silt loam, bedrock substratum, 0 to 2 percent slopes, occasionally flooded	0.02	0.37	6	1	Prime farmland if drained	Somewhat poorly drained	B/D	Non-Hydric	Moderate potential for compaction	60-80	Good
TAR-115.4	ERIE	KbA	Kibbie fine sandy loam, 0 to 2 percent slopes	0.09	0.2	3	1	Prime farmland if drained	Somewhat poorly drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-115.4	ERIE	TuA	Tuscola fine sandy loam, 0 to 2 percent slopes	0.03	0.24	3	1	All areas are prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>80	Good
TAR-115.4	ERIE	UdB	Udorthents, loamy, 0 to 6 percent slopes	0.11			3	Not prime farmland					N/A	
TAR-116.0	ERIE	KbA	Kibbie fine sandy loam, 0 to 2 percent slopes	0.11	0.2	3	1	Prime farmland if drained	Somewhat poorly drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-116.0	ERIE	UdB	Udorthents, loamy, 0 to 6 percent slopes	0.11			3	Not prime farmland					N/A	
TAR-116.2	ERIE	EcA	Elliott silt loam, bedrock substratum, 0 to 2 percent slopes	0.10	0.28	6	1	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	65-67	Good

TABLE 7.2-3

Summary of Soil Characteristics by County and State in Miles Affected by Temporary and Permanent Access Roads

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Length (miles) a/	Erodibility		Slope Percent d/, e/	Prime Farmland Soils Designation f/	Drainage Class	Dominant Hydrologic Group	Hydric g/	Compaction Potential h/	Average Approximate Depth to Bedrock (inches) i/	Re-vegetation Potential j/
					Water (K Factor) b/	Wind (WEG) c/								
TAR-116.2	ERIE	KbA	Kibbie fine sandy loam, 0 to 2 percent slopes	0.11	0.2	3	1	Prime farmland if drained	Somewhat poorly drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-119.3a	ERIE	HsA	Hornell silty clay loam, 0 to 2 percent slopes	0.02	0.43	7	1	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	20-40	Good
TAR-119.3b	ERIE	HsA	Hornell silty clay loam, 0 to 2 percent slopes	0.02	0.43	7	1	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	20-40	Good
TAR-119.8	ERIE	FrA	Fries silty clay loam, 0 to 1 percent slopes	0.17	0.28	7	0.5	Prime farmland if drained	Very poorly drained	D	Hydric	High potential for compaction	28-30	Fair
TAR-119.8	ERIE	HsA	Hornell silty clay loam, 0 to 2 percent slopes	0.53	0.43	7	1	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	20-40	Good
TAR-119.8	ERIE	MsA	Miner silt loam, bedrock substratum, 0 to 1 percent slopes	0.09	0.32	6	0.5	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>60	Fair
TAR-124	ERIE	JuA	Joliet silt loam, 0 to 1 percent slopes	0.07	0.28	6	0.5	Prime farmland if drained	Poorly drained	D	Hydric	High potential for compaction	19	Poor

TABLE 7.2-3

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					Water (K Factor) b/	Wind (WEG) c/								
TAR-124.4	ERIE	Mm A	Millsdale silty clay loam, 0 to 1 percent slopes	0.01	0.28	7	0.5	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	20-40	Fair
TAR-124.4	ERIE	RhA	Ritchey loam, 0 to 2 percent slopes	0.06	0.37	6	1	Not prime farmland	Well drained	D	Non-Hydric	Low potential for compaction	10-20	Poor
TAR-124.4	ERIE	TuB	Tuscola fine sandy loam, 2 to 6 percent slopes	0.00	0.24	3	4	All areas are prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>80	Good
TAR-124.5	ERIE	Cm A	Colwood loam, 0 to 1 percent slopes	0.07	0.28	5	0.5	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>60	Poor
TAR-124.5	ERIE	KbA	Kibbie fine sandy loam, 0 to 2 percent slopes	0.02	0.2	3	1	Prime farmland if drained	Somewhat poorly drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-124.5	ERIE	Mm A	Millsdale silty clay loam, 0 to 1 percent slopes	0.01	0.28	7	0.5	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	20-40	Fair
TAR-124.5	ERIE	TuB	Tuscola fine sandy loam, 2 to 6 percent slopes	0.03	0.24	3	4	All areas are prime farmland	Moderately well drained	C	Non-Hydric	Moderate potential for compaction	>80	Good
PAR-129.5	SANDUSKY	KbA	Kibbie fine sandy loam, 0 to 2 percent slopes	0.00	0.43	3	0.5	Prime farmland if drained	Somewhat poorly drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Good

TABLE 7.2-3

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					Water (K Factor) b/	Wind (WEG) c/								
PAR-132.1	SANDUSKY	KbA	Kibbie fine sandy loam, 0 to 2 percent slopes	0.01	0.43	3	0.5	Prime farmland if drained	Somewhat poorly drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Good
PAR-132.1	SANDUSKY	NpA	Nappanee silt loam, 0 to 3 percent slopes	0.00	0.37	6	0.2	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>60	Good
PAR-145.2	SANDUSKY	HoA	Hoytville clay loam, 0 to 1 percent slopes	0.02	0.24	4	0	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>80	Poor
PAR-153.1	SANDUSKY	DuB	Dunbridge sandy loam, 1 to 4 percent slopes	0.02		3	1	All areas are prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	18-42	Fair
PAR-153.1	SANDUSKY	Ms	Millsdale silty clay loam	0.05		6	0.5	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	20-40	Fair
TAR-129a	SANDUSKY	SoB	Spinks fine sand, 2 to 6 percent slopes	0.01	0.1	1	3	Not prime farmland	Well drained	A	Non-Hydric	Low potential for compaction	>100	Fair
TAR-129b	SANDUSKY	SoB	Spinks fine sand, 2 to 6 percent slopes	0.01	0.1	1	3	Not prime farmland	Well drained	A	Non-Hydric	Low potential for compaction	>100	Fair
TAR-134.3	SANDUSKY	DeA	Del Rey silt loam, 0 to 2 percent slopes	0.04	0.43	6	0.2	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-134.3	SANDUSKY	GtB	Glenford silt loam, 2 to 6 percent slopes	0.06	0.37	6	3	All areas are prime farmland	Moderately well drained	C/D	Non-Hydric	Moderate potential for compaction	>60	Good

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TAR-134.8a	SANDUSKY	DeA	Del Rey silt loam, 0 to 2 percent slopes	0.12	0.43	6	0.2	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-134.8a	SANDUSKY	Le	Lenawee silty clay loam	0.23	0.28	6	0.2	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>60	Fair
TAR-134.8b	SANDUSKY	DeA	Del Rey silt loam, 0 to 2 percent slopes	0.02	0.43	6	0.2	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-138.8a	SANDUSKY	Le	Lenawee silty clay loam	0.06	0.28	6	0.2	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>60	Fair
TAR-138.8b	SANDUSKY	Le	Lenawee silty clay loam	0.05	0.28	6	0.2	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>60	Fair
TAR-139.5a	SANDUSKY	DeA	Del Rey silt loam, 0 to 2 percent slopes	0.05	0.43	6	0.2	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-139.5a	SANDUSKY	Le	Lenawee silty clay loam	0.01	0.28	6	0.2	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>60	Fair
TAR-139.5b	SANDUSKY	DeA	Del Rey silt loam, 0 to 2 percent slopes	0.05	0.43	6	0.2	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-139.5b	SANDUSKY	Le	Lenawee silty clay loam	0.01	0.28	6	0.2	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>60	Fair

TABLE 7.2-3

Summary of Soil Characteristics by County and State in Miles Affected by Temporary and Permanent Access Roads

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Length (miles) a/	Erodibility		Slope Percent d/, e/	Prime Farmland Soils Designation f/	Drainage Class	Dominant Hydrologic Group	Hydric g/	Compaction Potential h/	Average Approximate Depth to Bedrock (inches) i/	Re-vegetation Potential j/
					Water (K Factor) b/	Wind (WEG) c/								
TAR-140.0a	SANDUSKY	Le	Lenawee silty clay loam	0.05	0.28	6	0.2	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>60	Fair
TAR-140.0b	SANDUSKY	Le	Lenawee silty clay loam	0.06	0.28	6	0.2	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>60	Fair
TAR-141.7	SANDUSKY	DeA	Del Rey silt loam, 0 to 2 percent slopes	0.22	0.43	6	0.2	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-141.9	SANDUSKY	DeA	Del Rey silt loam, 0 to 2 percent slopes	0.09	0.43	6	0.2	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-141.9	SANDUSKY	Le	Lenawee silty clay loam	0.11	0.28	6	0.2	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>60	Fair
TAR-142.5	SANDUSKY	DeA	Del Rey silt loam, 0 to 2 percent slopes	0.04	0.43	6	0.2	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-142.5	SANDUSKY	Le	Lenawee silty clay loam	0.00	0.28	6	0.2	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>60	Fair
TAR-142.6	SANDUSKY	DeA	Del Rey silt loam, 0 to 2 percent slopes	0.06	0.43	6	0.2	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-147.1	SANDUSKY	HoA	Hoytville clay loam, 0 to 1 percent slopes	0.11	0.24	4	0	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>80	Poor

TABLE 7.2-3

Summary of Soil Characteristics by County and State in Miles Affected by Temporary and Permanent Access Roads

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Length (miles) a/	Erodibility: Water (K Factor) b/	Erodibility: Wind (WEG) c/	Slope Percent d/, e/	Prime Farmland Soils Designation f/	Drainage Class	Dominant Hydrologic Group	Hydric g/	Compaction Potential h/	Average Approximate Depth to Bedrock (inches) i/	Re-vegetation Potential j/
TAR-147.1	SANDUSKY	NpA	Nappanee silt loam, 0 to 3 percent slopes	0.04	0.37	6	0.2	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-150.0	SANDUSKY	HoA	Hoytville clay loam, 0 to 1 percent slopes	0.07	0.24	4	0	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>80	Poor
TAR-150.0	SANDUSKY	NpA	Nappanee silt loam, 0 to 3 percent slopes	0.02	0.37	6	0.2	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-153.5	SANDUSKY	HoA	Hoytville clay loam, 0 to 1 percent slopes	0.15	0.24	4	0	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>80	Poor
TAR-153.5	SANDUSKY	NpA	Nappanee silt loam, 0 to 3 percent slopes	0.07	0.37	6	0.2	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-153.9	SANDUSKY	HoA	Hoytville clay loam, 0 to 1 percent slopes	0.08	0.24	4	0	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>80	Poor
TAR-153.9	SANDUSKY	NpA	Nappanee silt loam, 0 to 3 percent slopes	0.06	0.37	6	0.2	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>60	Good
PAR-163.3	WOOD	HoA	Hoytville clay loam, 0 to 1 percent slopes	0.03	0.24	4	0	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>80	Poor
TAR-158.8	WOOD	HoA	Hoytville clay loam, 0 to 1 percent slopes	0.18	0.24	4	0	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>80	Poor

TABLE 7.2-3

Summary of Soil Characteristics by County and State in Miles Affected by Temporary and Permanent Access Roads

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Length (miles) a/	Erodibility Water (K Factor) b/	Erodibility Wind (WEG) c/	Slope Percent d/, e/	Prime Farmland Soils Designation f/	Drainage Class	Dominant Hydrologic Group	Hydric g/	Compaction Potential h/	Average Approximate Depth to Bedrock (inches) i/	Re-vegetation Potential j/
TAR-160.3	WOOD	CaA	Castalia very cobbly loam, 0 to 2 percent slopes	0.06	0.2	8	1	Not prime farmland	Well drained	A	Non-Hydric	Low potential for compaction	20-40	Poor
TAR-160.3	WOOD	CbB	Castalia-Marblehead complex, very stony, 0 to 6 percent slopes	0.02		8	3	Not prime farmland	Well drained	A	Non-Hydric	Low potential for compaction	20-40	Poor
TAR-160.3	WOOD	HoA	Hoytville clay loam, 0 to 1 percent slopes	0.26	0.24	4	0	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>80	Poor
TAR-160.3	WOOD	Mh A	Millsdale silty clay loam, 0 to 1 percent slopes	0.02		6	0.5	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	20-40	Poor
TAR-160.3	WOOD	RbA	Randolph loam, 0 to 2 percent slopes	0.11		6	0.5	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	20-40	Good
TAR-161.6	WOOD	HoA	Hoytville clay loam, 0 to 1 percent slopes	0.35	0.24	4	0	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>80	Poor

TABLE 7.2-3

Summary of Soil Characteristics by County and State in Miles Affected by Temporary and Permanent Access Roads

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Length (miles) a/	Erodibility		Slope Percent d/, e/	Prime Farmland Soils Designation f/	Drainage Class	Dominant Hydrologic Group	Hydric g/	Compaction Potential h/	Average Approximate Depth to Bedrock (inches) i/	Re-vegetation Potential j/
					Water (K Factor) b/	Wind (WEG) c/								
TAR-161.6	WOOD	SpA	Sloan silty clay loam, 0 to 1 percent slopes, frequently flooded	0.20	0.28	6	0.2	Prime farmland if drained and either protected from flooding or not frequently flooded during the growing season	Very poorly drained	B/D	Hydric	High potential for compaction	>60	Poor
TAR-168.8a	WOOD	HoA	Hoytville clay loam, 0 to 1 percent slopes	0.17	0.24	4	0	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>80	Poor
TAR-168.8b	WOOD	HoA	Hoytville clay loam, 0 to 1 percent slopes	0.17	0.24	4	0	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>80	Poor
TAR-169.9	WOOD	AnA	Aurand loam, 0 to 2 percent slopes	0.06	0.32	5	1	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	>80	Good
TAR-169.9	WOOD	HoA	Hoytville clay loam, 0 to 1 percent slopes	0.57	0.24	4	0	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>80	Poor
TAR-169.9	WOOD	MfA	Mermill-Aurand complex, 0 to 1 percent slopes	0.11	0.28	6	0.5	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>80	Poor
TAR-173.8	WOOD	HoA	Hoytville clay loam, 0 to 1 percent slopes	0.14	0.24	4	0	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>80	Poor

TABLE 7.2-3

Summary of Soil Characteristics by County and State in Miles Affected by Temporary and Permanent Access Roads

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Length (miles) a/	Erodibility		Slope Percent d/, e/	Prime Farmland Soils Designation f/	Drainage Class	Dominant Hydrologic Group	Hydric g/	Compaction Potential h/	Average Approximate Depth to Bedrock (inches) i/	Re-vegetation Potential j/
					Water (K Factor) b/	Wind (WEG) c/								
TAR-173.9	WOOD	HoA	Hoytville clay loam, 0 to 1 percent slopes	0.14	0.24	4	0	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>80	Poor
TAR-173.9	WOOD	MfA	Mermill-Aurand complex, 0 to 1 percent slopes	0.08	0.28	6	0.5	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>80	Poor
TAR-174.6	WOOD	AnA	Aurand loam, 0 to 2 percent slopes	0.17	0.32	5	1	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	>80	Good
TAR-174.6	WOOD	HoA	Hoytville clay loam, 0 to 1 percent slopes	0.00	0.24	4	0	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>80	Poor
TAR-174.7	WOOD	HoA	Hoytville clay loam, 0 to 1 percent slopes	0.06	0.24	4	0	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>80	Poor
PAR-178.1	LUCAS	Mf	Mermill loam	0.01	0.32	6	1	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>80	Fair
PAR-178.9	LUCAS	HnA	Haskins loam, 0 to 3 percent slopes	0.00	0.37	5	2	Prime farmland if drained	Somewhat poorly drained	C/D	Non-Hydric	Moderate potential for compaction	>60	Good
PAR-178.9	LUCAS	Mf	Mermill loam	0.00	0.32	6	1	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>80	Fair
TAR-176.7	LUCAS	BxA	Bixler loamy fine sand, 0 to 2 percent slopes	0.02	0.17	2	1	Prime farmland if drained	Somewhat poorly drained	B	Non-Hydric	Moderate potential for compaction	>80	Fair

TABLE 7.2-3

Summary of Soil Characteristics by County and State in Miles Affected by Temporary and Permanent Access Roads

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Length (miles) a/	Erodibility Water (K Factor) b/	Erodibility Wind (WEG) c/	Slope Percent d/, e/	Prime Farmland Soils Designation f/	Drainage Class	Dominant Hydrologic Group	Hydric g/	Compaction Potential h/	Average Approximate Depth to Bedrock (inches) i/	Re-vegetation Potential j/
TAR-176.7	LUCAS	OtB	Ottokee fine sand, 0 to 6 percent slopes	0.30	0.15	1	3	Not prime farmland	Moderately well drained	A	Non-Hydric	Moderate potential for compaction	>80	Fair
TAR-176.7	LUCAS	RnA	Rimer loamy fine sand, 0 to 3 percent slopes	0.04	0.17	2	2	Prime farmland if drained	Somewhat poorly drained	A/D	Non-Hydric	Moderate potential for compaction	>80	Fair
TAR-179.9	LUCAS	SmC	Sisson loam, 6 to 12 percent slopes	0.01	0.32	5	9	Not prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>60	Good
TAR-179.9	LUCAS	So	Sloan loam, occasionally flooded	0.04	0.28	6	1	Prime farmland if drained	Very poorly drained	B/D	Hydric	High potential for compaction	>60	Poor
TAR-180.4	LUCAS	Co	Colwood loam	0.09	0.28	5	1	Prime farmland if drained	Very poorly drained	B/D	Hydric	High potential for compaction	>60	Fair
PAR-189.5	FULTON	Gr	Granby loamy fine sand	0.02	0.17	2	1	Farmland of local importance	Very poorly drained	A/D	Hydric	High potential for compaction	>80	Poor
TAR-195.4	FULTON	GoC3	Glynwood clay loam, 6 to 12 percent slopes, severely eroded	0.03	0.43	6	9	Not prime farmland	Moderately well drained	D	Non-Hydric	Moderate potential for compaction	>80	Good
TAR-195.4	FULTON	Mf	Mermill loam	0.04	0.32	5	1	Prime farmland if drained	Very poorly drained	C/D	Hydric	High potential for compaction	>80	Good

TABLE 7.2-3

Summary of Soil Characteristics by County and State in Miles Affected by Temporary and Permanent Access Roads

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Length (miles) a/	Erodibility		Slope Percent d/, e/	Prime Farmland Soils Designation f/	Drainage Class	Dominant Hydrologic Group	Hydric g/	Compaction Potential h/	Average Approximate Depth to Bedrock (inches) i/	Re-vegetation Potential j/
					Water (K Factor) b/	Wind (WEG) c/								
TAR-195.4	FULTON	NnA	Nappanee loam, 0 to 2 percent slopes	0.17	0.37	6	1	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-195.4	FULTON	NnB	Nappanee loam, 2 to 6 percent slopes	0.00	0.37	6	4	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-195.4	FULTON	RbB	Rawson sandy loam, 2 to 6 percent slopes	0.03	0.24	3	4	All areas are prime farmland	Moderately well drained	D	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-195.4	FULTON	Sh	Shoals silt loam, frequently flooded	0.02	0.24	6	1	Prime farmland if drained and either protected from flooding or not frequently flooded during the growing season	Somewhat poorly drained	B/D	Non-Hydric	Moderate potential for compaction	>60	Fair
TAR-202.7	FULTON	NnA	Nappanee loam, 0 to 2 percent slopes	0.11	0.37	6	1	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-202.7	FULTON	Zie5A	Ziegenfuss clay loam, 0 to 1 percent slopes	0.01	0.24	6	0.3	Prime farmland if drained	Poorly drained	C/D	Hydric	High potential for compaction	>80	Fair
Michigan														

TABLE 7.2-3

Summary of Soil Characteristics by County and State in Miles Affected by Temporary and Permanent Access Roads

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Length (miles) a/	Erodibility		Slope Percent d/, e/	Prime Farmland Soils Designation f/	Drainage Class	Dominant Hydrologic Group	Hydric g/	Compaction Potential h/	Average Approximate Depth to Bedrock (inches) i/	Re-vegetation Potential j/
					Water (K Factor) b/	Wind (WEG) c/								
PAR-206.5	LENAWEE	Zfsa cA	Ziegenfuss clay loam, 0 to 1 percent slopes	0.03	0.24	6	0.3	Prime farmland if drained	Poorly drained	C/D	Hydric	High potential for compaction	>80	Fair
PAR-222.5	LENAWEE	Zfsa cA	Ziegenfuss clay loam, 0 to 1 percent slopes	0.01	0.24	6	0.3	Prime farmland if drained	Poorly drained	C/D	Hydric	High potential for compaction	>80	Fair
TAR-202.8	LENAWEE	NnA	Nappanee loam, 0 to 2 percent slopes	0.02	0.37	6	1	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-202.8	LENAWEE	Zfsa cA	Ziegenfuss clay loam, 0 to 1 percent slopes	0.09	0.24	6	0.3	Prime farmland if drained	Poorly drained	C/D	Hydric	High potential for compaction	>80	Fair
TAR-204.6	LENAWEE	Zfsa cA	Ziegenfuss clay loam, 0 to 1 percent slopes	0.14	0.24	6	0.3	Prime farmland if drained	Poorly drained	C/D	Hydric	High potential for compaction	>80	Fair
TAR-220.7	LENAWEE	Pm	Pewamo clay loam	0.01	0.24	6	1	Prime farmland if drained	Poorly drained	C/D	Hydric	High potential for compaction	>60	Poor
TAR-220.7	LENAWEE	Zfsa cA	Ziegenfuss clay loam, 0 to 1 percent slopes	0.12	0.24	6	0.3	Prime farmland if drained	Poorly drained	C/D	Hydric	High potential for compaction	>80	Fair
TAR-223.9	LENAWEE	Zfsa cA	Ziegenfuss clay loam, 0 to 1 percent slopes	0.15	0.24	6	0.3	Prime farmland if drained	Poorly drained	C/D	Hydric	High potential for compaction	>80	Fair
TAR-225.0	MONROE	Zfsa cA	Ziegenfuss clay loam, 0 to 1 percent slopes	0.07	0.24	6	0.3	Prime farmland if drained	Poorly drained	C/D	Hydric	High potential for compaction	>80	Fair

TABLE 7.2-3

Summary of Soil Characteristics by County and State in Miles Affected by Temporary and Permanent Access Roads

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					Water (K Factor) b/	Wind (WEG) c/								
TAR-226.2a	MONROE	43A	Nappanee loam, 0 to 3 percent slopes	0.16	0.37	6	2	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-226.2a	MONROE	Zfsa cA	Ziegenfuss clay loam, 0 to 1 percent slopes	0.00	0.24	6	0.3	Prime farmland if drained	Poorly drained	C/D	Hydric	High potential for compaction	>80	Fair
TAR-226.2b	MONROE	Zfsa cA	Ziegenfuss clay loam, 0 to 1 percent slopes	0.21	0.24	6	0.3	Prime farmland if drained	Poorly drained	C/D	Hydric	High potential for compaction	>80	Fair
PAR-236.4	WASHTENAW	NaA	Nappanee silty clay loam, 0 to 2 percent slopes	0.01	0.37	7	1	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>60	Good
PAR-236.4	WASHTENAW	Zfsa cA	Ziegenfuss clay loam, 0 to 1 percent slopes	0.04	0.24	6	0.3	Prime farmland if drained	Poorly drained	C/D	Hydric	High potential for compaction	>80	Fair
PAR-245.6	WASHTENAW	BnB	Boyer loamy sand, 0 to 6 percent slopes	0.04	0.17	2	3	Farmland of local importance	Well drained	B	Non-Hydric	Low potential for compaction	>60	Fair
PAR-249.0	WASHTENAW	Wa A	Wasepi sandy loam, 0 to 4 percent slopes	0.10	0.2	3	2	Farmland of local importance	Somewhat poorly drained	B	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-231.6	WASHTENAW	Wb A	Wasepi sandy loam, loamy substratum, 0 to 3 percent slopes	0.06	0.2	3	2	Farmland of local importance	Somewhat poorly drained	B	Non-Hydric	Moderate potential for compaction	>60	Fair

TABLE 7.2-3

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TAR-231.6	WASHTENAW	YpA	Ypsi sandy loam, 0 to 4 percent slopes	0.37	0.2	3	2	Prime farmland if drained	Somewhat poorly drained	C	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-232.1	WASHTENAW	YpA	Ypsi sandy loam, 0 to 4 percent slopes	0.16	0.2	3	2	Prime farmland if drained	Somewhat poorly drained	C	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-232.8	WASHTENAW	WaA	Wasepi sandy loam, 0 to 4 percent slopes	0.49	0.2	3	2	Farmland of local importance	Somewhat poorly drained	B	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-232.8	WASHTENAW	YpA	Ypsi sandy loam, 0 to 4 percent slopes	0.37	0.2	3	2	Prime farmland if drained	Somewhat poorly drained	C	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-232.8	WASHTENAW	ZfsacA	Ziegenfuss clay loam, 0 to 1 percent slopes	0.08	0.24	6	0.3	Prime farmland if drained	Poorly drained	C/D	Hydric	High potential for compaction	>80	Fair
TAR-233.7	WASHTENAW	YpA	Ypsi sandy loam, 0 to 4 percent slopes	0.10	0.2	3	2	Prime farmland if drained	Somewhat poorly drained	C	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-233.8	WASHTENAW	YpA	Ypsi sandy loam, 0 to 4 percent slopes	0.14	0.2	3	2	Prime farmland if drained	Somewhat poorly drained	C	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-233.8	WASHTENAW	ZfsacA	Ziegenfuss clay loam, 0 to 1 percent slopes	0.07	0.24	6	0.3	Prime farmland if drained	Poorly drained	C/D	Hydric	High potential for compaction	>80	Fair
TAR-236.6	WASHTENAW	NaB	Nappanee silty clay loam, 2 to 6 percent slopes	0.04	0.43	7	4	Prime farmland if drained	Somewhat poorly drained	D	Non-Hydric	Moderate potential for compaction	>60	Good

TABLE 7.2-3

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					Water (K Factor) b/	Wind (WEG) c/								
TAR-236.6	WASHTENAW	Pc	Pella silt loam	0.04	0.28	6	1	Prime farmland if drained	Poorly drained	B/D	Hydric	High potential for compaction	>60	Good
TAR-236.6	WASHTENAW	StB	St. Clair clay loam, 2 to 6 percent slopes	0.09	0.37	6	4	Farmland of local importance	Moderately well drained	D	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-238.8	WASHTENAW	Wa A	Wasepi sandy loam, 0 to 4 percent slopes	0.17	0.2	3	2	Farmland of local importance	Somewhat poorly drained	B	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-240.4	WASHTENAW	Gf	Gilford sandy loam	0.02	0.2	3	1	Not prime farmland	Very poorly drained	B/D	Hydric	High potential for compaction	>80	Fair
TAR-240.4	WASHTENAW	Wa A	Wasepi sandy loam, 0 to 4 percent slopes	0.45	0.2	3	2	Farmland of local importance	Somewhat poorly drained	B	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-243.7	WASHTENAW	BnB	Boyer loamy sand, 0 to 6 percent slopes	0.02	0.17	2	3	Farmland of local importance	Well drained	B	Non-Hydric	Low potential for compaction	>60	Fair
TAR-243.9a	WASHTENAW	Wa A	Wasepi sandy loam, 0 to 4 percent slopes	0.01	0.2	3	2	Farmland of local importance	Somewhat poorly drained	B	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-243.9b	WASHTENAW	Wa A	Wasepi sandy loam, 0 to 4 percent slopes	0.01	0.2	3	2	Farmland of local importance	Somewhat poorly drained	B	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-244.1	WASHTENAW	Wa A	Wasepi sandy loam, 0 to 4 percent slopes	0.01	0.2	3	2	Farmland of local importance	Somewhat poorly drained	B	Non-Hydric	Moderate potential for compaction	>60	Good

TABLE 7.2-3

Summary of Soil Characteristics by County and State in Miles Affected by Temporary and Permanent Access Roads

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Length (miles) a/	Erodibility Water (K Factor) b/	Erodibility Wind (WEG) c/	Slope Percent d/, e/	Prime Farmland Soils Designation f/	Drainage Class	Dominant Hydrologic Group	Hydric g/	Compaction Potential h/	Average Approximate Depth to Bedrock (inches) i/	Re-vegetation Potential j/
TAR-244.3	WASHTENAW	BnB	Boyer loamy sand, 0 to 6 percent slopes	0.01	0.17	2	3	Farmland of local importance	Well drained	B	Non-Hydric	Low potential for compaction	>60	Fair
TAR-244.4	WASHTENAW	BnB	Boyer loamy sand, 0 to 6 percent slopes	0.12	0.17	2	3	Farmland of local importance	Well drained	B	Non-Hydric	Low potential for compaction	>60	Fair
TAR-244.4	WASHTENAW	MaA	Macomb loam, 0 to 4 percent slopes	0.11	0.28	5	2	Prime farmland if drained	Somewhat poorly drained	B	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-244.4	WASHTENAW	OwB	Owosso-Miami complex, 2 to 6 percent slopes	0.11	0.24	3	4	All areas are prime farmland	Well drained	B	Non-Hydric	Low potential for compaction	>60	Good
TAR-245.2	WASHTENAW	BnB	Boyer loamy sand, 0 to 6 percent slopes	0.17	0.17	2	3	Farmland of local importance	Well drained	B	Non-Hydric	Low potential for compaction	>60	Fair
TAR-248.9	WASHTENAW	WaA	Wasepi sandy loam, 0 to 4 percent slopes	0.03	0.2	3	2	Farmland of local importance	Somewhat poorly drained	B	Non-Hydric	Moderate potential for compaction	>60	Good
TAR-249.0	WASHTENAW	Gf	Gilford sandy loam	0.12	0.2	3	1	Not prime farmland	Very poorly drained	B/D	Hydric	High potential for compaction	>80	Fair
TAR-249.0	WASHTENAW	WaA	Wasepi sandy loam, 0 to 4 percent slopes	0.22	0.2	3	2	Farmland of local importance	Somewhat poorly drained	B	Non-Hydric	Moderate potential for compaction	>60	Good
			TOTAL:	***275.36***	***224.96***	***3,830***							***675***	

TABLE 7.2-3

Summary of Soil Characteristics by County and State in Miles Affected by Temporary and Permanent Access Roads

State, Facility	County	Map Unit	Soil Association/ Series/ Complex	Length (miles) a/	Erodibility		Slope Percent d/, e/	Prime Farmland Soils Designation f/	Drainage Class	Dominant Hydrologic Group	Hydric g/	Compaction Potential h/	Average Approximate Depth to Bedrock (inches) i/	Re-vegetation Potential j/
					Water (K Factor) b/	Wind (WEG) c/								

a/ Length of pipelines or access road segments
b/ Average K factor values of horizons of each soil type.
c/ Wind Erosion Group (WEG) status was obtained from the NRCS Soil Data Mart. WEGs range from one to eight, with one being the highest potential for wind erosion, and eight the lowest. Refer to Section 7.3.1.2.
d/ Slope classes assume all slopes are moderately complex and are based on the median slope span described for the series. Classes are defined as follows:

Median Slope (%) for Series	Slope Class
0	Flat
1-3	Nearly Level
4-8	Gently Sloping
9-15	Strongly Sloping
16-30	Moderately Steep
31-45	Steep
>45	Very Steep

e/ For soil map units including areas of Udorthents and Urban Land, NRCS data did not specify a slope range. A slope range of 0 to 8 % was assigned to these developed areas.
f/ Prime Farmland includes Farmland of Statewide Importance and Unique Farmland.
g/ All soils with Drainage Classifications of Very Poorly Drained and Poorly Drained are considered "Hydric". “Urban Land” and “Udorthents” map units do not have a NRCS designated drainage class. These map units were considered to be non-hydric soils. Map units comprised of complexes of hydric and non-hydric soil types were considered to be partially hydric.
h/ Compaction potential was determined by drainage class. High compaction potential includes very poorly drained and poorly drained soils, moderate compaction potential includes somewhat poorly drained to moderately well drained soils, and low compaction potential includes well drained soils.
i/ When available, depths to bedrock are recorded f in the SSURGO database.
j/ The ability of soils within the Project area to support successful revegetation was determined by using the revegetation potential of grasses as recorded in the SSURGO database.

APPENDIX 7A

Description of Soil Series Crossed by NEXUS Project Facilities

Soil Series in Ohio

Alexandria silt loam (AgF)
This deep, very steep, well-drained soil is on the side slopes along streams and drainageways on till plains. Slopes range from 25 to 50 percent. Depth to bedrock is greater than 80 inches. The seasonal high water table ranges in depth from 48 to 72 inches during extended wet periods. Permeability is slow and runoff is rapid due to the slope. Most of the areas are used as woodland due to the potential for erosion if the land was cleared for pasture or crops. These soils are not classified as hydric.

Allis clay loam (AkA)
The Allis series soils consist of moderately deep soils. These nearly level soils are on till plains and lake plains. Slopes range from 0 to 2 percent. These soils formed in glacial till that is 20 to 40 inches deep over shale. Depth to bedrock is 36 inches. Runoff is medium and permeability is slow or very slow. Allis soils have a high water table during wet seasons, typically 0 to 1 foot. These soils are classified as hydric.

Amanda-Dekalb-Rock Outcrop association (AnG)
The Amanda series consists of very deep, well drained soils formed in loamy till and a thin layer of loess in some areas. Depth to bedrock is greater than 60 inches. These soils are on end moraines and ground moraines. Slopes range from 2 to 70 percent. The potential for surface runoff is low to high. The Amanda component makes up 50 percent of the map unit. These are not classified as hydric.

The Dekalb component makes up 25 percent of the map unit. Slopes are 40 to 70 percent. This component is on backslopes. The parent material consists of sandstone residuum. Depth to root restrictive layer, sandstone bedrock, is 20 to 40 inches. The natural drainage class is well drained. Permeability is rapid. Depth to seasonably high water table is more than 6 feet. There is a slight hazard of wind erosion. These soils are not classified as hydric.

Amanda Loam (AmF)
The Amanda loam series consists of very deep and well-drained soils formed in loamy till and a thin layer of loess in some areas. The depth to bedrock is greater than 60 inches. These soils are found on end moraines and ground moraines. Slopes range from 35 to 70 percent. Rock fragments consist of partially weathered, angular or subrounded fragments of sandstone and shale of local origin with minor amounts of limestone and crystalline rocks. Depth to the top of an intermittent perched high water table ranges from 3.5 to 6 feet between December and May in normal years. These soils are not classified as hydric.

Aquents, nearly level (An)
Aquents consist of silt loams or silty clay loams and are in areas where the landscape has been altered by construction activities. They are located on flats or in the slight depressions with some areas used as a source of borrow material. Slopes range from 0 to 2 percent. The soil is a mixture of material from the subsoil and substratum of natural soils. In some places, much of the surface layer, subsoil, or substratum has been removed and in other places soil has been added. The available water capacity varies, and the content of the organic matter is generally very low. These soils have a seasonal high water table in most areas, especially in depressions or bowl shaped areas where water can accumulate. Most areas only have sparse vegetation due to the surface layer crusting after hard rains. These soils are classified as hydric.

Aurand fine sandy loam (AmA, AnA)
The Aurand series consists of very deep, somewhat poorly drained soils that are deep to dense till. These soils formed in glaciolacustrine material 20 to 40 inches thick and the underlying till. The soils can be found on lake plains and beach ridges. Slopes range from 0 to 2 percent. The depth to the top of an intermittent perched high water table ranges from 0.5 to 1.5 feet between December and May in normal years. The potential for surface runoff is very low to medium. Depth to bedrock is greater than 80 inches. Permeability is moderate in the upper part of the solum, and slow or very slow in the substratum. This soil is not classified as hydric.

Belmore loam (BaB)

The belmore series consists of deep, well drained soils formed in loamy and gravelly outwashand are underlain by gravelly, sandy and loamy outwash deposits. They are on terraces, outwash plains and glacial drainage channels. Slopes range from 2 to 6 percent. Depth to bedrock is greater than 77 inches. The potential for surface runoff is negligible to medium. Permeability is moderately rapid in the solum and rapid in the underlying material. This soil is not classified as hydric.

Bennington silt loam (BgA, BnA, BgB, BnB)

The Bennington silt loam series is very deep, somewhat poorly drained soils located on ground moraines and lake plains. Slopes range from 0 to 6 percent. Depth to bedrock is greater than 80 inches. The parent material consists of till. Depth to seasonal high water table is 1 to 2.5 feet due to a perched water table. Root restrictive layer between 25 and 50 inches. Permeability is slow in the substratum. Slight wind erosion hazard. These soils are not classified as hydric.

Berks channery silt loam (BkD, BkB, BkE, BkC)

The Berks channery silt loam consists of moderately deep, well drained soils. Parent material consists of residuum weathered from interbedded sedimentary rock. Depth to bedrock is 20 to 40 inches. Slopes range from 0 to 40 percent. Permeability is moderate or moderately rapid above the bedrock. The potential for surface runoff is high. Depth to the seasonal high water table is greater than 1.9 feet. These soils are not classified as hydric.

Bethesda and Fairpoint channery silt loams (BtF4F1)

The Bethesda component consists of very deep, well drained soils that are located on shoulders, backslopes, or summits. Slopes range from 25 to 70 percent. Parent material consists of acid residuum of fine earth and rock fragments from coal extraction mine spoil derived from interbedded sedimentary rock. Permeability is moderately slow or slow. Depth to bedrock is greater than 80 inches. The potential for surface runoff is high. These soils are not classified as hydric.

The Fairpoint component consists of very deep, well drained soils that are located on shoulders backslopes, or summits. Slopes range from 25 to 70 percent. Parent material consists of medium acid residuum of fine earth and rock fragments from coal extraction mine spoil derived from interbedded sedimentary rock. Permeability is moderate or moderately slow. Depth to bedrock is greater than 80 inches. The potential for surface runoff is very high. These soils are not classified as hydric.

Bixler loamy fine sand (BkA, BxA, BkB, BxB)

The Bixler loamy fine sand series consists of very deep, somewhat poorly drained soils that are located on flat areas, rises, and knolls. Slopes range from 0 to 6 percent. Depth top bedrock is greater than 80 inches. Permeability is rapid in the sandy materials and moderate in the stratified lacustrine deposits. Seasonal high water table ranges from 1.5 to 3.0 feet. The Bixler series has a severe wind erosion hazard. These soils are not classified as hydric.

Bogart loam (BtA, BgA, BtB, BgB)

The Bogart loam series soils consist of deep, nearly level, moderately well-drained soils located on the flat part of stream terraces and on outwash plains. Slopes range from 0 to 6 percent. Depth to bedrock is greater than 60 inches. Permeability is moderate or moderately rapid in the subsoil and rapid in the substratum. The seasonal high water table ranges from 24 to 42 inches. Runoff is slow. The main management concern is droughtiness. These soils are not classified as hydric.

Bogart silt loam (BoA, BtB, BoB)

The Bogart silt loam series soils are deep, gently sloping, moderately well-drained soils located in slightly convex areas on stream terraces, outwash plains, and Kames. Slopes range from 2 to 6 percent. Depth to bedrock is greater than 60 inches. Permeability is moderate or moderately rapid in the subsoil and rapid in the substratum. The seasonal high water table ranges from 24 to 42 inches during extended wet periods.

Surface runoff is medium. A moderate hazard is the main concern in management of these soils. These soils are not classified as hydric.

Canadice silty clay loam (Ca)
Canadice silty clay loam series soils consist of nearly level, very deep, poorly drained soils formed dominantly in clayey glaciolacustrine sediments on wisconsinan age lake plains, slackwater terraces and valley floors. The Canadice silt loams occur in swales and in somewhat depressional areas that are commonly dissected by small streams. Included in the soil mapping are areas of small shallow depressions that are very poorly drained and have a mucky surface layer. These areas are also subject to flooding during periods of heavy rainfall and spring snow melt. Slopes range from 0 to 3 percent. Permeability is very slow. The potential for surface runoff is negligible to high. Depth to bedrock is greater than 60 inches. Depth to an intermittent apparent water table is .5 to 1.0 feet from November to June. These soils are classified as hydric.

Caneadea silt loam (CcA)
Caneadea series soils consist of very deep somewhat poorly drained nearly level to strongly sloping soils on slackwater terraces of lake plains and valley floors of depressional landscapes. Slopes range from 0 to 2 percent. Depth to bedrock is greater than 60 inches. Permeability is very slow. The potential for surface runoff is negligible to high. Depth to intermittent perched water table is .5 to 1.0 feet from November to May. Seasonal wetness and very slow permeability are the limitations for non-farming. These soils are not classified as hydric.

Canfield silt loam (CdA, CdD2, CcD, CcB, CdB, CdB2, CcE, CdC, CcC, CdC2)
Canfield series soils consist of very deep, well-drained soils formed in wisconsinan age till plains. Slopes range from 0 to 12 percent. Depth to bedrock is greater than 80 inches. Soils have a root restrictive fragipan layer 18 to 30 inches from the soil surface. Permeability above the fragipan is moderate and slow below it. The potential for surface runoff is medium to high depending on the slope. Seasonal high water table (perched) is 1.2 to 2.3 feet. These soils are not classified as hydric.

Canfield silt loam sandstone substratum (CeB)
The Canfield silt loam sandstone substratum has the same soils description as above, but is underlain by sandstone bedrock at a depth of 40 to 60 inches. Slopes range from 2 to 6 percent. The depth to bedrock are limitations to some nonfarm uses. These soils are not classified as hydric.

Cardington silt loam (CgE2, CaB, CgB CgC2)
The Cardington silt loam series soils consist of very deep, moderately well-drained soils formed in till of medium lime content. These soils are located on summits, shoulders and backslopes on ground morains and end morains. Slopes range from 2 to 25 percent. Depth to bedrock is at 78 inches. Permeability is slow. The potential for surface runoff is negligible to high. The depth to the intermittent perched seasonal high water table is 1 to 2 feet between November and April. A root restrictive layer comprised of unweathered till is located 28 to 50 inches below the soil surface. These soils are not classified as hydric.

Cardington silty clay loam (CbC2)
The Cardington silt loam series soils consist of very deep, moderately well-drained soils formed in till of medium lime content. These soils are located on dissected areas on ground morains. Slopes range from 6 to 12 percent. Depth to bedrock is at 78 inches. Permeability is slow. The potential for surface runoff is negligible to high. The depth to the intermittent perched seasonal high water table is 1 to 2 feet between November and April. A root restrictive layer comprised of unweathered till is located 28 to 50 inches below the soil surface. These soils are not classified as hydric.

Carlisle muck (Cg, Ch)
Carlisle muck consists of very deep, nearly level, very poorly drained soils formed in woody and herbaceous organic materials in depressions within lake plains, outwash plains, flood plains, ground

morrains, and morrains. Most of these soils are located within swampy low-lying areas. Slopes range from 0 to 2 percent. Depth to bedrock is greater than 60 inches. Permeability is moderately slow to moderately rapid. The potential for surface runoff is low or negligible. The seasonal high water table ranges from 2 feet above the surface to 1 foot below the surface. These soils are too wet for crops unless they are drained. These soils are classified as hydric.

Castalia very cobbly loam (CaA)

The Castalia very cobbly loam series soils consist of moderately deep, well drained soils found on knolls and rises on reefs on lake plains. Slopes range from 0 to 2 percent. Permeability is rapid. Depth to bedrock is 20 to 40 inches. Parent material consists of loamy and sandy beach or eolian deposits mixed with glacially displaced limestone or dolostone fragments of local origin. The depth to the seasonally high water table is 1.7 feet. Surface runoff is considered low with a slight chance of wind erosion. These soils are not classified as hydric.

Castalia very channery loam (CcA, CcB)

Castalia very channery loam series soils consists of moderately deep, well-drained soils formed on reefs and lake plains. Slopes range from 0 to 6 percent. Depth to bedrock is 20 to 40 inches. Permeability is rapid. Parent material consists of beach or eollian sediments mixed with glacially displaced limestone fragments overlying limestone or dolostone. The depth to the seasonally high water table is over 6 feet. The hazard of wind erosion is slight. These soils are not classified as hydric.

Castalia very stony loam (ChB)

Castalia very stony loam series soils consists of moderately deep, nearly level and gently sloping, well-drained soils located on knolls and slight rises on lake plains. Slopes range from 1 to 6 percent. This soil contains stones on the surface measuring 4 inches to almost 4 feet across that can be 5 to 30 apart. Depth to bedrock is between 20 and 40 inches. Permeability is rapid and runoff is slow. The soil is poorly suited for cultivation and pasture land. These soils are not classified as hydric.

Castalia-Marblehead complex very stony (CbB)

Castalia-Marblehead complex very stony consists of moderately deep, well-drained soils formed on knolls and rises on reefs on lake plains. These soils can be found on backslopes, summits and shoulders. Slopes range from 0 to 6 percent. Depth to bedrock is 20 to 40 inches. Permeability is rapid and run off is very low. Depth to seasonal high water table is more than 1.8 feet. Parent material consists of loamy and sandy beach or eolian deposits mixed with glacially displaced limestone or dolostone fragments of local origin. These soils are not classified as hydric.

Chagrin silt loam, alkaline and alkaline phase (Ck)

The Chagrin series consists of deep, well drained moderately permeable soils that formed in alluvium on flood plains. Although this soil is mildly alkaline, it retains the same series description. Slopes range from 0 to 3 percent. Chagrin soils are located on flood plains receiving alluvium mainly from upland areas of sandstone, siltstone, shale, limestone, and low-lime glacial drift. Surface runoff is slow and permeability is moderate. Flooding is the hazard associated with this soil. These soils are not classified as hydric.

Chili gravelly loam (CoD2, CoE2, CoC, CoC2)

The Chili gravelly loam series consists of deep, moderately steep and steep, well-drained soils on kames and stream terraces. Slopes range from 6 to 25 percent. Depth to bedrock is greater than 60 inches. The present surface layer is a mixture of the original surface layer and the subsoil material due to erosion. Included with this soil are seeps and springs. Permeability is moderately rapid. The root zone is deep and the runoff is rapid. This soil is a good source for sand and gravel. These soils are not classified as hydric.

Chili loam (ClA, CnA, CnB, CnC)

The Chili loam soils consist of deep, well-drained soils on broad outwash plains and on stream terraces and low kames. Slopes range from 0 to 12 percent. Depth to bedrock is greater than 60 inches.

Permeability is moderately rapid. The available water capacity is moderate. Runoff is medium to rapid depending on slope. Erosion and slight droughtiness are the main concerns in management. These soils are not classified as hydric.

Chili loam, loamy substratum (ChB)
The Chili loam, loamy substratum consists of very deep, well-drained soils on beach ridges, lake plains and stream terraces. Slopes range from 2 to 6 percent. Root zone extends to more than 80 inches. Depth to seasonal high water table is more than 6 feet. Permeability is moderately rapid. The hazard of wind erosion is slight. The substratum is 41 to 80 inches in depth and consists of friable gravelly sandy loam from 41 inches to 77 inches and friable loam from 77 inches to 80 inches. These soils are not classified as hydric.

Chili silt loam (CpA, CpB, ChC, CpC, CpC2)
The Chili silt loam soils have the same profile as described by the series except that the surface layer and upper part of the subsoil have a higher content of silt. The Chili series consists of very deep, well-drained soils on outwash plains, terraces kames, and beach ridges. Slopes range from 0 to 12 percent. The soils formed in Wisconsinan age stratified outwash derived largely from non-calcareous sandstone and shale that contains a high amount of quartz gravel. Commonly, the outwash is mantled with silt. The potential for runoff is negligible to high. Permeability is moderately rapid in the subsoil and rapid in the substratum. These soils are not classified as hydric

Chili-Wooster complex (CwC2)
The Chili series component consists of very deep, well-drained soils on outwash plains, terraces kames, and beach ridges. Slopes range from 6 to 12 percent. Depth to bedrock is greater than 60 inches. The soils formed in Wisconsinan age stratified outwash derived largely from non-calcareous sandstone and shale that contains a high amount of quartz gravel. Commonly, the outwash is mantled with silt. The potential for runoff is negligible to high. Permeability is moderately rapid in the subsoil and rapid in the substratum. These soils are not classified as hydric

The Wooster series component consists of deep, well drained soils formed in low-lime loamy glacial till with a thin loess mantle in some places. Slopes range from 2 to 50 percent. Depth to bedrock is greater than 85 inches. Permeability is moderate above the fragipan and moderately slow in the fragipan. Depth to the fragipan ranges from 18 to 40 inches. Coarse fragments are dominantly sandstone, but include shale and a few crystalline rocks. Runoff is medium to very rapid. Permeability is moderate above the fragipan and moderately slow in the fragipan. These soils are not classified as hydric.

Colonie fine sand (CoB, CoC)
The Colonie series consists of very deep, well drained to excessively drained soils formed in glaciolucustrine, glaciofluvial, or eolian deposits dominated by sand and very fine sand. The soils are found on nearly level to steeply dissected slopes on Wisconsinan age lake plains, dunes outwash plains, beach ridges, and deltas. Depth to bedrock is greater than 80 inches. The potential for surface runoff ranges from negligible to medium. These soils are not classified as hydric.

Colwood fine sandy loam (Co)
The Colwood fine sandy loam consists of nearly level, deep, very poorly drained soil that is located on flats and in depressions on lake plains and outwash plains. Slopes range from 0 to 2 percent. Depth to bedrock is greater than 60 inches. The lower parts of the depressions can be ponded by runoff from higher lying adjacent soils. Permeability is moderate. The content of organic matter is high. Runoff is very slow or ponded. The seasonal high water table is near or above the surface. These soils are classified as hydric.

Colwood loam (Co, CmA)
The Colwood loam series soils consist of very deep, poorly and very poorly drained soils that are formed on lake plains. These soils are located on extensive flat areas, drainageways, and depressions. Slopes

range from 0 to 1 percent. The seasonal high water table is apparent and is 1 foot above the surface to 1 foot below the surface. Root zone extends to a depth past 80 inches. Permeability is moderately slow in the subsoil. There are very brief periods of ponding associated with this soil. These soils are classified as hydric.

Colwood silt loam, bedrock substratum (CnA)
The Colwood silt loam, bedrock substratum soils consist of deep, poorly drained and very poorly drained soils that are formed on lake planes. These soils are located on extensive flat areas and depressions. Slopes range from 0 to 1 percent. The seasonal high water table is apparent and is 1 foot above the surface to one foot below the surface. Depth to bedrock is 40 to 60 inches. Permeability is moderately slow. There are very brief periods of ponding associated with the soil. These soils are classified as hydric.

Condit silt loam (CoA, Cy)
The Condit silt loam series consists of very deep, very poorly drained soils that are formed on ground morains. These soils can be found in extensive flat areas, drainageways, and depressions. Slopes range from 0 to 1 percent. The seasonal high water table is perched and is 1 foot above the surface to 1 foot below the surface. Bedrock extends to a depth below 80 inches. Permeability is slow. There are brief periods of ponding associated with these soils. These soils are classified as hydric.

Conotton gravelly loam (CyD2, CyE2, CyB, CuC)
The Conotton gravelly loam series consists of very deep, well drained soils formed in Wisconsinan age stratified outwash deposits. These soils can be found on outwash plains, stream terraces, kames eskers, and beach ridges. Slopes range from 2 to 25 percent. Depth to seasonal high water table is greater than 6 feet below the surface. Depth to bedrock is greater than 80 inches. Permeability is rapid. The potential for surface runoff is negligible to medium. These soils are not classified as hydric.

Conotton loam (CtB)
The Conotton loam series soils consist of very deep, well drained soils formed in Wisconsinan age stratified outwash deposits. These soils can be found on outwash plains, stream terraces, kames eskers, and beach ridges. Slopes range from 2 to 6 percent. Depth to seasonal high water table is more than 6 feet below the surface. Depth to bedrock is greater than 80 inches. Permeability is rapid. The potential for surface runoff is negligible to medium. These soils are not classified as hydric.

Conotton-Oshtemo complex (CyD, CyE, CyF)
The Conotton-Oshtemo complex consists of very deep, well drained Conotton and Oshtemo soils. Slopes range from 12 to 50 percent. Conotton series makes up approximately 50 to 60 percent of the complex, while the Oshtemo series makes up 20 to 30 percent of the complex. Depth to bedrock is greater than 80 inches. Conotton soils are typically located on kames and sides of drainageways, while the Oshtemo series are located on outwash plains valley trains, moraines, and beach ridges. Permeability for both soils is rapid. This soil complex is not classified as hydric

Coshocton silt loam (CoC)
The Coshocton series consists of deep to very deep, moderately well drained soils that formed in residuum weathered from interbedded shale, siltstone, sandstone, and occasional thin strata of coal, coal underclay, and limestone. Depth to bedrock is 40 to 84 inches. Coshocton soils are located on hill slopes, summits, shoulders and back slopes. Slopes range from 6 to 15 percent. The rock fragment ranges from 2 to 20 percent within Coshocton series. These soils are not classified as hydric.

Damascus loam (Da)
The Damascus series consists of deep, poorly drained, nearly level soils formed in sandy and loamy outwash material of Wisconsin age. These soils are found on outwash terraces. These soils are nearly level to depressional areas. Permeability is moderate in the solum over rapid or very rapid in the

substratum. Runoff is slow. Depth to bedrock is greater than 75 inches. These soils are ponded in the spring, fall and portions of the summer. These soils are classified as hydric.

Dekalb sandy loam (DkF)
The Dekalb series soils consist of moderately deep, well drained sloping to very steep soils. These soils formed in residuum weathered from coarse-grained, acid sandstone. These soils are located on the upper parts of hillslopes. Slopes range from 25 to 70 percent. Depth to sandstone bedrock is 36 inches. Permeability is rapid above the bedrock. Seeps or springs occur along the lower slopes in some areas. Erosion is a severe hazard if the soil is cultivated. Runoff is medium to rapid. These soils are not classified as hydric.

Del Rey loam (DdA, DeA)
The Del Rey series soils consist of somewhat poorly drained, nearly level soils on outwash plains and deltas. These soils are found on slight rises and broad flats. Slopes range from 0 to 3 percent. Depth to bedrock is greater than 60 inches. Permeability is slow in the subsoil and rapid in the substratum. Runoff is slow. These soils are not classified as hydric.

Del Rey silt loam (DeA)
The Del Rey series soils consist of somewhat poorly drained, nearly level to gently sloping soils on the lower parts of the undulating topography and on broad flats of the lake plain. These soils formed in lacustrine deposits. Slopes range from 0 to 2 percent. Depth to bedrock is greater than 60 inches. Permeability is slow. These soils have a perched water table in the winter and in the spring. These soils are not classified as hydric.

Digby loam (DmA)
The Digby series soils consists of very deep, somewhat poorly drained soils located on flats and rises on beach ridges on lake plains. Slopes range from 0 to 3 percent. Depth to bedrock is greater than 60 inches. Depth to the top of the seasonal high water table is 0.5 foot to 1.5 feet. Permeability is moderate in the solum and rapid in the substratum. Surface runoff is negligible. There is no ponding associated with these soils. These soils are not classified as hydric.

Digby sandy loam (DgA)
The Digby series soils consists of very deep, somewhat poorly drained soils located on flats and rises on beach ridges on lake plains. Slopes range from 0 to 2 percent. Depth to bedrock is greater than 60 inches. Depth to the top of the seasonal high water table is 0.5 foot to 1.5 feet. Permeability is moderate in the solum and rapid in the substratum. Surface runoff is negligible. There is no flooding or ponding associated with these soils. Wind erosion potential is moderate. These soils are not classified as hydric.

Dixboro fine sandy loam (DsA)
Dixboro series soils consist of nearly level, somewhat poorly drained soil located on outwash plains and deltas. These soils can be found on low ridges and oval on low knolls. Slopes range from 0 to 2 percent. Depth to bedrock is greater than 60 inches. Permeability is moderate and runoff is slow. The seasonally high water table is near the surface during extended wet periods. Drainage is the main management concern. These soils are not classified as hydric.

Dixboro-Kibbie complex (DkA)
The Dixboro-Kibbie complex consists of deep, nearly level, somewhat poorly drained soils that are found on broad flats and slight rises on lake plains and deltas. Slopes range from 0 to 2 percent. The complex consists of approximately 65 percent Dixboro soils and 25 percent Kibbie soils. Permeability is moderate in the Dixboro and Kibbie soils. Runoff is slow for both soils. They have a seasonally high water table at a depth of 12 to 24 inches during extended wet periods. These soils are not classified as hydric.

Dunbridge loamy sand (DuA, DuB)

The Dunbridge loamy sand series soils consist of moderately deep, well drained soils formed in sandy and loamy drift overlying limestone or dolostone. Slopes range from 0 to 6 percent. Depth to limestone bedrock is between 20 and 40 inches. Depth to seasonal high water table is more than 6 feet. Permeability is moderately rapid. These soils have a severe wind erosion hazard. These soils are not classified as hydric.

Dunbridge sandy loam (DuB)

The Dunbridge sandy loam series soils consist of shallow to deep, well drained soils formed in sandy and loamy glaciolacustrine deposits overlying limestone or dolostone. Slopes range from 1 to 4 percent. Depth to lithic bedrock is 18 to 42 inches. Depth to seasonal high water table is more than 2.5 feet. There is no flooding or ponding associated with these soils. Permeability is moderately rapid in the upper part of the solum and moderately rapid in the lower part of the solum. These soils have a moderate wind erosion hazard. These soils are not classified as hydric.

Dunbridge-Spinks, deep to limestone, loamy fine sands (DsB)

The Dunbridge series soils associated with the complex consists of shallow to deep, well drained soils formed in sandy and loamy glaciolacustrine deposits overlying limestone or dolostone. Slopes range from 2 to 6 percent. Depth to lithic bedrock is 18 to 42 inches. Depth to seasonal high water table is more than 2.1 feet. There is no flooding or ponding associated with these soils. Permeability is moderately rapid in the upper part of the solum and moderately rapid in the lower part of the solum. Surface runoff is negligible. These soils have a severe wind erosion hazard. These soils are not classified as hydric.

The Spinks series soils associated with the complex consist of deep, well drained soils formed in sandy eolian or glaciolacustrine deposits overlying limestone or dolostone. Slopes range from 0 to 6 percent. Depth to lithic bedrock is 42 to 60 inches. Depth to seasonal high water table is more than 4.2 feet. There is no flooding or ponding associated with these soils. Permeability is moderately rapid or rapid. Surface runoff is negligible. These soils have a severe wind erosion hazard. These soils are not classified as hydric.

Eel loam (Ee)

The Eel loam series soils consist of very deep, moderately well drained soils formed in loamy alluvium. These soils are found on flats, rises, and natural levees on flood plains. Slopes range from 0 to 2 percent. Depth to bedrock is greater than 60 inches. Depth to seasonal high water table is 1.5 to 2 feet. This soil frequently floods. Permeability is moderate in the solum and moderate or moderately rapid in the substratum. Surface runoff is negligible. These soils have a slight wind erosion hazard. These soils are not classified as hydric.

Elliott silt loam bedrock substratum (EcA)

The Elliot series soils consist of very deep somewhat poorly drained soils formed in till overlying limestone. These soils are found on flat areas, slight rises, and toeslopes near depressions. Slopes range from 0 to 2 percent. Depth to bedrock is 65 to 67 inches. Depth to the seasonal high water table is 1 to 2 feet from the soil surface. Potential for surface runoff is low to high. Permeability is slow or moderately slow in the substratum. These soils have a slight wind erosion hazard. These soils are not classified as hydric.

Ellsworth (EID2, ElE2, ElB, ElB2, ElF, ElC, ElC2)

The Ellsworth series soils consist of very deep, moderately well drained soils formed in till. These soils are found on backslopes, shoulders and summits. Slopes range from 2 to 70 percent. Depth bedrock is greater than 80 inches. Depth to seasonal high water table is 1.5 to 3 feet from the soil surface. Permeability is very slow or slow in the substratum. These soils have a slight wind erosion hazard. These soils are not classified as hydric.

Elnora loamy fine sand (EnA)
The Elnora series soils consist of very deep, moderately well drained soils formed in sandy lacustrine deposits. These soils are found on rises, summits, backslopes and shoulders. Slopes range from 0 to 4 percent. Depth to bedrock is greater than 80 inches. Depth to seasonal high water table is 1.5 to 2.0 feet from the soil surface. Permeability is rapid. These soils have a severe wind erosion hazard. These soils are not classified as hydric.

Euclid silt loam, occasionally flooded (EvA)
The Euclid series soils consist of deep, nearly level, somewhat poorly drained soil on low stream terraces. These soils were formed in stratified silty deposits derived from materials high in sandstone and shale on treads on low stream terraces. Slopes range from 0 to 2 percent. This soil is subject to occasional flooding for very brief periods in the winter and spring. The seasonal high water table is between depths of 12 and 30 inches during extended wet periods. Runoff is slow. Depth to bedrock is greater than 74 inches. Permeability is moderate in the surface layer and moderately slow in the subsoil and substratum. These soils are not classified as hydric.

Fairpoint silty clay loam (FcD)
The Fairpoint series consists of very deep, well drained soils originating from coal extraction mine spoil derived from nonacid regolith of weathered fine- earth and fragments of neutral to calcareous shale, sandstone and siltstone. Depth to bedrock is about 60 inches. These soils are located on hill slopes, summits, shoulders, back slopes, foot slopes, surface mines, spoil piles, and reclaimed lands. Slopes range from 8 to 25 percent. Rock fragment size ranges from 2 mm to 25 cm, but can include stones and boulders. These soils are not classified as hydric.

Fitchville silt loam (FcA, FdA, FcB)
The Fitchville series consists of very deep, somewhat poorly drained soils formed in stratified Wisconsinan age glaciolacustrine sediments on lake plains and slackwater terraces. Slopes range from 0 to 6 percent. Depth to bedrock is greater than 80 inches. Permeability is moderate in the surface, moderately slow in the subsoil and moderate or moderately slow in the substratum. There is no ponding or flooding associated with this soil. The potential for surface runoff is low to high. Depth to the top of an intermittent apparent seasonal high water table ranges from 0.5 to 1.0 foot from November to May. These soils are not classified as hydric.

Fluvaquents, silty (FeA)
Fluvaquents series consists of very deep very poorly drained soils that were formed in alluvium. These soils that are located on flood plains which are perennially covered by water. The soil material consists of dark and light colored stratified sandy, loamy, silty or clayey alluvial deposits. Slopes range from 0 to 1 percent. Depth to bedrock is greater than 80 inches. The seasonal high water table is at or near the surface. Permeability is slow to rapid. Flooding happens frequently and ponding can occur for long durations. The potential for surface runoff is negligible. These soils are classified as hydric.

Fredericktown gravelly loam (FnC2)
The Fredericktown gravelly loam series soil consists of very deep, well drained soils formed in loess over glaciofluvial outwash. These soils are located on stream and kame terraces. Slopes range from 6 to 15 percent. Depth to bedrock is greater than 80 inches. The seasonal high water table is greater than 6 feet below the soil surface. Permeability is moderate to rapid. These soils do not pond or flood. The potential for surface runoff is low. These soils have a slight wind erosion hazard. These soils are not classified as hydric.

Fredericktown silt loam (FoB)
The Fredericktown series consists of very deep, well drained soils formed in early Wisconsinan or Illinoian age outwash, with or without a thin loess mantle, on stream terraces and kame terraces. Slopes range from 2 to 6 percent. Permeability is moderate in the surface, moderately rapid or rapid in the subsoil

and rapid in the substratum. The potential for surface runoff is medium to negligible. Depth to bedrock is greater than 80 inches. These soils are not characterized as hydric.

Frenchtown silt loam (Fr)
The Frenchtown series consists of very deep, poorly drained soils formed in loamy till on plains. Slopes range from 0 to 8 percent. Depth to bedrock is greater than 80 inches. The depth to an intermittent perched water table ranges from 0.5 feet above the surface to 0.5 feet below the surface. Frequent brief and very brief ponding occurs during periods of heavy rainfall and snowmelt. Permeability is moderate above the fragipan and slow or very slow in the fragipan. These soils have a slight wind erosion hazard. These soils are classified as hydric.

Fries silty clay loam (FrA)
The Fries soil series consists of moderately deep, very poorly drained soils formed in glacial till or lacustrine deposits overlaying shale bedrock on till plains and lake plains. Slopes range from 0 to 1 percent. Depth to bedrock is 28 to 30 inches. Seasonal high water table ranges from 1 foot below the surface to 1 foot above the surface. Permeability is slow. The potential for surface runoff is negligible or low. These soils briefly pond during heavy rain events and snowmelt. These soils have a slight wind erosion hazard. These soils are classified as hydric.

Gilford fine sandy loam (Gf)
The Gilford series consists of very deep, poorly drained and very poorly drained soils formed in loamy over sandy sediments on outwash plains, near-shore zones (relict), and flood-plain steps. These soils can be found on flat areas, depressions and drainageways. Slopes range from 0 to 1 percent. Depth to bedrock is greater than 80 inches. The seasonal high water table ranges from 0.5 foot above the surface to 1.0 foot below the surface. Permeability is rapid in the lower part of the subsoil and in the substratum. This soil experiences brief periods of ponding. These soils have a moderate wind erosion hazard. These soils are classified as hydric.

Gilpin silt loam (GnD, GnB, GnC)
The Gilpin series consist of moderately deep, well drained soils formed in residuum from interbedded gray and brown acid siltstone, shale and sandstone. Depth to bedrock ranges from 20 to 40 inches. These soils are found on interfluves, head slopes, nose slopes and side slopes of upland ridges, hills and hillslopes. Slopes range from 2 to 25 percent. Rock content is 5 to 40 percent, by volume, in the solum and 30 to 90 percent, by volume, in the C horizon. Rock fragments are mostly angular to subangular channers of shale, siltstone, and sandstone. These soils are not classified as hydric.

Glenford silt loam (GfA, GtB, GfB, GfC, GfC2)
The Glenford series consists of very deep, moderately well drained soils formed in stratified Wisconsinan age glaciolacustrine or stream sediments derived from materials high in sandstone and shale. Depth to bedrock is greater than 60 inches. These soils are found on summits, shoulders and side slopes on lake plains and on risers and treads on terraces of streams and outwash plains. Slopes range from 0 to 12 percent. Rock fragments are typically absent, but range up to 3 percent in the BC horizon and 10 percent in the C horizon. Stratification is evident within the series control section. Depth to the top of an intermittent apparent seasonal high water table is from 1 to 2 feet from December to April in normal years. These soils are not classified as hydric.

Glynwood clay loam (GoC3)
The Glynwood clay loam series consists of very deep, moderately well drained soils that are moderately deep or deep to dense till. They formed in a thin layer of loess and the underlying clay loam or silty clay loam till. The depth to bedrock is greater than 80 inches. These soils are found on side slopes of ridges and on breaks of slopes along drainageways. Slope ranges from 6 to 12 percent. In some areas, the substratum is at the surface. Rock fragments are dominantly limestone and crystalline glacial erratics. The depth to the top of an intermittent perched high water table ranges from 2 to 3.5 between during extended

wet periods. Permeability is slow in the solum and slow or very slow in the dense till. These soils are not classified as hydric.

Glynwood silt loam (GwB)
The Glynwood silt loam series consists of deep, moderately well drained soils that are moderately deep or deep to dense till. They formed in a thin layer of loess and the underlying clay loam or silty clay loam till. The depth to bedrock is greater than 80 inches. These soils are found on knolls, ridges and on side slopes at the head of drainageways. Slope ranges from 2 to 6 percent. Rock fragments are dominantly limestone and crystalline glacial erratics. The depth to the top of an intermittent perched high water table ranges from 2 to 3.5 feet during extended wet periods. Permeability is slow in the solum and slow or very slow in the dense till. These soils are not classified as hydric.

Granby loamy fine sand (Gr)
The Granby series consists of very deep, poorly drained or very poorly drained soils formed in sandy outwash or sandy glaciolacustrine deposits. The depth to bedrock is greater than 80 inches. These soils are found on outwash plains, lake plains, and glacial drainageways. Slopes range from 0 to 3 percent.

The particle-size control section averages less than 10 percent clay. The sand fraction has a high percentage of fine and very fine sand. Permeability in these soils is rapid and they are not classified as hydric.

Haskins loam (HkA, HsA, HnA, HsB)
The Haskins series consists of very deep, somewhat poorly drained soils that are moderately deep or deep to dense till. They formed in loamy water-sorted or glaciolacustrine material 20 to 40 inches thick and in the underlying till. The depth to bedrock is greater than 80 inches. Depth to the underlying till is 30 to 60 inches. These soils are found on lake plains and till plains. Slopes range from 0 to 6 percent. Rock fragments consist of glacial erratics, primarily of limestone, dolostone, and crystalline lithology. The depth to the top of an intermittent perched high water table ranges from 0.5 to 1.5 feet between November and April in normal years. These soils are not classified as hydric.

Haskins Sandy loam (HaB)
The Haskins sandy loam series consists of deep, somewhat poorly drained soils that are moderately deep or deep to dense till. They formed in loamy water-sorted or glaciolacustrine material 20 to 40 inches thick and in the underlying till. The depth to bedrock is greater than 80 inches. Depth to the underlying till is 30 to 60 inches. These soils are found on lake plains, stream terraces and till plains. Slopes range from 1 to 4 percent. Rock fragments consists of glacial erratics, primarily of limestone, dolostone, and crystalline lithology. The depth to the top of an intermittent perched high water table ranges from 1 to 2.5 feet during extended wet periods. These soils are not classified as hydric.

Hazleton channery loam (HeE, HeC, HeD)
The Hazleton series consists of deep and very deep, well drained soils formed in residuum of acid gray, brown or red sandstone. Depth to bedrock (lithic contact) ranges from 40 to 80 inches. Slopes range from 6 to 40 percent. These soils are found in upland summits, shoulders and the upper third of backslopes. Slopes are usually convex with gradients of 0 to 80 percent. Rock fragments of angular sandstone, dominantly less than 10 inches in size, range from 5 to 70 percent in individual horizons of the solum and from 35 to 80 percent in the C horizon. Boulders, stones, flags and channers cover about 5 to 60 percent of the surface of some pedons. These soils are not classified as hydric.

Holly silt loam (Ho, Hy, HoA)
The Holly series consists of very deep, very poorly and poorly drained soils formed in loamy alluvium. The depth to bedrock is greater than 60 inches. These soils are found on broad flat areas and in slight depressions on flood plains receiving alluvium from upland areas of low-lime drift and noncalcareous sandstone and shale. Slopes range from 0 to 1 percent. The average clay content in the particle size

control section ranges from 18 to 30 percent. The depth to an intermittent apparent seasonal high water table is 1 foot above to 1 foot below the surface from October through June in normal years. These soils are subject to rare to frequent flooding and are classified as hydric.

Hornell silt loam (HrB)
The Hornell series consists of moderately deep, somewhat poorly drained soils formed in till overlying shale or siltstone. Depth to bedrock (lithic contact) ranges from 20 to 40 inches. Slopes range from 2 to 6 percent. These soils occur on bedrock-controlled uplands. Rock fragment content ranges from 0 to 35 percent, in the A horizon; 1 to 35 percent in the B horizon; and 10 to 60 percent in the C horizon. Rock fragments are dominantly channers or flagstones of shale or siltstone. In Hornell silt loam, the depth to the seasonal high water table is 0.5 to 1.5 feet. These soils are not classified as hydric.

Hornell silty clay loam (HsA)
The Hornell series consists of moderately deep, somewhat poorly drained soils formed in till overlying shale or siltstone. Depth to bedrock (lithic contact) ranges from 20 to 40 inches. Slopes range from 0 to 2 percent. These soils occur on bedrock-controlled uplands. Rock fragment content ranges from 0 to 35 percent, in the A horizon; 1 to 35 percent in the B horizon; and 10 to 60 percent in the C horizon. Rock fragments are dominantly channers or flagstones of shale or siltstone. In the Hornell silty cay loam series, the depth to the seasonal high water table is 0.5 to 1.5 feet. These soils are not classified as hydric.

Hoytville clay loam (HoA)
The Hoytville series consists of very deep, very poorly drained soils that are deep or very deep to dense till. They formed in till that has been leveled by wave action. The depth to bedrock is greater than 80 inches. The depth to dense till is 50 to 70 inches. These soils are found on lake plains. Slope ranges from 0 to 1 percent. Rock fragments consist of mixed glacial erratics (limestone, dolostone, shale, igneous and metamorphic lithologies). A perched water table ranges from 1 foot above to 1 foot below the surface from January to April in normal years. They are subject to brief periods of ponding at a depth of 1 foot. These soils are classified as hydric.

Jimtown loam (JtA)
The Jimtown series consists of very deep, somewhat poorly drained soils formed in stratified outwash deposits. The depth to bedrock is greater than 60 inches. These soils are found on stream terraces, outwash terraces, outwash plains, and beach ridges. Slopes range from 0 to 2 percent. Rock fragments are dominantly sandstone and shale, with a significant portion of igneous pebbles and cobbles. The particle size control section averages 18 to 27 percent clay and 20 to 55 percent sand. Permeability is moderate or moderately rapid in the solum and in the underlying material. The depth to an intermittent apparent water table is 0.5 to 1 foot between October and June in most years. These soils are not classified as hydric.

Jimtown silt loam (JwB)
The Jimtown silt loam series consists of very deep and somewhat poorly drained soils formed in stratified glaciofluvial outwash deposits. The depth to bedrock is greater than 80 inches. These soils are found on the tread of stream terraces. Slopes range from 2 to 6 percent. This series can contain gravelly or very gravelly layers. The depth to the top of an apparent high water table is 0.5 to 1 feet. These soils are not classified as hydric.

Joliet silt loam (JuA)
The Joliet series consists of shallow, poorly drained soils formed in 10 to 20 inches of loamy glacial drift overlying limestone or dolostone bedrock. The depth to limestone bedrock (lithic contact) is 19 inches. These soils are found on lake plains, outwash plains, and stream terraces. Slope ranges from 0 to 1 percent. An intermittent perched seasonal high water table is at a depth of 0 to 1 feet below the surface at some time during the spring in most years. These soils are classified as hydric.

Joliet silty clay loam (JoA)
The Joliet series consists of shallow, poorly drained soils formed in 10 to 20 inches of loamy glacial drift overlying limestone or dolostone bedrock. The depth to limestone bedrock (lithic contact) is 19 inches. These soils are found on lake plains, outwash plains, and stream terraces. Slope ranges from 0 to 1 percent. An intermittent perched seasonal high water table is at a depth of 0 to 1 feet below the surface at some time during the spring in most years. These soils are classified as hydric.

Kensington silt loam (KnD, KnC)
The Kensington series consists of deep, moderately well drained soils formed in loess, Illinoian age or early Wisconsinan age till, and residuum weathered from the underlying Pennsylvanian age shale, fine grained sandstone or siltstone. The till thickness ranges from 10 to 30 inches. The depth to bedrock is greater than 60 inches and consists of siltstone. These soils are found on interfluves, side slopes, nose slopes and head slopes of till plains. Slopes range from 6 to 25 percent. Permeability is moderate in the till and moderate or moderately rapid in the underlying material, above the bedrock. In undisturbed areas, the depth to a perched seasonal high water table is at a depth of 1.5 to 3.5 feet during November to April. These soils are not classified as hydric.

Kibbie fine sandy loam (KbA)
The Kibbie series consists of very deep, somewhat poorly drained soils that formed in stratified loamy and silty glaciofluvial or glaciolacustrine deposits. The depth to bedrock is greater than 60 inches.

Silty clay loam and clay loam till is below 40 inches in some pedons. Sandy substratum phases that have sand or fine sand below 40 inches are present. These soils are found on lake plains, ground moraines, outwash plains, and deltas. Slopes range from 0 to 2 percent. Rock fragment content ranges from 0 to 1 percent. In Kibbie fine sandy loam, the depth to the seasonal high water table ranges from 0.5 to 1.5 feet below the surface from November to May in normal years. These soils are not classified as hydric.

Lamson fine sandy loam (La)
The Lamson series consists of very deep, poorly drained and very poorly drained soils that formed in water sorted sediments dominated by very fine sand and fine sand in glaciofluvial, glaciolacustrine and deltaic deposits. Depth to bedrock is greater than 60 inches. These soils are found on depressional or concave areas of glacial lake plains. Slopes range from 0 to 3 percent. Rock fragments are commonly absent, but subhorizons in some pedons have up to 15 percent pebbles. These soils are classified as hydric.

Latham silt loam (LaD)
The Latham series consists of moderately deep, moderately well drained soils formed in residuum from soft acid shale, and in some areas strata of more resistant bedrock, such as siltstone, are included with the shale. The depth to bedrock is 20 to 40 inches. These soils are found on hills and hillslopes. Slopes range from 12 to 18 percent. Rock fragment content is 0 to 14 percent in the A and E horizons and 0 to 30 percent in the B horizons and substratum. The depth to a seasonal high water table is 14 to 23 inches from January to April. These soils are not classified as hydric.

Lenawee silty clay loam (Le)
The Lenawee series consists of very deep, poorly drained and very poorly drained soils formed in lacustrine deposits. Depth to bedrock is greater than 60 inches. These soils are found on lake plains and in depressional areas on moraines, outwash plains, and glacial drainageways. Slopes range from 0 to 2 percent. The seasonal high water table is near or above the surface during extended wet periods. This soil is classified as hydric.

Linwood muck (Ld)
The Linwood series consists of very deep, very poorly drained soils formed in former lakes or ponds in highly decomposed woody, organic materials underlain by loamy till at depths of 16 to 51 inches. Depth

to bedrock is greater than 60 inches. These soils are found in drainageways and depressions on end moraines, ground moraines, outwash plains, and lake plains. Slope ranges from 0 to 2 percent. The organic material is dominantly muck with areas of mucky peat or peat. Depth to the top of a seasonal high water table ranges from one foot above to one foot below the surface between November and June in normal years. These soils are classified as hydric.

Lobdell silt loam (Lb, Le)
The Lobdell series consists of very deep, moderately well drained soils that formed in recent loamy alluvium. Depth to bedrock is greater than 60 inches. These soils are found on nearly level flood plains receiving loamy alluvium from upland areas of sandstone, shale, and low lime glacial drift. Slopes range from 0 to 3 percent. Content of rock fragments in the A horizon is 0 to 5 percent, and in the Bw and C horizons commonly is 0 to 15 percent. Rock fragments are predominantly sandstone, siltstone, or shale.

Permeability is moderate in the solum and moderate or moderately rapid in the underlying material. These soils are subject to brief flooding and are not classified a hydric.

Lorain silty clay loam (Ln)
The Lorain silty clay loam series consists of very deep, very poorly drained soils that formed in Wisconsin age fine-textured glaciolacustrine sediments on lake plains, terraces and till plains. A sandy loam or loamy sand is at a depth of 40 to 60 inches. Depth to bedrock is greater than 60 inches. These soils are found in depressional areas on lake plains. Slopes range from 0 to 2 percent. Rock fragments, mainly pebbles, range from 0 to 2 percent in the solum and 0 to 5 percent in the substratum. In undrained sites, depth to the apparent water table ranges from greater than to less than 1 foot from the surface from November to June in most years and commonly ponds sometime during this time. These soils are classified as hydric.

Loudonville silt loam (LnD, LoD, LoB)
The Loudonville series consists of gently sloping to steep, moderately deep, well drained soils formed in glacial till and partly in residuum weathered from the underlying sandstone bedrock. Depth to sandstone bedrock is 20 to 40 inches. These soils are found in uplands on hillsides and sideslopes. Slopes range from 2 to 18 percent. The subsoil above the bedrock has many fragments of sandstone. These soils are not classified as hydric.

Luray silt loam (Ly, Lz)
The Luray series consists of very deep, very poorly drained soils formed in silty lacustrine material or slackwater sediments. Depth to bedrock is greater than 60 inches. These soils are found on lake plains, terraces, outwash plains, and some local areas on till plains. Slopes range from 0 to 2 percent. The Luray series has a perched water table that is near the surface for much of the year and water is likely to pond during heavy rainfall. These soils are classified as hydric.

Mahoning silt loam (MgA, MgB, MgB2)
The Mahoning series consists of very deep, somewhat poorly drained soils that formed in glacial till on uplands. Depth to bedrock is 40 to 60 inches. These are found on low-lime till on till plains. Slopes range from 0 to 6 percent. On long slopes, the Mahoning silt loam series contains internal lateral movement of water which collects in low areas and forms seeps at or near the base of slopes. A perched and/or apparent seasonal high water table can be present from 6 to 12 inches below the surface from October through June in most years. These soils are not classified as hydric.

Mahoning silt loam, sandstone substratum (MlA)
The Mahoning series consists of very deep, somewhat poorly drained soils that formed in glacial till on uplands. Depth to bedrock is 40 to 60 inches. These are found on low-lime till on till plains. Slopes are 0 to 2 percent. The Mahoning silt loam, sandstone substratum series is found near the base sandstone hills and distinguished by broken or solid sandstone bedrock at a depth of 40 to 60 inches. Just above the

sandstone is loam or clay loam till. A perched and/or apparent seasonal high water table can be present from 6 to 12 inches below the surface from October through June in most years. These are not classified as hydric.

Mahoning-Tiro silt loams (MkA, MkB)
Mahoning-Tiro silt loam complex occurs in irregularly shaped areas and is comprised of Mahoning and Tiro soils. The Mahoning series consists of very deep, somewhat poorly drained soils that formed in glacial till. Depth to bedrock is 40 to 60 inches. These are found on low-lime till on till plains. Slopes range from 0 to 6 percent. A perched and/or apparent seasonal high water table can be present from 6 to 12 inches below the surface from October through June in most years. Tiro soils consist of very deep, somewhat poorly drained soils that formed in silty lacustrine deposits. Depth to bedrock is greater than 60 inches. These are found on water modified till plains. Slopes range from 0 to 6 percent. Permeability is moderate in the upper part of the solum and moderately slow or slow in the lower part. These soils are not classified as hydric.

Mechanicsburg silt loam (McB, McC)
The Mechanicsburg series consists of deep and very deep, well drained soils formed in till 20 to 36 inches thick and material weathered from the underlying fractured, fine grained sandstone or siltstone. Depth to bedrock (lithic contact) ranges from 40 to 72 inches. These soils are found on upland interfluves, head slopes, nose slopes and side slopes. Slopes range from 2 to 15 percent. Rounded rock fragments of mixed lithology are 0 to 10 percent in the Ap, A, and E horizons and 1 to 20 percent in Bt and BC horizons; thin flat fragments of siltstone or fine grained sandstone are 15 to 50 percent in 2Bt and 2BC horizons and 60 to 90 percent in the 2C horizon. These soils have moderate permeability in the till-derived material and moderately rapid permeability in the underlying residuum, above bedrock.

They are not classified as hydric.

Mentor silt loam (MeB)
The Mentor series consists of very deep, well drained soils formed in stratified glaciolacustrine or terrace deposits derived from materials high in sandstone and shale. Depth to bedrock is greater than 60 inches. These soils are found on treads and risers on terraces, lake plains, and outwash plains. Slopes range from 1 to 6 percent. Rock fragments range from 0 to 2 percent in the solum and 0 to 10 percent in the C horizon below a depth of 50 inches. Rock fragments in the gravelly substratum phase range from 5 to 35 percent in the lower part of the solum and from 15 to 35 percent in the substratum. The depth to an intermittent apparent water table is 3.5 to 6 feet between February and March in most years. The gravelly substratum phase does not have a water table within 6 feet. These soils are not classified as hydric.

Mermill loam (Mf, Mo)
The Mermill series consists of very deep, very poorly drained soils that formed in loamy glaciolacustrine deposits and the underlying till. Depth to bedrock is greater than 80 inches. Depth to till is 20 to 40 inches. Slopes range from 0 to 1 percent. These soils are found on lake plains and till plains. Rock fragments consist of glacial pebbles, primarily of limestone, dolostone, and crystalline lithology. Permeability is moderate in the loamy material and slow or very slow in the underlying till. The depth to the top of an intermittent perched high water table ranges from 1 foot above to 1 foot below the surface between December and May in normal years. Brief ponding occurs at a depth of 1 foot. These soils are classified as hydric.

Mermill silty clay loam (MeA)
The Mermill silty clay loam series consists of very deep, very poorly drained soils that formed in loamy glaciolacustrine or water-sorted material 20 to 40 inches thick and in the underlying till. Depth to bedrock is greater than 80 inches. Depth to unweathered till or lacustrine deposits is 24 to 48 inches. These soils are found in extensive flat areas, depressions and drainageways on ground moraines and lake plains. Slopes range from 0 to 1 percent. Permeability is moderate in the loamy material and slow or very slow in

the underlying till. The depth to the top of an intermittent perched high water table ranges from 1 foot above to 1 foot below the surface. Soils are subject to brief ponding. These are classified as hydric.

(Source: Soil Survey of Erie County, OH, 2006)

Mermill-Aurand complex (MfA)
The Mermill-Aurand complex consists of very deep soils that formed in loamy glaciolacustrine deposits and the underlying till. Depth to bedrock is greater than 80 inches. Slopes range from 0 to 1 percent. Mermill soils are found on depressions, drainageways and extensive flats on lake plains. Aurand soils are found on rises and knolls on lake plains. In Mermill soils, the depth to the perched seasonal high water table is between the surface and 1 foot below the surface and brief ponding takes place at a depth of 1 foot. In Aurand soils, the depth to the perched seasonal high water table is between 0.5 feet and 1.5 feet below the surface. Aurand soils are not subject to ponding. Mermill soils are classified as hydric, and Aurand soils are not classified as hydric.

Metamora sandy loam (MmA)
The Metamora series consists of very deep, somewhat poorly drained soils formed in loamy glaciofluvial or lacustrine deposits and the underlying loamy till on lake plains. Depth to bedrock is greater than 60 inches. These soils are found on lake plains, nearshore zones (relict), till plains and low moraines. Slopes range from 0 to 3 percent. Rock fragment content ranges from 0 to 10 percent gravel throughout and 0 to 3 percent cobbles in the 2Bt and 2C horizons. The depth to the top of an apparent seasonal high water table ranges from 6 to 18 inches between March and May and in October and November in normal years. These soils are not classified as hydric.

Milford silty clay loam (MfA)
The Milford series consists of very deep, poorly drained and very poorly drained soils formed in lacustrine sediments. The depth to bedrock is greater than 60 inches. These soils are found on low broad summits or in depressions on glacial lake plains. Slopes range from 0 to 1 percent. Rock fragment content of the series control section is 0 to 5 percent. Average clay content of the particle-size control section is 35 to 42 percent. The apparent seasonal high water table is 0.5 foot above to 1 foot below the surface at some time during the spring in most years. These soils are classified as hydric.

Millgrove loam (Mo, MgA)
The Millgrove series consists of very deep, very poorly drained soils that formed in loamy and gravelly outwash overlying sandy, gravelly and loamy outwash deposits. Depth to bedrock ranges from 60 to 80 inches. A till substratum phase is recognized that has till below 60 inches. These soils are found on outwash plains and terraces. Slopes range from 0 to 1 percent. Rock fragments consist mainly of glacial pebbles of mixed lithology. The depth to the top of an intermittent apparent high water table ranges from 1 foot above to 1 foot below the surface between November and May in normal years. The soils are subject to rare flooding and are classified as hydric.

Millsdale silty clay loam (Ms, MhA, MmA)
The Millsdale series consists of moderately deep, very poorly drained soils formed in till overlying limestone or dolostone. Depth to bedrock (lithic contact) ranges from 20 to 40 inches. These soils are located on till plains, lake plains and terraces. Slopes range from 0 to 1 percent. The depth to the top of an intermittent apparent high water table ranges from 1 foot above to 1 foot below the surface between November and May in normal years. These soils are classified as hydric.

Milton silt loam (MnA, MnB)
The Milton series consists of moderately deep, well drained soils formed in the loess and the underlying till and residuum from limestone or dolomite. The depth to bedrock (lithic contact) ranges between 40 and 60 inches. These soils are found on till plains. Slopes range from 0 to 6 percent. In Milton silt loam, the depth to the seasonal high water table is greater than 6 feet. These soils are not classified as hydric.

<u>*Miner silt loam, bedrock substratum (MsA)*</u>
The Miner series consists of very deep, very poorly drained soils formed in low-lime till principally derived from acid shale. The depth to bedrock is greater than 60 inches. A shale substratum phase occurs in some places at depth of 40 to 60 inches. Slopes range from 0 to 1 percent. These soils are found in shallow depression and narrow drainageways on lake plains and till plains. Rock fragments are mainly shale with some sandstone, limestone, and crystalline rocks. Clay content averages 35 to 45 percent in the particle-size control section. Depth to the top of a perched and/or apparent seasonal high water table ranges from 1 foot above the surface to 1.0 below the surface from October to May in most years.

Frequent long duration ponding occurs during extended wet periods. These soils are classified as hydric.

<u>*Miner silty clay loam (Mr, MrA)*</u>
The Miner series consists of very deep, very poorly drained soils formed in low-lime till principally derived from acid shale. The depth to bedrock is greater than 60 inches. A shale substratum phase occurs in some places at depth of 40 to 60 inches. Slopes range from 0 to 1 percent. These soils are found in shallow depression and narrow drainageways on lake plains and till plains. Rock fragments are mainly shale with some sandstone, limestone, and crystalline rocks. Clay content averages 35 to 45 percent in the particle-size control section. Depth to the top of a perched and/or apparent seasonal high water table ranges from 1 foot above the surface to 1 foot below the surface from October to May in most years.

Frequent long duration ponding occurs during extended wet periods. These soils are classified as hydric.

<u>*Mitiwanga silt loam (MxA, MtB)*</u>
The Mitiwanga series consists of moderately deep, somewhat poorly drained soils formed in 20 to 40 inches of till underlain by bedrock. The depth to bedrock (lithic contact) ranges from 20 from 40 inches. In some pedons, a few inches of fractured sandstone are above lithic contact. These soils are found on till plains and lake plains. Slopes range from 0 to 6 percent. Depth to an intermittent apparent seasonal high water table is 0.5 to 1 feet below the surface from November to June in most years. These soils are not classified as hydric.

<u>*Nappanee loam (NnA, NnB)*</u>
The Nappanee series consists of very deep, somewhat poorly drained soils that are moderately deep or deep to dense till that formed in clayey till. The depth to bedrock is greater than 60 inches. These soils are found on wave-worked till plains, till-floored lake plains, till plains and moraines. Slopes range from 0 to 6 percent. Rock fragments consist of glacial erratics of mixed lithology, primarily shale, limestone, and igneous gravel. The depth to the top of an intermittent perched high water table ranges from 0.5 to 2 feet between November and May in normal years. These soils are not classified as hydric.

<u>*Nappanee sandy loam (NmA)*</u>
The Nappanee sandy loam series consists of very deep, somewhat poorly drained soils that are moderately deep or deep to dense till that formed in wave-planed till. The depth to bedrock is greater than 60 inches. These soils are found on wave-worked till plains, till-floored lake plains, till plains and moraines. Slopes range from 0 to 2 percent. The depth to the top of a perched seasonal high water table ranges from 0.5 to 1 feet between November and May in normal years. These soils are not classified as hydric.

<u>*Nappanee silt loam (NpA)*</u>
The Nappanee silt loam series consists of deep, somewhat poorly drained soils that are moderately deep or deep to dense till that formed in clayey till. The depth to bedrock is greater than 60 inches. These soils are found on slight rises and low slope breaks along drainageways. Slopes range from 0 to 3 percent. The depth to the top of a perched seasonal high water table ranges from 1 to 2 feet during extended wet periods. These soils are not classified as hydric.

Nappanee silty clay loam (NpA, NpB, NpB2)
The Nappanee series consists of very deep, somewhat poorly drained soils that are moderately deep or deep to dense till that formed in clayey till. The depth to bedrock is greater than 60 inches. These soils are found on wave-worked till plains, till-floored lake plains, till plains and moraines. Slopes range from 0 to 6 percent. In Nappanee silty clay loam, the depth to the top of the perched seasonal high water table ranges from 0.5 to 1 feet between November and May in normal years. These soils are not classified as hydric.

Nolin silt loam (NoA)
The Nolin series consists of very deep, well drained soils formed in alluvium derived from limestones, sandstones, siltstones, shales, and loess. Depth to bedrock is greater than 60 inches. These soils are found on nearly level flood plains, in depressions which receive runoff from surrounding slopes, or on natural levees or major streams and rivers. Slopes are typically 0 to 2 percent. Coarse fragments, mostly rounded pebbles, ranges from none to about 5 percent in the A and Bw horizon and from 0 to 35 percent in the C horizon. Redoximorphic features, if present, are below 72 inches. The soil is subject to rare to frequent flooding or ponding in depressions for variable duration. These soils are not classified as hydric.

Oakville fine sand (OaB, OaC)
The Oakville fine sand series consists of very deep, well drained soils formed in sandy eolian deposits. Depth to bedrock is greater than 80 inches. These soils occur on the side slopes of long, narrow beach ridges and sand dunes on outwash plains, lake plains and moraines. Slopes range from 0 to 12 percent. The depth to an apparent seasonal high water table is more than 6 feet. These soils are not classified as hydric.

Ogontz fine sandy loam (OgA)
The Ogontz fine sandy loam series consist of very deep, moderately well drained soils formed in calcareous, stratified loamy and silty glaciolacustrine deposits. Depth to bedrock is greater than 80 inches. These soils are found on slightly dissected lake plains and deltas of Wisconsinan age. Slopes range from 0 to 2 percent. The depth to the top of an intermittent apparent high water table ranges from 1.5 to 3 feet between November and May in normal years. These soils are not classified as hydric.

Ogontz silt loam (OhB)
The Ogontz silt loam series consist of very deep, moderately well drained soils formed in calcareous, stratified loamy and silty glaciolacustrine deposits. Depth to bedrock is greater than 80 inches. These soils are found on slightly dissected lake plains and deltas of Wisconsinan age. Slopes range from 2 to 6 percent. The depth to the top of an intermittent apparent high water table ranges from 1.5 to 3 feet between November and May in normal years. These soils are not classified as hydric.

Olmsted loam (Od)
The Olmsted loam series consists of very deep, poorly drained soils that formed in loamy fluvial sediments from sandstone, shale and siltstone. The depth to bedrock is greater than 60 inches. These level to nearly level soils are found in slight depressions and on outwash terraces. In some areas, the surface layer is either silt loam or light silty clay loam. Some areas have glacial till at depths as shallow as 5 feet. These soils are classified as hydric.

Orrville silt loam (Or, OrA, OpA)
The Orrville series consists of very deep, somewhat poorly drained soils formed in alluvium from upland areas of low-lime drift, and from areas of sandstone, siltstone, shale, and limestone. Depth to bedrock is greater than 60 inches. These soils are found on floodplains and floodplain steps.

Slopes range from 0 to 2 percent. Average clay content ranges from 18 to 30 percent and average sand content coarser than very fine sand ranges from 15 to 40 percent in the particle-size control section. The depth to the top of an intermittent apparent seasonal high water table ranges from 0.5 to 1.0 foot from

November to May in normal years. Orrville soils are subject to occasional or frequent flooding. These soils are not classified as hydric.

Oshtemo loamy sand (OsB)
The Oshtemo series consists of deep, well drained, nearly level to sloping soils that formed in stratified loamy and sandy deposits of Wisconsin age that have a high content of quartz and contain variable amounts of material derived from igneous and metamorphic rocks, sandstone, limestone and dolomite. The depth to bedrock is greater than 80 inches. These soils are found on outwash plains, valley trains, moraines and beach ridges. Oshtemo loamy sands range in slope from 0 to 6 percent. In some areas, the loamy sand contains bands of irregularly shaped bodies of sandy loam or loam. In some areas, these soils are gravelly throughout the profile, but in others, they are gravel free. Permeability is moderately rapid in the upper loamy materials and very rapid in the lower sandy materials. These soils are not classified as hydric.

Oshtemo sandy loam (OtB, OsB, OsC)
The Oshtemo series consists of deep, well drained, nearly level to sloping soils that formed in stratified loamy and sandy deposits of Wisconsin age that have a high content of quartz and contain variable amounts of material derived from igneous and metamorphic rocks, sandstone, limestone and dolomite. The depth to bedrock is greater than 80 inches. These soils are found on outwash plains, valley trains, moraines and beach ridges. Oshtemo sandy loams range in slope from 2 to 12 percent. Permeability is moderately rapid in the upper loamy materials and very rapid in the lower sandy materials. These soils are not classified as hydric.

Ottokee fine sand (OtB, OuB)
The Ottokee series consists of very deep, moderately well drained soils formed in sandy glaciolacustrine, eolian, or water-sorted deposits. The depth to bedrock is greater than 80 inches. These soils are found on beach ridges and dunes on lake plains and on outwash plains. Slopes range from 0 to 6 percent. The dominant sand size is fine with significant amounts of very fine sand. Clay content ranges from 27 to 42 percent. Rock fragment content ranges from 2 to 10 percent. An apparent high water table is 2 to 3.5 feet below the surface from January to April in normal years. These soils are not classified as hydric.

Pewamo silty clay loam (PcA)
The Pewamo series consists of very deep, very poorly drained soils formed in till. The depth to bedrock is greater than 60 inches. These soils are found on moraines, near-shore zones (relict), and lake plains. Slopes range from 0 to 1 percent. Depth to an apparent seasonal high water table ranges from 1 foot above the surface to 1 foot below the surface from December to May in normal years. These soils are classified as hydric.

Plumbrook fine sandy loam (PmA)
The Plumbrook series consists of very deep, somewhat poorly drained soils formed in loamy and sandy sediments overlying silty lacustrine sediments. The depth to bedrock is greater than 80 inches. These soils are found on lake plains of Wisconsinan age. Slopes range from 0 to 2 percent. Depth to silty lacustrine sediments is 60 to 80 inches. Rock fragments consists of glacial erratics of sedimentary and crystalline lithology. The depth to the top of an intermittent perched high water table ranges from 1 to 2.5 feet between December and May in normal years. These soils are not classified as hydric.

Randolph loam (RbA)
The Randolph series consists of moderately deep, somewhat poorly drained soils formed in till overlying residuum from limestone or dolostone. They are found on till plains. The depth to lithic contact ranges from 20 to 40 inches. Slopes range from 0 to 2 percent. The depth to the top of an intermittently apparent high water table ranges from 0.5 to 1 foot between January and April in normal years. These are not classified as hydric soils.

Randolph silt loam (RaA)

The Randolph series consists of moderately deep, somewhat poorly drained soils formed in till overlying residuum from limestone or dolostone. They are found on flat areas and slight rises on lake plains. The depth to lithic contact ranges from 20 to 40 inches. Slopes range from 0 to 2 percent. The depth to the top of an intermittently apparent high water table ranges from 1 to 2.5 feet between January and April in normal years. These are not classified as hydric soils.

Ravenna silt loam (ReA, ReB)

The Ravenna series consists of very deep, somewhat poorly drained soils formed in Wisconsinan age till. Some pedons have a thin mantle of loess or other silty material. The depth to bedrock is greater than 80 inches. Ravenna soils are found on till plains, on broad, nearly level to gently sloping base slopes and interfluves. Slopes range from 0 to 6 percent. Rock content fragments range from 0 to 6 percent by volume above the fragipan, and 2 to 25 percent in the fragipan and below it. They are dominantly sandstone but include shale and some crystalline rocks. Depth to the top of the fragipan ranges from 14 to 30 inches, but is typically deeper than 20 inches. In undisturbed soils, the depth to the top of a perched seasonal high water table is 7 to 11 inches during October to June in normal years. These soils are not classified as hydric.

Rawson loam (RdA, RdB)

The Rawson series consists of very deep, moderately well drained soils that are moderately deep or deep to dense till. The depth to bedrock is greater than 60 inches. Rawson soils formed in loamy sediments and till and are found on till plains, outwash plains, and lake plains. Slopes range from 0 to 6 percent. Depth to the top of an intermittent perched high water table ranges from 2.0 to 3.5 feet between January and April in normal years. Nearly all areas of these soils are cultivated. These soils are not classified as hydric.

Rawson sandy loam (RcA, RcB)

The Rawson sandy loam series consists of very deep, moderately well drained soils that are moderately deep or deep to dense till. The depth to bedrock is greater than 60 inches. Rawson soils formed in loamy sediments and till and are found on till plains, outwash plains, and lake plains. Slopes range from 0 to 6 percent. Depth to unweathered till or lacustrine deposits ranges from 25 to 51 inches. Depth to the top of an intermittent perched high water table ranges from 2.0 to 3.5 feet between January and April in normal years. These soils are not classified as hydric.

Rimer loamy fine sand (RgA, RnA, RoB)

The Rimer series consists of very deep, somewhat poorly drained soils that are deep or moderately deep to dense till. These soils formed in glaciolacustrine deposits in the underlying till. The depth to bedrock is greater than 80 inches. These soils are found on convex surfaces of lake plains, wave-worked till plains, till-floored lake plains, and till plains. Slopes range from 0 to 4 percent. The depth to the top of an intermittent perched high water table ranges from 0.5 to 1.5 feet between January and April in normal years. These soils are not classified as hydric.

Ritchey loam (RhA, RhB, RhC)

The Ritchey loam series consists of shallow, well drained soils formed in till over limestone or dolostone bedrock. The depth to the base of soil development and depth to lithic contact ranges from 10 to 20 inches. Ritchey loam is found on till plains of Wisconsinan age Slopes range from 0 to 12 percent. Rock fragments are primarily glacial erratics of sedimentary and crystalline lithology. A stony surface phase is recognized. These soils are not classified as hydric.

Rittman silt loam (RsD2, RsE2, RsB, RsB2, RsF, RsC, RsC2)

The Rittman series consist of very deep, moderately well drained soils formed in Wisconsinan age low lime till. The depth to bedrock ranges from 40 to 60 inches. Rittman soils are found on till plains. A large proportion of Rittman soils is either cultivated or in pasture. Slopes range from 2 to 70 percent. Depth to fragipan ranges from 18 to 36 inches. Rock fragments range from 0 to 10 percent above the fragipan and from 2 to 15 percent in the fragipan and substratum. In undisturbed areas the top of an intermittent perched seasonal high water table ranges from 10 to 27 inches from November to April in normal years. These soils are not classified as hydric.

Rossburg silt loam, occasionally flooded (Rs)
The Rossburg series consists of very deep, well drained soils formed in loamy alluvium derived from Wisconsinan age drift. The depth to bedrock is greater than 60 inches. These soils are found on floodplains. Slopes range from 0 to 3 percent. Rock fragments consist of glacial erratics of mixed lithology. The depth to the top of an intermittently high water table is greater than 6 feet. These soils are subject to seasonal flooding. These soils are not classified as hydric.

Saylesville silt loam (SbF)
The Saylesville silt loam series consists of very deep, steeply sloping, well drained soils formed in silty clay loam lacustrine deposits with a thin silty or loamy mantle. The depth to bedrock is greater than 60 inches. These soils are found on the backslopes of dissected areas on lake plains. Slopes range from 25 to 40 percent. Most pedons do not have rock fragments, but some pedons have as much as 5 percent gravel in the upper part of the solum. A seasonal high water table is at a depth of 3 to 6 feet. These soils are not classified as hydric.

Saylesville silty clay loam (SbC2)
The Saylesville silty clay loam series consists of deep, sloping, moderately well drained soils formed in silty clay loam lacustrine deposits with a thin silty or loamy mantle. The depth to bedrock is greater than 60 inches. These soils are found on slope breaks along drainageways on lake plains. Slopes range from 6 to 12 percent. A seasonal high water table is at a depth of 36 to 72 inches during extended wet periods. These soils are not classified as hydric.

Sebring silt loam (Sb, Sg, Se, St)
The Sebring series consists of very deep, poorly drained soils formed in stratified Wisconsinan age glaciolacustrine sediments. The depth to bedrock is greater than 60 inches. These soils are found on broad flats and depressions on lake plains and slackwater terraces. Slopes range from 0 to 2 percent. Frequent ponding occurs during periods of heavy rainfall and during spring snowmelt. Depth to the top of an intermittent apparent seasonal high water table ranges from greater than to less than 0.5 feet from the surface. These soils are not classified as hydric.

Seward and Ottokee, till substratum, loamy fine sands (SdA)
The Seward and Ottokee series consists of very deep, moderately well drained soils formed in sandy glaciolacustrine deposits and the underlying till. The depth to bedrock is greater than 80 inches. These soils are found on the summits, shoulders, and backslopes of knolls on lake plains, dunes, and beach ridges on lake plains. Slope ranges from 0 to 2 percent. The series has a perched water table located between 1.5 and 3 feet and is not typically subject to flooding or ponding. These soils are not classified as hydric.

Seward loamy fine sand (SdB)
The Seward loamy fine sand series consists of very deep, moderately well drained soils that formed in 25 to 40 inches of sandy glaciolacustrine sediments or eolian material and the underlying till. The depth to bedrock is greater than 80 inches. Depth to till ranges from 25 to 40 inches. Seward loamy fine sand soils are found on ridges and knolls of outwash plains, on beach ridges, and on deltas. Slopes range from 2 to 6 percent. These soils are not classified as hydric.

Shinrock silt loam (ShB)
The Shinrock silt loam series consists of very deep, moderately well drained soils formed in silty and clayey glaciolacustrine sediments. The depth to bedrock is greater than 60 inches. These soils are found

on knolls, summits, backslopes and shoulders of the lake plains of late Wisconsinan age that have been dissected by modern stream valleys. Slopes range from 2 to 6 percent. Rock fragments are typically absent. Depth to an intermittently perched water table is 1.5 to 3 feet. This soil is not classified as hydric.

Shinrock silty clay loam (SkD2, SkC2)
The Shinrock silty clay loam series consists of very deep, moderately well drained soils formed in silty and clayey glaciolacustrine sediments. The depth to bedrock is greater than 60 inches. These soils are found on the backslopes and shoulders of dissected areas on lake plains of late Wisconsinan age. Slope range from 6 to 18 percent. Rock fragments are typically absent. Depth to an intermittently perched water table is 1.5 to 3 feet. This soil is not classified as hydric.

Shoals loam (Sh)
The Shoals loam series consists of very deep, somewhat poorly drained soils that formed in loamy alluvium on floodplains. The depth to bedrock is greater than 60 inches. Shoals loam soils are found on flats and rises on floodplains and subject to occasional and frequent flooding. Slopes range from 0 to 2 percent. These soils are not classified as hydric.

Shoals silt loam (Sh)
The Shoals silt loam series consists of very deep, somewhat poorly drained soils that formed in loamy alluvium on floodplains. The depth to bedrock is greater than 60 inches. Shoals silt loam soils are found on flats and rises on floodplains and subject to frequent flooding. Slopes range from 0 to 2 percent. These soils are not classified as hydric.

Sission loam (SmC)
The Sission series consists of deep, well drained soils that formed in stratified loamy and silty material. The depth to bedrock is greater than 60 inches. The potential for surface runoff ranges from negligible to high depending on the slope gradient. Permeability is moderate. These soils are found mainly on deltas in areas of former lake plains. Slopes range from 6 to 12 percent. These are not classified as hydric.

Sloan loam (So)
The Sloan series consists of very deep and very poorly drained soils formed in loamy alluvium washed mainly from soils formed in loamy calcareous drift. The depth to bedrock is greater than 60 inches. These are found on floodplains or in depressions along streams receiving sediment from areas of Wisconsinan age glaciation. Slopes range from 0 to 2 percent. Depth to the top of an intermittent apparent high water table ranges from 1 foot above the surface to 1 foot below the surface between November and June in normal years. These soils are subject to flooding from late fall to spring and are classified as hydric.

Sloan silt loam (Sl, So, SnA)
Sloan silt loam shares characteristics of the Sloan series. Soils are very deep and very poorly drained and formed in loamy alluvium washed mainly from soils formed in loamy calcareous drift. The depth to bedrock is greater than 60 inches. Sloan silt loam is found in backswamps and flats on floodplains. Slopes range from 0 to 1 percent. The seasonal high water table is at the surface or one foot below the surface. Soils are subject to flooding and brief ponding to depths of one foot. These soils are classified as hydric.

Sloan silty clay loam (SpA, So)
Sloan silty clay loam shares characteristics of the Sloan series. Soils are very deep and very poorly drained and formed in loamy alluvium washed mainly from soils formed in loamy calcareous drift. The depth to bedrock is greater than 60 inches. Sloan silty clay loam is found on flats and backswamps and on floodplains. Slopes range from 0 to 1 percent. The seasonal high water table is at the surface or one foot below the surface. Soils are subject to frequent flooding and brief ponding to depths of one foot. These soils are classified as hydric.

<u>*Spinks fine sand (SoB)*</u>
The Spinks series consists of very deep, well drained soils formed in sandy eolian or outwash material. The depth to bedrock is greater than 100 inches. Spinks soils are found on dunes, moraines, till plains, outwash plains, beach ridges and lake plains. Slopes ranges from 2 to 6 percent. Rock fragment content consists of glacial erratics (dominantly gravel) of sedimentary and crystalline lithology. These soils are not classified as hydric.

<u>*Spinks loamy fine sand (SpB)*</u>
The Spinks series consists of very deep, well drained soils formed in sandy eolian or outwash material. The depth to bedrock is greater than 100 inches. Spinks soils are found on dunes, moraines, till plains, outwash plains, beach ridges and lake plains. Slopes ranges from 0 to 6 percent. Rock fragment content consists of glacial erratics (dominantly gravel) of sedimentary and crystalline lithology. These soils are not classified as hydric.

<u>*St. Clair loam (StC2)*</u>
The St. Clair loam series consists of very deep, moderately well drained soils formed in drift. The depth to bedrock is greater than 48 inches and typically greater than 60 inches. St-Clair loam soils are found on the summits, shoulders, and backslopes of rises, knolls and dissected areas along streams and on lake plains. Slopes range from 6 to 12 percent. These soils are not classified as hydric.

<u>*St. Clair silty clay loam (SuD2, SuE3, SuE2, SuC2)*</u>
The St. Clair silty clay loam series consists of very deep, moderately well drained soils formed in drift. The depth to bedrock is greater than 48 inches and typically greater than 60 inches. St-Clair silty clam loam soils are found on the summits, shoulders, and backslopes of rises, knolls and dissected areas along streams and on lake plains. Slopes range from 4 to 25 percent, with some areas eroded and severely eroded. These soils are not classified as hydric.

<u>*Tedrow fine sand (TdA)*</u>
Tedrow fine sand soils are deep and somewhat poorly drained soils that formed in sandy material on glacial beach ridges and dunes. The depth to bedrock is greater than 60 inches. These soils are found in long narrow areas on low beach ridges and in oval areas on dunes. Slopes range from 0 to 3 percent. Permeability is rapid. The water table is near the surface during extended wet periods. These soils are not classified as hydric.

<u>*Tedrow loamy fine sand (TdA)*</u>
Tedrow loamy fine sand soils are deep and somewhat poorly drained soils that formed in sandy material on glacial beach ridges and dunes. The depth to bedrock is greater than 60 inches. These soils are found on low beach ridges and sand dunes as long and narrow or circular areas. Slopes range from 0 to 3 percent. Permeability is rapid. These soils are not classified as hydric.

<u>*Teegarden silt loam (TeC, TeC2)*</u>
The Teegarden series consists of very deep, moderately well drained soils formed in loess, Illinoian or early Wisconsinan age till, and material weathered from the underlying Pennsylvanian age shale, fine-grained sandstone, or siltstone. The depth to bedrock is greater than 60 inches. The depth to the top of the fragipan ranges from 18 to 30 inches. Teegarden soils are located on till plains. Slopes range from 6 to 15 percent. Permeability is moderate above the fragipan, slow in the fragipan and moderate to slow below the fragipan, above bedrock. Rock fragments are dominantly sandstone, but include shale, siltstone, and some crystalline rocks. These soils are not classified as hydric.

<u>*Tioga fine sandy loam (Tg)*</u>
The Tioga fine sandy loam consists of well-drained, nearly level soils formed in moderately coarse textured to coarse textured alluvium. The depth to bedrock is greater than 50 inches. These soils are found in floodplains. Rock fragments range from 0 to 35 percent by volume in individual layers in the solum

and consist of pebbles or channers, and range from 0 to 60 percent by volume in individual layers in the substratum and consist of mostly pebbles and channers. These soils are not classified as hydric.

Toledo silty clay (To)
The Toledo silty clay series consists of deep, very poorly drained soils formed in clayey glaciolacustrine sediments. The depth to bedrock is greater than 80 inches. These soils are found on the lake plains of Wisconsinan age, specifically on broad flats and in long, narrow concave areas on lake plains. Slopes range from 0 to 2 percent. Rock fragments are typically absent. The depth to the top of an intermittent apparent high water table ranges from 1 foot above the surface to 1 foot below between November and May in normal years. The ponded phase has an apparent high water table ranging from 3 feet above the surface to 1 foot below between September and May in normal years. These soils are classified as hydric.

Toledo silty clay loam (Tp)
The Toledo silty clay loam (ponded) series consists of deep, very poorly drained soils formed in clayey glaciolacustrine sediments. The depth to bedrock is greater than 80 inches. This series is found on the lake plains of Wisconsinan age, specifically in long, narrow concave areas along drainageways and on broad flats on lake plains. Slopes range from 0 to 2 percent and the area remains ponded for long periods with a seasonal high water table near or above the surface most of the year. These soils are classified as hydric.

Trumbull silty clay loam (TrA)
The Trumbull silty clay loam series consists of very deep, poorly drained soils formed in low-lime glacial till. Trumbull soils are found on level to gently sloping depressional portions of till plains including drainageways. The depth to bedrock is greater than 60 inches. Slopes range from 0 to 2 percent. Rock fragments are dominantly gravel but cobbles and range from 2 to 10 percent in the lower part of the subsoil and in the substratum. These soils are classified as hydric.

Tuscola fine sandy loam (TuA, TuB)
The Tuscola series consists of very deep and moderately well drained soils formed in stratified loamy and silty lacustrine deposits. Depth to bedrock is greater than 80 inches. These soils are found on lake plains and deltas of Wisconsin age. Slopes range from 0 to 6 percent. These soils are not classified as hydric.

Udipsamments-Spinks complex (UcB)
The Udipsamments-Spinks complex consists of very deep, well drained soils. Spinks soils are formed in Eolian or beach deposits; Udipsamments soil parent material is not provided in the county soil survey. Depth to bedrock is greater than 80 inches. The Udipsamments-Spinks complex is found on beach ridges on lake plains and dunes on lake plains. Udipsamments soils are concentrated in the flat areas and rises and Spinks soils are concentrated on the backslopes and shoulders. These areas are altered when mined for sand. Slopes range from 0 to 6 percent. These soils are not classified as hydric.

Udorthents (Ua)
These deep nearly level soils are in areas where the landscape has been extensively altered by construction activities. Some areas have been used as a source of borrow materials while others have been used as sites for landfills. The soils in these areas are comprised of a mixture of materials from the subsoil and substratum of the natural soils. In some places much of the surface layer, subsoil, or substratum has been removed. The mixture of the soil materials varies so considerably that it cannot be classified at the series level.

Udorthents loam (Ud, UdB)
The Udorthents loam series consists of soils in areas that have been cut and filled. These are found mostly in construction areas and small pits from which material other than gravel or bedrock have been removed. Slopes range from 0 to 6 percent. In areas where soil has been removed, the remaining material is typically similar to the subsoil or substratum of adjacent soils. In fill or disposal areas, the soil material is

more varied although the soil material generally originates from the subsoil and substratum of nearby soils.

Udorthents, refuse substratum (Ub)
The Udorthents series consists of soils in areas that have been cut and filled. The Udorthents refuse substratum series consists of very deep, excessively drained to moderately well drained soils used as sites for sanitary landfills. The soils have been cut, filled and graded. About 2 feet of soil material is used to cap compacted refuse and other buried debris. Due to extensive mixing of the unconsolidated soil material, soil texture can be highly variable and soil profile development is absent or weak. These soils are found in till plains, terraces and hills. Slopes range from 2 to 25 percent. Depth to bedrock is greater than 80 inches. These soils are unranked for hydric classification.

Udorthents, sanitary landfill (Uf) no slope designation
These are areas that have been built up from deposits of compacted solid refuse deposited in layers and then covered by soil throughout the disposal period. In some instances this has been done to create more usable land.

Wadsworth silt loam (WaA, WaB, WaC, WaC2)
The Wadsworth series consists of very deep, somewhat poorly drained soils formed in Wisconsinan age till that was strongly influenced by sandstone and clay shale. Some pedons have a thin mantle of loess or other silty material. The depth to bedrock is typically greater than 60 inches and depth to fragipan ranges from 18 to 30 inches. Wadsworth soils are found on interfluves, side slopes and base slopes on till plains. Slopes range from 0 to 12 percent. Rock fragment content ranges from 0 to 4 percent in the A, BE, and Bt horizons and from 2 to 15 percent in the Btx, BC, and C horizons. These soils are not classified as hydric.

Wakeman sandy loam (WaB, WaC)
The Wakeman series consists of moderately deep and well drained soils formed in sandy and loamy residuum over sandstone bedrock. The depth to bedrock ranges from 20 to 40 inches. Wakeman soils are found on bedrock controlled landforms on till plans and lake plains. Slopes range from 2 to 12 percent. Permeability is moderately rapid. These soils are not classified as hydric.

Wallkill silt loam (Wc)
The Wallkill series consists of very deep and very poorly drained soils formed in alluvial mineral soil deposits over organic soil materials. The depth to bedrock is greater than 59 inches. Wallkill soils are found along streams that run through organic soil areas and along the margins of depressional areas adjacent to upland mineral soils. Slopes range from 0 to 3 percent. Rock fragments are typically absent but some pedons contain up to 20 percent gravel in the mineral horizons. These soils are classified as hydric.

Weinbach silt loam (WhA, WhB)
The Weinbach series consists of deep, somewhat poorly drained, very slowly permeable soils formed in old acid alluvium and stratified silt loam, silty clay loam and loam with some sand in the underlying materials. The depth to bedrock is typically greater than 60 inches. The depth to fragipan ranges from 20 to 36 inches. Weinbach soils are found on nearly level to gently sloping terraces. Slopes range from 0 to 6 percent. These soils are not classified as hydric.

Wheeling silt loam (WrA, WrB, WrC)
The Wheeling series consists of very deep, well drained soils with moderate permeability. These soils formed in silty or loamy alluvial materials on river terraces. Depth to bedrock ranges from 40 to 60 inches or more. Slopes range from 0 to 12 percent. Typically, Wheeling soils are on nearly-level river terraces. The content of rock fragments in the solum ranges from 0 to 35 percent. The percent of clay averages between 18 and 30 in the particle size control section. In some areas there are noticeable mica flakes throughout the profile. These soils are not classified as hydric.

Wick silt loam (WoA)

The Wick series consists of very deep, very poorly drained soils formed in silty alluvium mostly derived from Wisconsin age till on floodplains. Depth to bedrock is greater than 80 inches. Wick series soils are found on floodplain steps and floodplains. Slopes range from 0 to 2 percent. Rock fragment content ranges from 0 to 2 percent in the A horizon, 0 to 5 percent in the B horizons and 0 to 15 percent in the C horizons. These soils are classified as hydric.

Willette muck (Wt)

The Willette series consists of black organic soils that are very poorly drained and formed in muck deposits 16 to 48 inches thick. A representative profile of Willette soils contains black muck to a depth of 30 inches with a dark gray silty clay loam between 30 and 36 inches. Slopes are nearly level. These soils are found in swampy depressions on terraces and in potholes on hummocky uplands. The Willette muck series is soft, compressible and unstable. It is swampy tending to catch surface waters draining from the adjacent higher elevations. These soils are classified as hydric.

Wooster silt loam (WuD,WuD2, WuE2, WuB, WuF2, WuF2, WuC, WuC2, WuD2)

The Wooster series consists of deep, well drained soils formed in low-lime loamy glacial till with a thin loess mantle in some places. The depth to the fragipan ranges from 18 to 40 inches. Wooster soils are found on till plains and moraines of Wisconsinan age. Slopes have a convex surface, and gradients range from 2 to 50 percent. Coarse fragments are dominantly sandstone, but include shale and a few crystalline rocks. They range from 2 to 20 percent by volume in horizons above the fragipan, 5 to 25 percent in the Btx, and 5 to 30 percent in the C horizon. These soils are not classified as hydric; permeability is moderate above the fragipan and moderately slow in the fragipan.

Wooster-Riddles silt loams (WuD2, WvB, WvC2, WuC2)

The Wooster-Riddles silt loam complex consists of deep, well-drained soils that formed mainly in glacial till but in some places, the till was covered by a thin mantle of loess. These soils are found on side slopes of ridgetops and along drainageways on uplands. Depth to bedrock is typically greater than 60 inches, but occasionally occurs at 40 to 60 inches. Slopes range from 6 to 12 percent. Permeability is moderately slow in the Wooster soil and moderate in the Riddle soil. These soils are not classified as hydric.

Zepernick silt loam (ZeA)

The Zepernick series consists of very deep, somewhat poorly drained soils formed in silty alluvium whose source was Wisconsinan age till, lacustrine sediments and outwash. Permeability of these soils is moderate to moderately slow and they are subject to occasional flooding. The depth to bedrock is greater than 60 inches. Zepernick soils are found on floodplain steps and floodplains. Slopes range from 0 to 2 percent. Rock content ranges from 0 to 2 percent in the A and B horizons and 0 to 45 percent in the C horizon. These soils are not classified as hydric.

Ziegenfuss clay loam (Zie5A)

The Ziegenfuss series consists of very deep, poorly drained soil found in clayey ablation till overlying dense basal till. Depth to bedrock is typically greater than 80 inches. Ziegenfuss soils are found on till plains, wave-worked till plains, till-floored lake plains, end moraines and ground moraines. Slopes range from 0 to 1 percent. Rock fragment content is 0 to 10 percent. These soils are classified as hydric.

Zurich silt loam (ZuC2, ZuD2, ZuE2, ZuF)

The Zurich series consists of very deep, moderately well-drained soils formed from lacustrine deposits.

The depth of bedrock is greater than 80 inches. These soils are found on the backslopes and shoulders of dissected areas on lake plains. Slopes range from 6 to 40 percent. These soils are not classified as hydric.

Soils Series in Michigan

Berrien sandy loam (BcA,)
The Berrien series consists of moderately well drained soils formed in sand or fine sand that was sorted by water and wind. Below the sand is calcareous glacial till or lake-laid sediments of loam to clay texture. Permeability is rapid in the upper part of the profile and slow to medium in the loamy and clayey material. These soils are not classified as hydric.

Blount loam (13A)
The Blount loam series consists of very deep, somewhat poorly drained soils that are formed in till and located on wave-worked till plains and near shore zones (relict). Slopes range from 0 to 6 percent. Permeability is slow in the solum and slow or very slow in the dense till. Depth to perched seasonal high water table is 0.5 to 2 feet. Potential for surface runoff is low to high. Drainage is the main management concern. This soil is not classified as hydric.

Boyer loamy sand (BnB)
The Boyer series soils consist of very deep, well drained soils that were formed in sandy and loamy drift underlain by sand or gravelly sand outwash at depths 20 to 40 inches. These soils are located on outwash plains, valley trains, kames, beach ridges, river terraces, lake terraces, deltas and morrains. Slopes range from 0 to 50 percent. Permeability is rapid in the solum and very rapid in the substratum. The seasonal high water table is greater than 6 feet. The potential for surface runoff is negligible to medium depending upon the slope. Droughtiness is the main limitation. These soils are not classified as hydric.

Brady and Macomb loams (BkA)
The Brady series consists of very deep, somewhat poorly drained soils formed in loamy outwash materials on outwash plains, valley trains, terraces, and lake plains. Slopes range from 0 to 3 percent. Depth to bedrock is greater than 80 inches. Depth to the seasonal high water table ranges from 0.5 to 1.5 feet from November to May. The potential for surface runoff is negligible to low. Permeability is moderately rapid. These soils are not classified as hydric.

The Macomb series consists of very deep, somewhat poorly drained soils formed in outwash and the underlying till on lake plains and till plains. Slopes range from 0 to 3 percent. Depth to bedrock is greater than 60 inches. Potential for surface runoff is very low to medium. Permeability id moderately slow. These soils are not classified as hydric.

Brady sandy loam (BhA)
The Brady series consists of very deep, somewhat poorly drained soils formed in loamy outwash materials on outwash plains, valley trains, terraces, and lake plains. Slopes range from 0 to 3 percent. Depth to bedrock is greater than 80 inches. Depth to the seasonal high water table ranges from 0.5 to 1.5 feet from November to May. The potential for surface runoff is negligible to low. Permeability is moderately rapid. These soils are not classified as hydric.

Cohoctah fine sandy loam, frequently flooded (Cc)
The Cohactah series consists of very deep, poorly drained soils formed in loamy alluvial deposits. The depth to bedrock is greater than 80 inches. Cohactah soils are found in abandoned drainage ways and depressions on floodplains. Slopes range from 0 to 2 percent. These soils are commonly flooded for brief to long periods of time from November to May. The depth to the top of an apparent seasonal high water table ranges from near the surface to 1 foot below the surface from September to May in normal years. These soils are classified as hydric.

Conover loam (CoB)
The Conover loam series consists of very deep and somewhat poorly drained soils formed in loamy till. The depth to bedrock is greater than 60 inches. These soils are found on low parts of moraines and till

plains. Slopes range from 0 to 4 percent. Rock fragment content ranges from 0 to 10 percent in the solum. These soils are not classified as hydric.

Corunna sandy loam (24)
The Corunna series consists of very deep, poorly-drained soils formed in loamy till and the underlying lacustrine deposits. The depth to bedrock is greater than 60 inches. Corunna soils are found on lake plains. Slopes range from 0 to 2 percent. These soils are classified as hydric.

Dixboro-Kibbie fine sandy loams (DoA)
The Dixboro-Kibbie fine sandy loam series is comprised of very deep and somewhat poorly drained soils that formed in stratified deposits of alternating layers of sandy and loamy textured sediments. Depth to bedrock is greater than 60 inches. These soils are found in low-lying areas and along drainageways of lake plains and outwash plains. Slopes range from 0 to 4 percent. Depth to the top of a seasonal high water table ranges from 1 to 2 feet between November and April in normal years. These soils are not classified as hydric.

Fox loam (FbA)
The Fox series consists of very deep, well drained soils formed in beach deposits. Slopes range from 2 to 6 percent. Depth to bedrock is greater than 80 inches. The seasonal high water table is more than 6 feet from the soil surface. Permeability is moderate in the subsoil and rapid or very rapid in the subsoil. These soils have a slight wind erosion hazard. These soils are not classified as hydric.

Fox sandy loam (FoA)
The Fox series consists of very deep, well drained soils formed in beach deposits. Slopes range from 2 to 6 percent. Depth to bedrock is greater than 80 inches. The seasonal high water table is more than 6 feet from the soil surface. Permeability is moderate in the subsoil and rapid or very rapid in the subsoil. These soils have a slight wind erosion hazard. These soils are not classified as hydric.

Genesee loam (GaA)
The Genesee series consists of very deep, well drained soils that formed in loamy alluvium flood plains. These soils are located on flats, rises, and natural levees on flood plains. Slopes range from 0 to 3 percent. Depth to bedrock is greater than 60 inches. Permeability is moderate in the solum and moderate or moderately rapid in the in the substratum. The potential for surface runoff is very low or low. The soils are subject to flooding at periodic intervals unless protected by a levee. The depth to seasonal high water table is greater than 2 feet. These soils have a slight wind erosion hazard. These soils are not classified as hydric.

Gilford sandy loam (GF)
The Gilford series consists of very deep, poorly drained and very poorly drained soils formed in loamy over sandy sediments on outwash plains, near-shore zones (relict), and flood-plain steps. These soils can be found on flat areas, depressions and drainageways. Slopes range from 0 to 1 percent. Depth to bedrock is greater than 80 inches. The seasonal high water table ranges from 0.5 foot above the surface to 1.0 foot below the surface. Permeability is rapid in the lower part of the subsoil and in the substratum. This soil experiences brief periods of ponding. These soils have a moderate wind erosion hazard. These soils are classified as hydric.

Hoytville and Wauseon loams (100A, HfA)
The Hoytville and Wauseon loam series consists of very deep, poorly drained or very poorly drained soils that are deep or very deep to dense till. These soils formed in till that has been leveled by wave action. Depth to dense till ranges from 50 to 70 inches. Depth to bedrock is greater than 80 inches. These soils are found on lake plains, and slopes range from 0 to 3 percent. A perched water table ranges from 1 foot above the surface to 1 foot below the surface from January to April in normal years. These soils are classified as hydric.

Kendallville loam (KeB)
The Kendallville series consists of very deep, well drained soils formed in as much as 18 inches of loess and the underlying outwash and loamy till. Depth to the underlying till is less than 40 inches. Depth to bedrock is greater than 60 inches. These soils are found on moraines, kames, eskers and outwash terraces. Slopes range from 2 to 6 percent. Rock fragments consists mainly of glacial pebbles (gravel) with some cobblestones and boulders, including some crystalline rocks. The depth to a seasonal high water table is greater than 6 feet. These soils are not classified as hydric.

Kibbie fine sandy loam (KnA)
The Kibbie series consists of very deep, somewhat poorly drained soils that formed in stratified loamy and silty glaciofluvial or glaciolacustrine deposits. The depth to bedrock is greater than 60 inches.

Silty clay loam and clay loam till is below 40 inches in some pedons. Sandy substratum phases that have sand or fine sand below 40 inches are present. These soils are found on lake plains, ground moraines, outwash plains, and deltas. Slopes range from 0 to 6 percent. Rock fragment content ranges from 0 to 1 percent. In Kibbie fine sandy loam, the depth to the seasonal high water table ranges from 0.5 to 1.5 feet below the surface from November to May in normal years. These soils are not classified as hydric.

Lenawee silty clay loam (Le)
The Lenawee series consists of very deep, poorly drained and very poorly drained soils formed in lacustrine deposits. Depth to bedrock is greater than 60 inches. These soils are found on lake plains and in depressional areas on moraines, outwash plains, and glacial drainageways. Slopes range from 0 to 2 percent. The seasonal high water table is near or above the surface during extended wet periods. This soil is classified as hydric.

Macomb fine sandy loam (MaA)
The Macomb fine sandy loam series consists of very deep, somewhat poorly drained soils formed in outwash and the underlying till. Depth to bedrock is greater than 60 inches. These soils are found along the western edge of the lake plain; along glacial drainageways; as small, shallow areas in outwash plains; or on the borders of lakes and swamps. Slopes range from 0 to 3 percent. In some places during wet periods, there is a seepage zone, or lateral-moving, suspended groundwater. These soils are not classified as hydric.

Macomb loam (MaA)
The Macomb loam series consists of very deep, somewhat poorly drained soils formed in outwash and the underlying till. Depth to bedrock is greater than 60 inches. These soils are found in broad, low-lying areas and along drainageways on lake plains and till plains Slopes range from 0 to 4 percent. These soils have a seasonal high water table and are subject to ponding in nearly level areas. These soils are not classified as hydric.

Metamora sandy loam (23A)
The Metamora series consists of very deep, somewhat poorly drained soils formed in loamy glaciofluvial or lacustrine deposits and the underlying loamy till on lake plains. Depth to bedrock is greater than 60 inches. These soils are found on lake plains, nearshore zones (relict), till plains and low moraines. Slopes range from 0 to 4 percent. The depth to the top of an apparent seasonal high water table ranges from 6 to 18 inches between March and May and in October and November in normal years. These soils are not classified as hydric.

Morley loam (MoB)
The Morley loam series consists of very deep, moderately well drained soils that are moderately deep to dense till and formed in as much as 18 inches of loess and in the underlying clay loam or silty clay loam till. Depth to bedrock is greater than 80 inches. These soils are found on till plains and moraines. Slopes

range from 2 to 6 percent. Depth to the top of an intermittent perched high water table ranges from 2 to 3.5 feet between January and April in normal years. These soils are not classified as hydric.

Nappanee loam (43A)
The Nappanee series consists of very deep, somewhat poorly drained soils that are moderately deep or deep to dense till that formed in clayey till. The depth to bedrock is greater than 60 inches. These soils are found on wave-worked till plains, till-floored lake plains, till plains and moraines. Slopes range from 0 to 6 percent. Rock fragments consist of glacial erratics of mixed lithology, primarily shale, limestone, and igneous gravel. The depth to the top of an intermittent perched high water table ranges from 0.5 to 2 feet between November and May in normal years. These soils are not classified as hydric.

Nappanee loam (NnA)
The Nappanee series consists of very deep, somewhat poorly drained soils that are moderately deep or deep to dense till that formed in clayey till. The depth to bedrock is greater than 60 inches. These soils are found on wave-worked till plains, till-floored lake plains, till plains and moraines. Slopes range from 0 to 2 percent. Rock fragments consist of glacial erratics of mixed lithology, primarily shale, limestone, and igneous gravel. The depth to the top of an intermittent perched high water table ranges from 0.5 to 2 feet between November and May in normal years. These soils are not classified as hydric.

Nappanee silt loam (NaA)
The Nappanee silt loam series consists of deep, somewhat poorly drained soils that are moderately deep or deep to dense till that formed in clayey till. The depth to bedrock is greater than 60 inches. These soils are found on slight rises and low slope breaks along drainageways. Slopes range from 0 to 3 percent. The depth to the top of a perched seasonal high water table ranges from 1 to 2 feet during extended wet periods. These soils are not classified as hydric.

Nappanee silty clay loam (NaA)
The Nappanee series consists of very deep, somewhat poorly drained soils that are moderately deep or deep to dense till that formed in clayey till. The depth to bedrock is greater than 60 inches. These soils are found on wave-worked till plains, till-floored lake plains, till plains and moraines. Slopes range from 0 to 6 percent. In Nappanee silty clay loam, the depth to the top of the perched seasonal high water table ranges from 0.5 to 1 feet between November and May in normal years. These soils are not classified as hydric.

Oakville find sand (49B)
The Oakville fine sand series consists of very deep, well drained soils formed in sandy eolian deposits. Depth to bedrock is greater than 80 inches. These soils occur on the side slopes of long, narrow beach ridges and sand dunes on outwash plains, lake plains and moraines. Slopes range from 0 to 12 percent. The depth to an apparent seasonal high water table is more than 6 feet. These soils are not classified as hydric.

Oshtemo loamy sand (OsB)
The Oshtemo series consists of deep, well drained, nearly level to sloping soils that formed in stratified loamy and sandy deposits of Wisconsin age that have a high content of quartz and contain variable amounts of material derived from igneous and metamorphic rocks, sandstone, limestone and dolomite. The depth to bedrock is greater than 80 inches. These soils are found on outwash plains, valley trains, moraines and beach ridges. Oshtemo loamy sands range in slope from 0 to 6 percent. In some areas, the loamy sand contains bands of irregularly shaped bodies of sandy loam or loam. Permeability is moderately rapid in the upper loamy materials and very rapid in the lower sandy materials. These soils are not classified as hydric.

Owosso-Miami complex (OwC)

The Owosso-Miami complex is found in broad upland areas and on low rises and side slopes of till plains and moraines. The complex consists of the Owosso series and Miami series. Slopes for the complex range from 2 to 6 percent. The Owosso series consists of very deep, well drained soils that formed in loamy glaciofluvial deposits and the underlying till on till plains and moraines. Depth to bedrock is greater than 60 inches. The Miami series consists of very deep, moderately well drained soils that are moderately deep to dense till and formed in as much as 18 inches of loess or silty material in the underlying loamy till. These are found on till plains. Depth to bedrock is greater than 80 inches. In Miami soils, the depth to the top of a perched seasonal high water table ranges from 2 to 3 feet between December and April in normal years. These soils in the Owosso-Miami complex are not classified as hydric.

Pella silt loam (Pc)

The Pella series consists of very deep, poorly drained soils formed in 20 to 40 inches of loamy or silty sediments and the underlying stratified loamy glacial sediments. Depth to bedrock is greater than 60 inches. These soils are found on nearly level or depressional areas on lake plains, outwash plains, and till plains. They have plane or convex slopes with gradients typically less than 1 percent although slopes range from 0 to 3 percent. Average fine and coarser sand content of the particle-size control section is less than 15 percent, and average clay content of the particle-size control section is 27 to 35 percent. An apparent seasonal high water table is at 0.5 foot above the surface to 1.0 foot below the surface at some time during spring in most years. These soils are classified as hydric.

Pewamo clay loam (Pm, 22)

The Pewamo series consists of very deep, very poorly drained soils formed in till. The depth to bedrock is greater than 60 inches. These soils are found on moraines, near-shore zones (relict), and lake plains. Slopes range from 0 to 1 percent. Depth to an apparent seasonal high water table ranges from 1 foot above the surface to 1 foot below the surface from December to May in normal years. These soils are classified as hydric.

Plainfield and Berrien loamy sands (PdA)

The Plainfield and Berrien loamy sands consist of very deep, moderately well-drained to excessively drained soils formed in sandy drift. Depth to bedrock is greater than 60 inches. Plainfield soils are found on outwash plains, alley trains, glacial lake basins, stream terraces and moraines and other upland areas. Berrien soils are found on narrow beach ridges of old glacial lakes and on the swells of sandbars. Slopes range from 0 to 3 percent. In Plainfield soils, the particle-size control section is dominated by medium sand, but individual horizons within or below the particle-size control section are fine sand or coarse sand. Volume of gravel ranges from 0 to 15 percent as a weighted average throughout the pedon, but thin subhorizons contain as much as 35 percent gravel in some pedons. These soils are not classified as hydric.

Rawson sandy loam (RbB)

The Rawson sandy loam series consists of very deep, moderately well drained soils that are moderately deep or deep to dense till. The depth to bedrock is greater than 60 inches. Rawson soils formed in loamy sediments and till and are found on till plains, outwash plains, and lake plains. Slopes range from 2 to 6 percent. Depth to unweathered till or lacustrine deposits ranges from 25 to 51 inches. Depth to the top of an intermittent perched high water table ranges from 2.0 to 3.5 feet between January and April in normal years. These soils are not classified as hydric.

Sebewa sandy loam (SbA)

The Seweba series consists of poorly to very poorly drained soils that formed in loamy materials. The soils overlie calcareous sand and gravel. Depth to bedrock is greater than 80 inches. Depth to calcareous sand and gravel ranges from 24 to 42 inches. These soils are found on naturally wet flats in old glacial drainageways and on outwash or delta plains. Slopes range from 0 to 3 percent. In places there is a thin layer of muck on the surface. These soils are classified as hydric.

Seward sandy loam, loamy subsoil variant (SfB)
The Seward variant series consists of very deep, moderately well drained soils that are moderately deep or deep to dense till. They formed in a thin layer of loamy textured glaciofluvial deposits over clayey textured glacial till or lacustrine deposits. Depth to bedrock is greater than 80 inches. These are located on lake plains, ground moraines and till plains. Slopes range from 2 to 6 percent. The depth to the top of an intermittent perched high water table ranges from 18 to 36 inches between January and April in normal years. These soils are not classified as hydric.

Sisson fine sandy loam (SnB)
The Sission series consists of deep, well drained soils that formed in stratified loamy and silty material. The depth to bedrock is greater than 60 inches. The potential for surface runoff ranges from negligible to high depending on the slope gradient. Permeability is moderate. These soils are found mainly on deltas in areas of former lake plains. Slopes range from 2 to 18 percent. These are not classified as hydric.

Sloan loam (30, Sc)
The Sloan series consists of very deep and very poorly drained soils formed in loamy alluvium washed mainly from soils formed in loamy calcareous drift. The depth to bedrock is greater than 60 inches. These are found on floodplains or in depressions along streams receiving sediment from areas of Wisconsinan age glaciation. Slopes range from 0 to 2 percent. Depth to the top of an intermittent apparent high water table ranges from 1 foot above the surface to 1 foot below the surface between November and June in normal years. These soils are subject to flooding from late fall to spring and are classified as hydric.

Spinks loamy sand (SpB)
The Spinks series consists of very deep, well drained soils formed in sandy eolian or outwash material. The depth to bedrock is greater than 100 inches. Spinks soils are found on dunes, moraines, till plains, outwash plains, beach ridges and lake plains. Slopes ranges from 0 to 12 percent. Rock fragment content consists of glacial erratics (dominantly gravel) of sedimentary and crystalline lithology. These soils are not classified as hydric.

St. Clair loam (SdD, StB)
The St. Clair loam series consists of very deep, moderately well drained soils formed in drift. The depth to bedrock is greater than 48 inches and typically greater than 60 inches. St-Clair loam soils are found on the summits, shoulders, and backslopes of rises, knolls and dissected areas along streams and on lake plains. Slopes range from 2 to 25 percent. These soils are not classified as hydric.

Thetford loamy sand (40A)
The Thetford series consists of very deep, somewhat poorly drained soils formed in sandy till or outwash. Depth to bedrock is greater than 60 inches. These are found on ground moraines, end moraines, lake plains, outwash plains, terraces and beach ridges. Slopes range from 0 to 3 percent. The depth to the top of a seasonal high water table ranges from 1 to 2 feet between February and May in normal years. These soils are not classified as hydric.

Wasepi Sandy Loam (WaA)
The Wasepi series consists of very deep, somewhat poorly drained soils formed in loamy and sandy glaciofluvial deposits underlain by sand and gravel at 20 to 40 inches. Depth to bedrock is greater than 60 inches. These soils are found on outwash plains, deltas, valley trains, glacial drainageways, and lake plains. Slopes range from 0 to 4 percent. These soils are not classified as hydric.

Wasepi sandy loam, loamy substratum (WbA)
The Wasepi series consists of very deep, somewhat poorly drained soils formed in loamy and sandy glaciofluvial deposits underlain by sand and gravel at 20 to 40 inches. These soils are the same as the previous soils with the exception of having a loamy substratum. Depth to bedrock is greater than 60

inches. These soils are found on outwash plains, deltas, valley trains, glacial drainageways, and lake plains. Slopes range from 0 to 4 percent. These soils are not classified as hydric.

Wauseon fine sandy loam (Ws)
The Wauseon series consists of very deep, poorly drained to very poorly drained soils formed in loamy and sandy glaciolacustrine sediments and in the underlying till. The depth to bedrock is greater than 60 inches. Wauseon soils are found on lake plains and deltas of the late Wisconsinan age. Slopes range from 0 to 2 percent. Rock fragment content is unlikely to exceed 10 percent and is of glacial origin. These soils are classified as hydric.

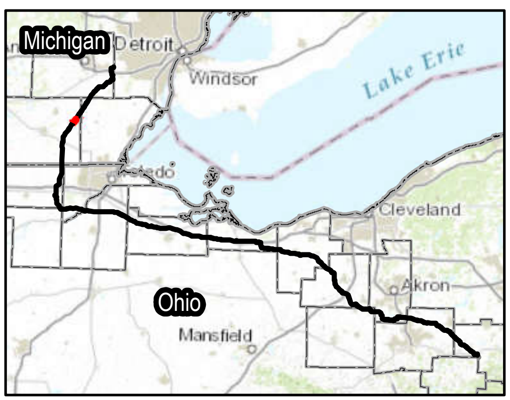
Wauseon loam (WcA)
The Wauseon series consists of very deep, poorly drained to very poorly drained soils formed in loamy and sandy glaciolacustrine sediments and in the underlying till. The depth to bedrock is greater than 60 inches. Wauseon soils are found on lake plains and deltas of the late Wisconsinan age. Slopes range from 0 to 2 percent. Rock fragment content is unlikely to exceed 10 percent and is of glacial origin. These soils are classified as hydric.

Ypsi sandy loam (YpA, 103A)
The Ypsi series consists of very deep, somewhat poorly drained soils formed in loamy lacustrine deposits overlying clayey till or lacustrine deposits. Depth to clayey material ranges from 24 to 40 inches. Depth to bedrock is greater than 60 inches. These soils are found on lake plains terraces and ground moraines Slopes range from 0 to 4 percent. Rock fragment content ranges from 0 to 20 percent in the solum and 0 to 10 percent in the 2C horizons. This soil has a seasonal high water table and subject to ponding in nearly level areas. These soils are not classified as hydric.

Ziegenfuss clay loam (ZfsacA)
The Ziegenfuss series consists of very deep, poorly drained soil found in clayey ablation till overlying dense basal till. Depth to bedrock is typically greater than 80 inches. Ziegenfuss soils are found on till plains, wave-worked till plains, till-floored lake plains, end moraines and ground moraines. Slopes range from 0 to 1 percent. Rock fragment content is 0 to 10 percent. These soils are classified as hydric.

APPENDIX 7B

Soils Crossed by the NEXUS Project Pipeline Facilities



Legend

- ○ Mileposts (0.1 mile)
- NEXUS Mainline Pipeline
- TGP Interconnect
- Access Roads
- Permanent Easement
- Temporary Workspace
- ATWS
- Proposed Compressor Station
- Proposed Contractor Yard
- NRCS Soils
- Project Counties
- Adjacent Page

0 250 500
Feet

Projection: NAD83, UTM Zone 17N US Survey Feet, Grid North. Sources: ESRI, SPECTRA, TRC, USDA NRCS

Appendix 7B

Soils Crossed by the NEXUS Project Pipeline Facilities

Lenawee County

NEXUS GAS TRANSMISSION

Created: 6/1/2015

Legend

- Mileposts (0.1 mile)
- NEXUS Mainline Pipeline
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Feet

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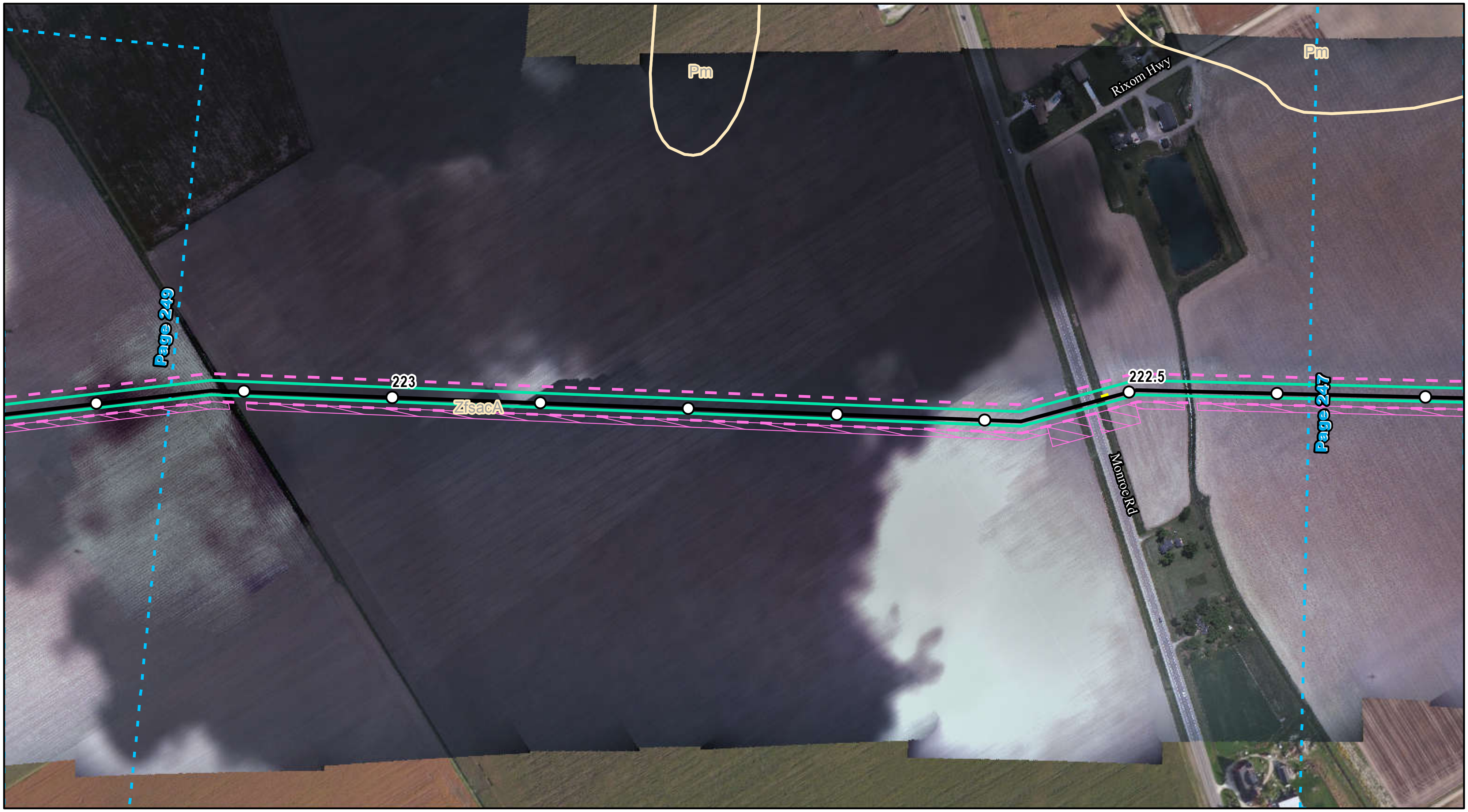
Appendix 7B

Soils Crossed by the NEXUS Project Pipeline Facilities

Lenawee County

NEXUS GAS TRANSMISSION

Created: 6/1/2015



Legend

- Mileposts (0.1 mile)
- NEXUS Mainline Pipeline
- TGP Interconnect
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- Adjacent Page

N

0 250 500
Feet

Projection: NAD83, UTM Zone 17N US Survey Feet, Grid North. Sources: ESRI, SPECTRA, TRC, USDA NRCS

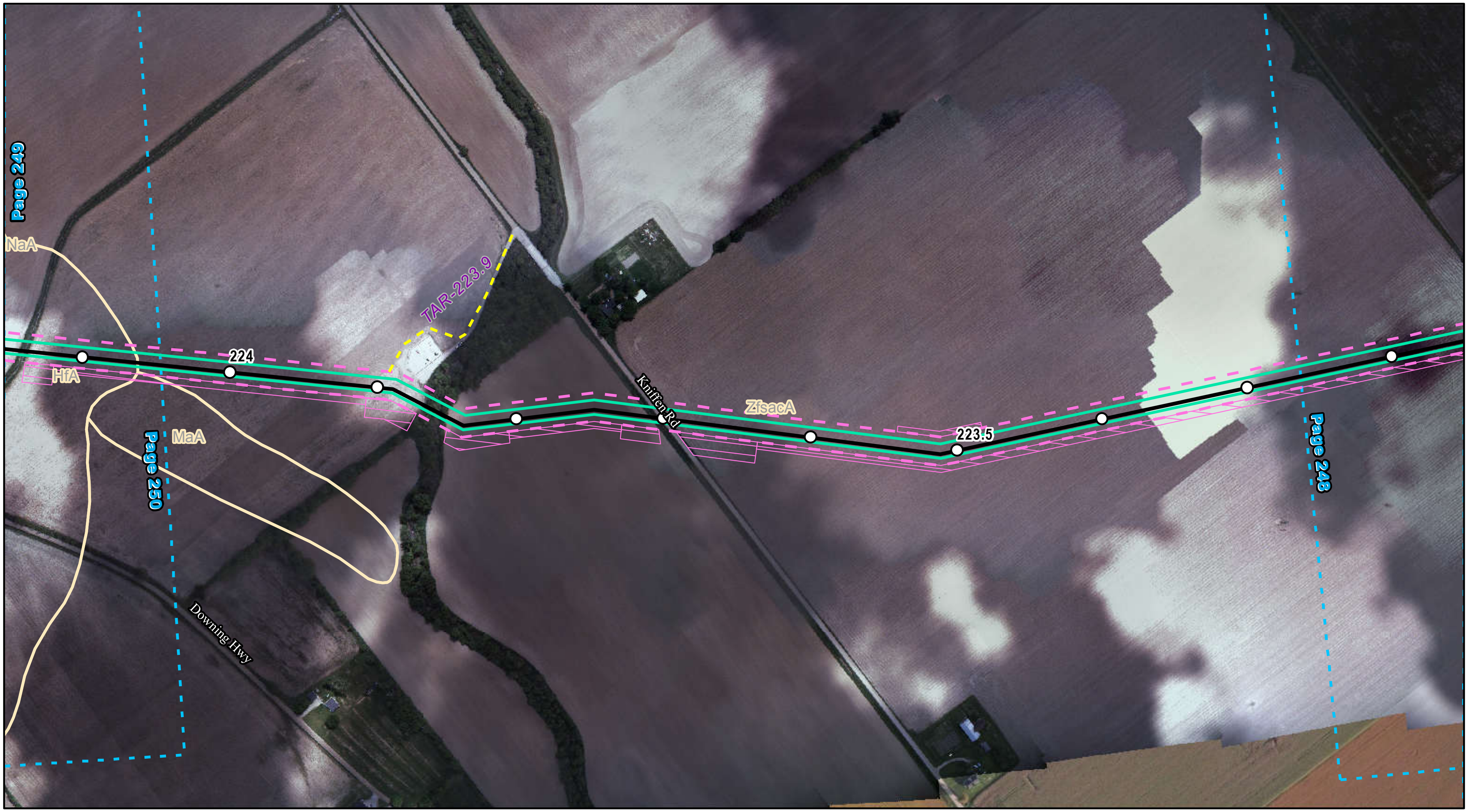
Appendix 7B

Soils Crossed by the NEXUS Project Pipeline Facilities

Lenawee County

NEXUS GAS TRANSMISSION

Created: 6/1/2015



Legend

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N

0 250 500
Feet

Projection: NAD83, UTM Zone 17N US Survey Feet, Grid North. Sources: ESRI, SPECTRA, TRC, USDA NRCS

Appendix 7B

Soils Crossed by the NEXUS Project Pipeline Facilities

Lenawee County

NEXUS GAS TRANSMISSION

Created: 6/1/2015

Legend

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Feet

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Appendix 7B

Soils Crossed by the NEXUS Project Pipeline Facilities

Lenawee County

NEXUS GAS TRANSMISSION

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0 250 500
Feet

Projection: NAD83, UTM Zone 17N US Survey Feet, Grid North. Sources: ESRI, SPECTRA, TRC, USDA NRCS

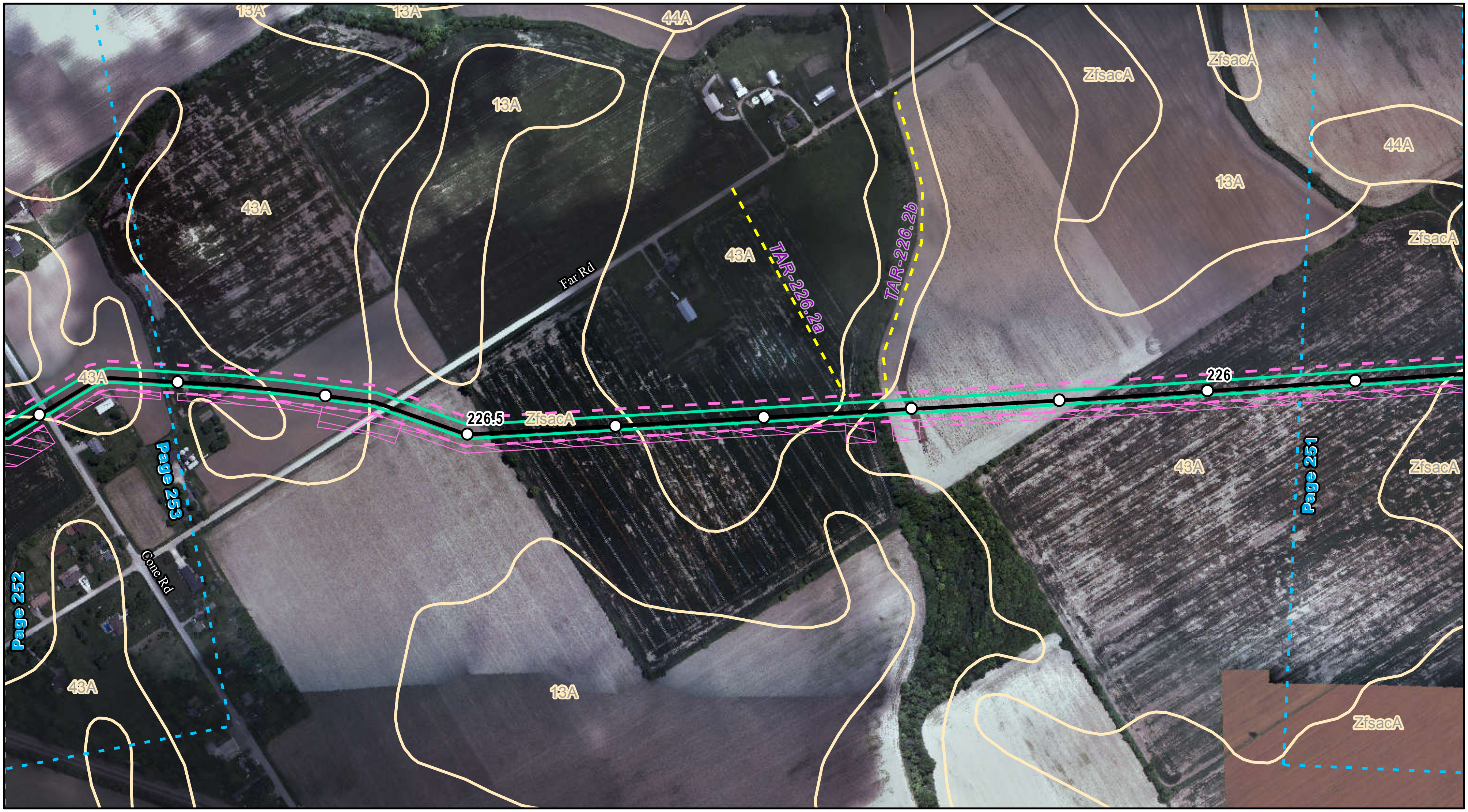
Appendix 7B

Soils Crossed by the NEXUS Project Pipeline Facilities

Monroe County

NEXUS GAS TRANSMISSION

Created: 6/1/2015



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0 250 500
Feet

Projection: NAD83, UTM Zone 17N US Survey Feet, Grid North. Sources: ESRI, SPECTRA, TRC, USDA NRCS

Appendix 7B

Soils Crossed by the NEXUS Project Pipeline Facilities

Monroe County

NEXUS GAS TRANSMISSION

Created: 6/1/2015

Legend

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N

0 250 500
Feet

Projection: NAD83, UTM Zone 17N US Survey Feet, Grid North. Sources: ESRI, SPECTRA, TRC, USDA NRCS

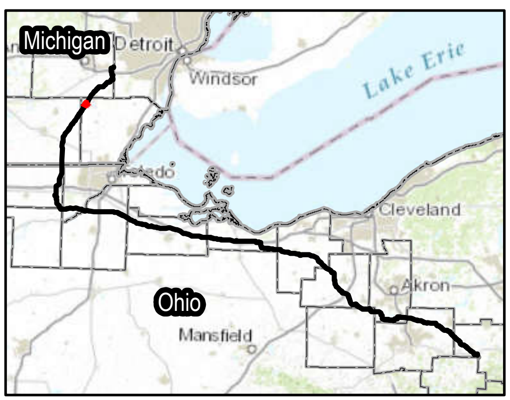
Appendix 7B

Soils Crossed by the NEXUS Project Pipeline Facilities

Monroe County

NEXUS GAS TRANSMISSION

Created: 6/1/2015



Legend

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0 250 500

Feet

Projection: NAD83, UTM Zone 17N US Survey Feet, Grid North. Sources: ESRI, SPECTRA, TRC, USDA NRCS

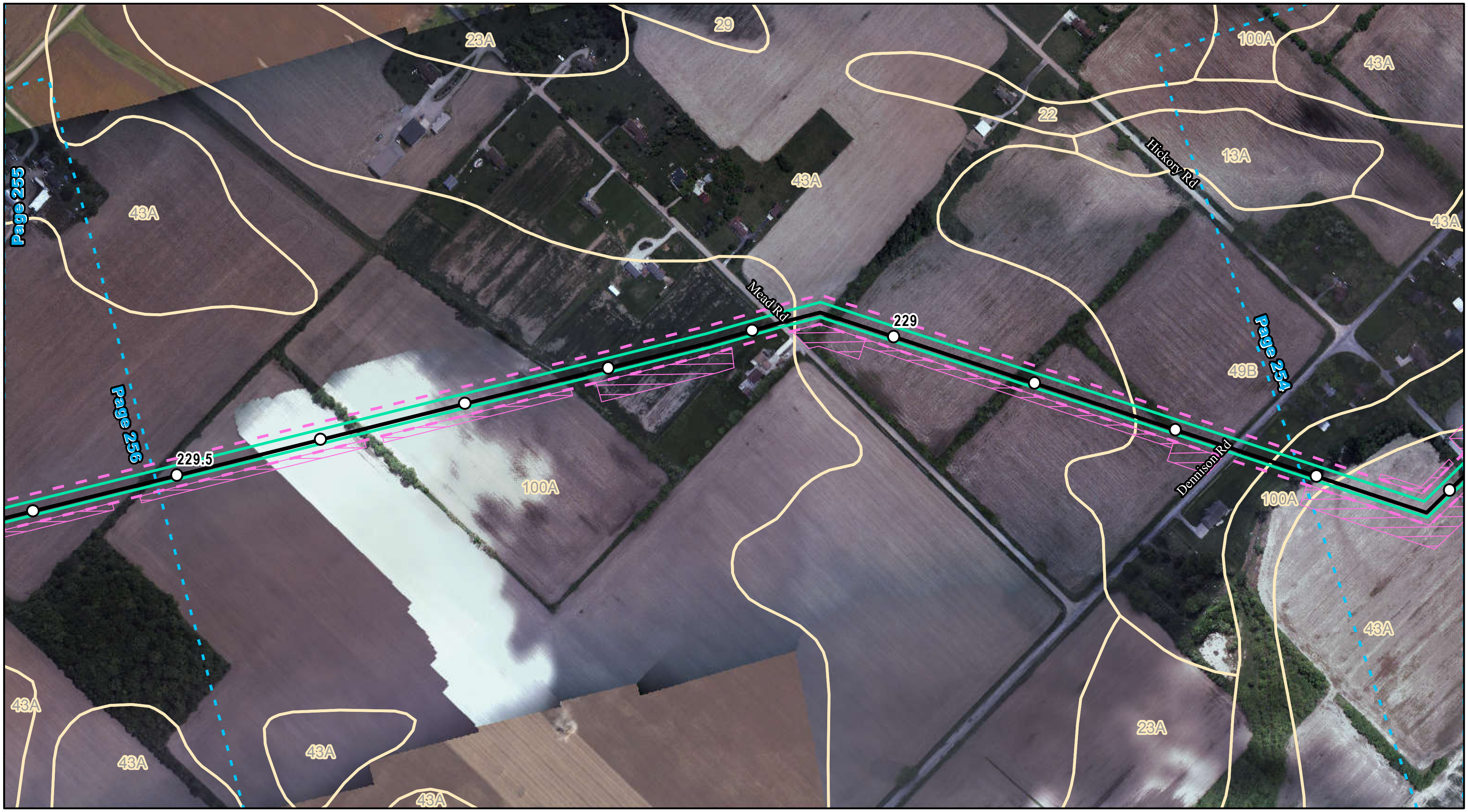
Appendix 7B

Soils Crossed by the NEXUS Project Pipeline Facilities

Monroe County

NEXUS GAS TRANSMISSION

Created: 6/1/2015



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N

0 250 500
Feet

Projection: NAD83, UTM Zone 17N US Survey Feet, Grid North. Sources: ESRI, SPECTRA, TRC, USDA NRCS

Appendix 7B

Soils Crossed by the NEXUS Project Pipeline Facilities

Monroe County

NEXUS GAS TRANSMISSION

Created: 6/1/2015

Legend

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N

0 250 500
Feet

Projection: NAD83, UTM Zone 17N US Survey Feet, Grid North. Sources: ESRI, SPECTRA, TRC, USDA NRCS

Appendix 7B

Soils Crossed by the NEXUS Project Pipeline Facilities

Monroe County

NEXUS GAS TRANSMISSION

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Legend

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0 250 500
Feet

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Appendix 7B

Soils Crossed by the NEXUS Project Pipeline Facilities

Monroe County

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0 250 500
Feet

Projection: NAD83, UTM Zone 17N US Survey Feet, Grid North. Sources: ESRI, SPECTRA, TRC, USDA NRCS

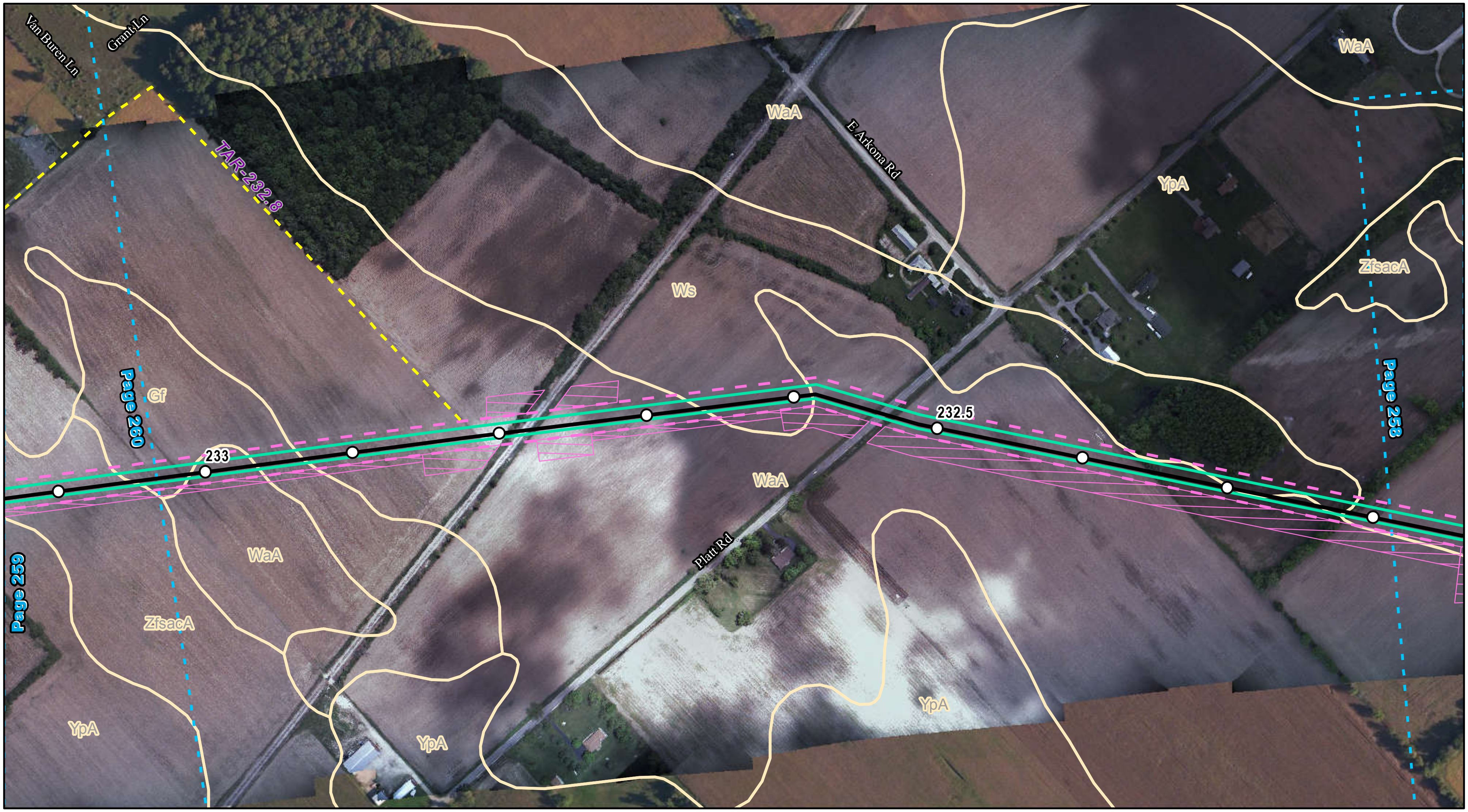
Appendix 7B

Soils Crossed by the NEXUS Project Pipeline Facilities

Washtenaw County

NEXUS GAS TRANSMISSION

Created: 6/1/2015



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0 250 500
Feet

Projection: NAD83, UTM Zone 17N US Survey Feet, Grid North. Sources: ESRI, SPECTRA, TRC, USDA NRCS

Appendix 7B

Soils Crossed by the NEXUS Project Pipeline Facilities

Washtenaw County

NEXUS GAS TRANSMISSION

Created: 6/1/2015

Legend

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N

0 250 500
Feet

Projection: NAD83, UTM Zone 17N US Survey Feet, Grid North. Sources: ESRI, SPECTRA, TRC, USDA NRCS

Appendix 7B

Soils Crossed by the NEXUS Project Pipeline Facilities

Washtenaw County

NEXUS GAS TRANSMISSION

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N

0 250 500
Feet

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Appendix 7B

Soils Crossed by the NEXUS Project Pipeline Facilities

Washtenaw County

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Legend

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Feet

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Appendix 7B

Soils Crossed by the NEXUS Project Pipeline Facilities

Washtenaw County

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Legend

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0 250 500
Feet

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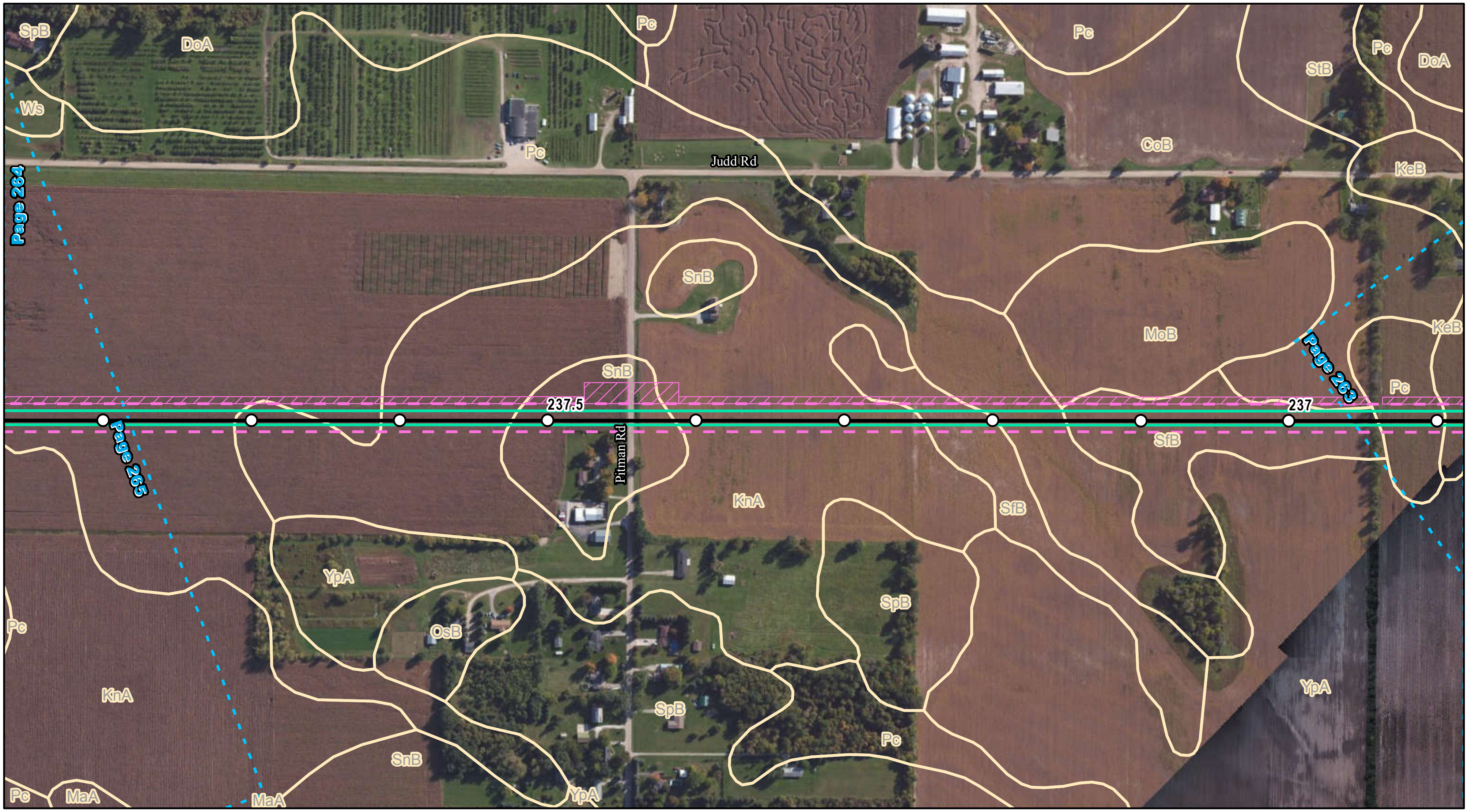
Appendix 7B

Soils Crossed by the NEXUS Project Pipeline Facilities

Washtenaw County

NEXUS GAS TRANSMISSION

Created: 6/1/2015



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0 250 500
Feet

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Appendix 7B

Soils Crossed by the NEXUS Project Pipeline Facilities

Washtenaw County

NEXUS GAS TRANSMISSION

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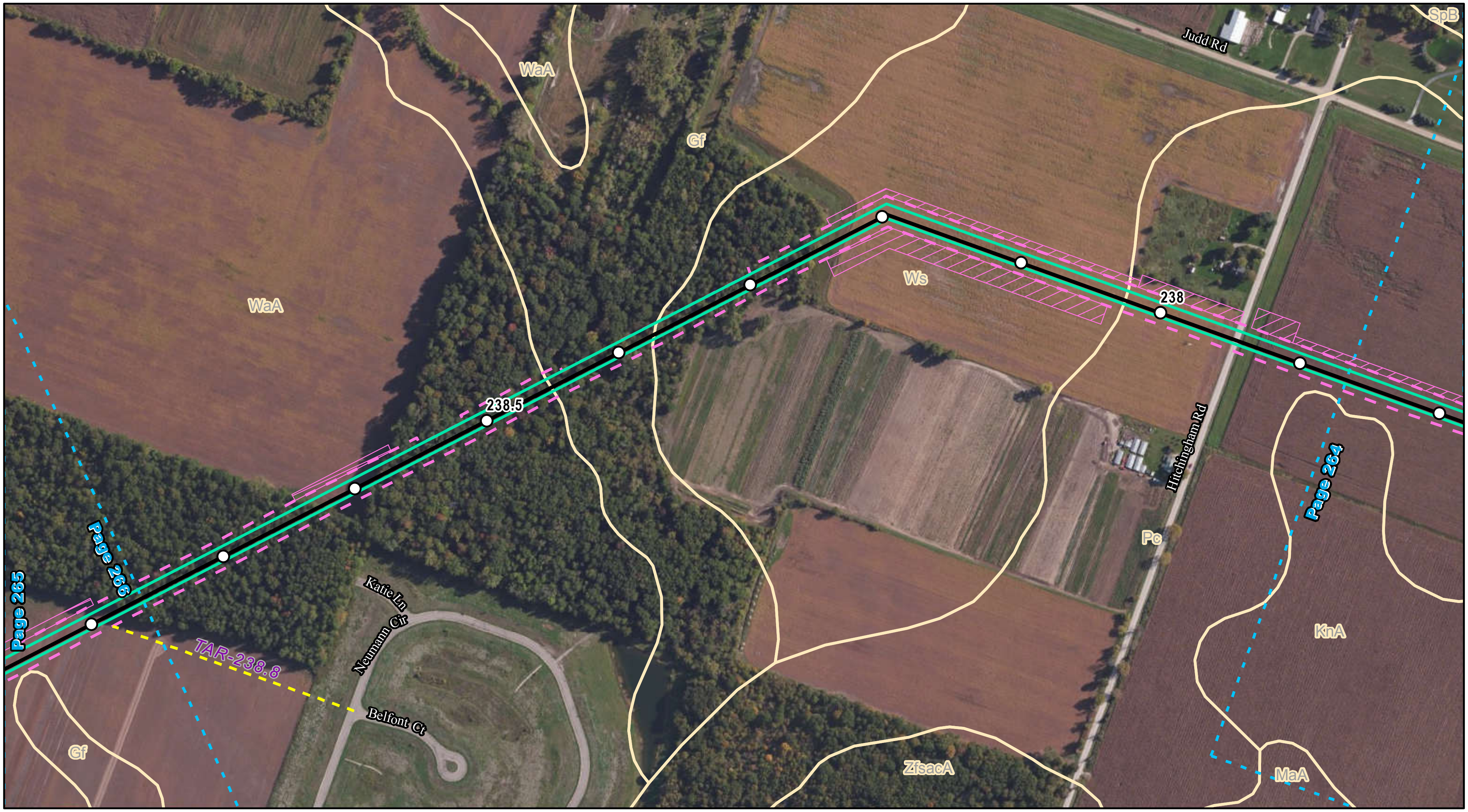
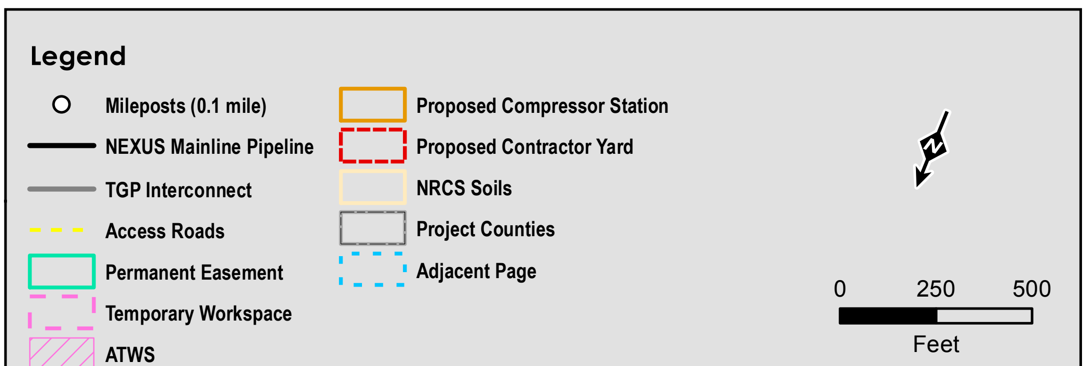




Projection: NAD83, UTM Zone 17N US Survey Feet, Grid North. Sources: ESRI, SPECTRA, TRC, USDA NRCS

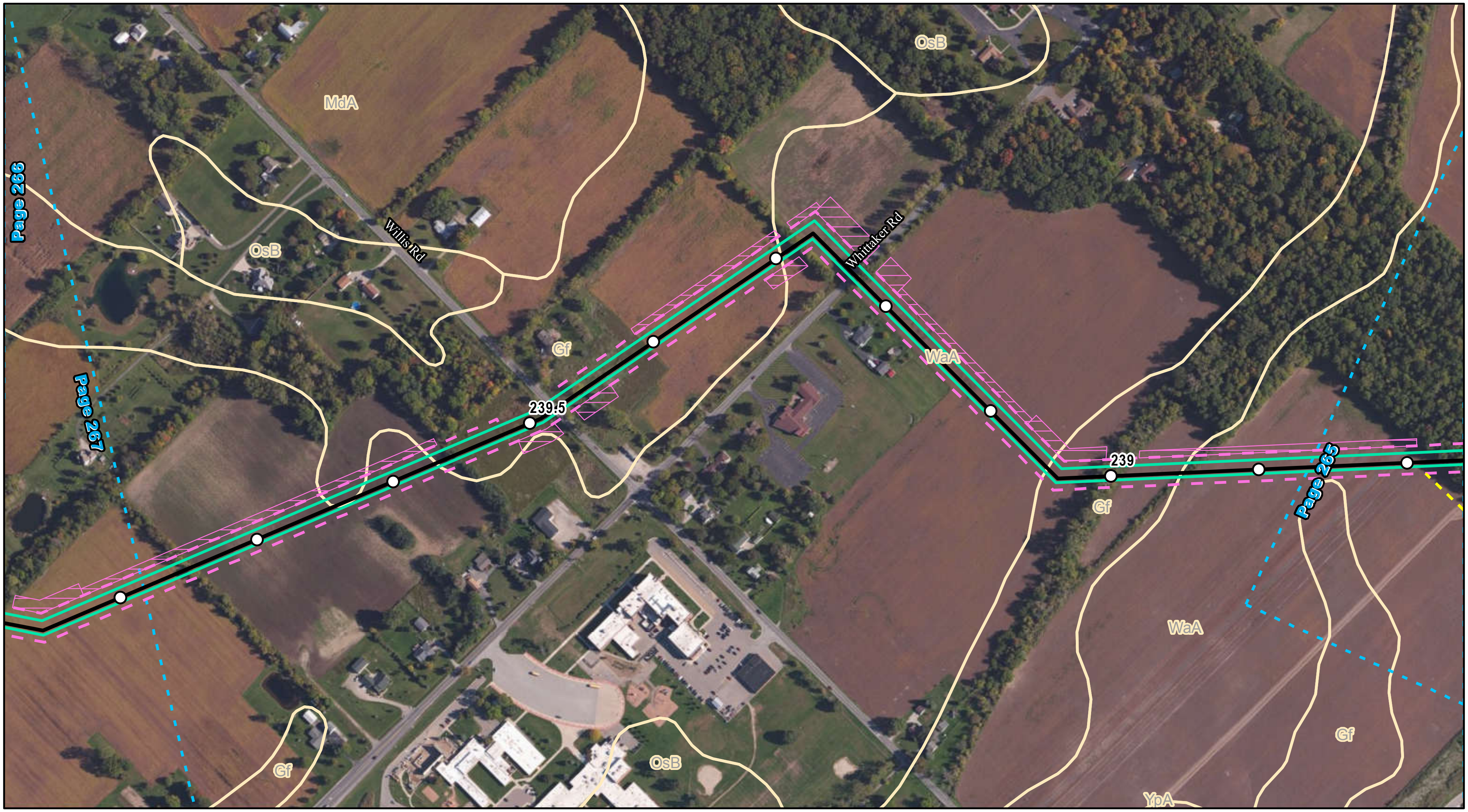
Appendix 7B

Soils Crossed by the NEXUS Project Pipeline Facilities

Washtenaw County

NEXUS GAS TRANSMISSION

Created: 6/1/2015



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0 250 500
Feet

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Appendix 7B

Soils Crossed by the NEXUS Project Pipeline Facilities

Washtenaw County

NEXUS GAS TRANSMISSION

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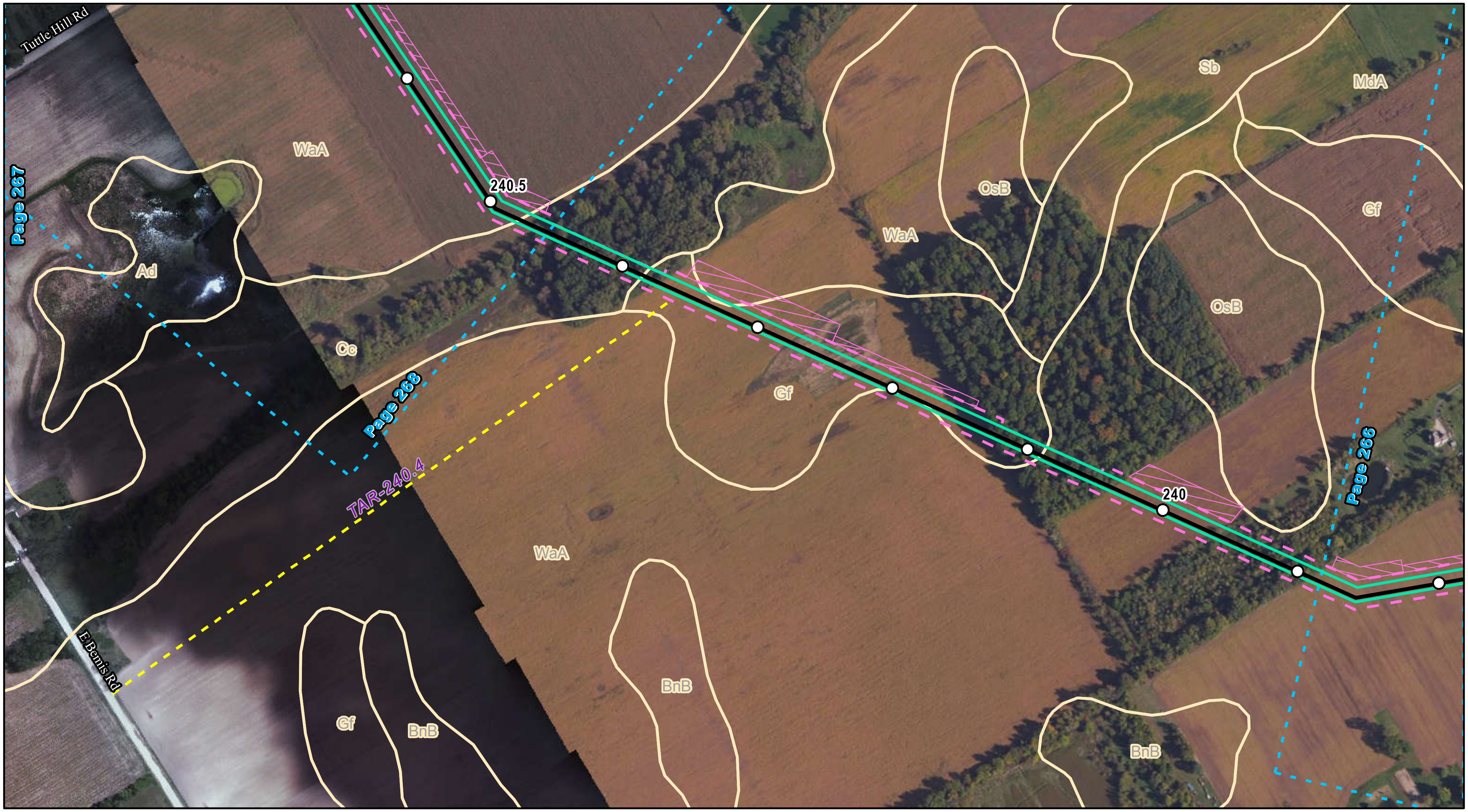

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N

0 250 500
Feet

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Appendix 7B

Soils Crossed by the NEXUS Project Pipeline Facilities

Washtenaw County

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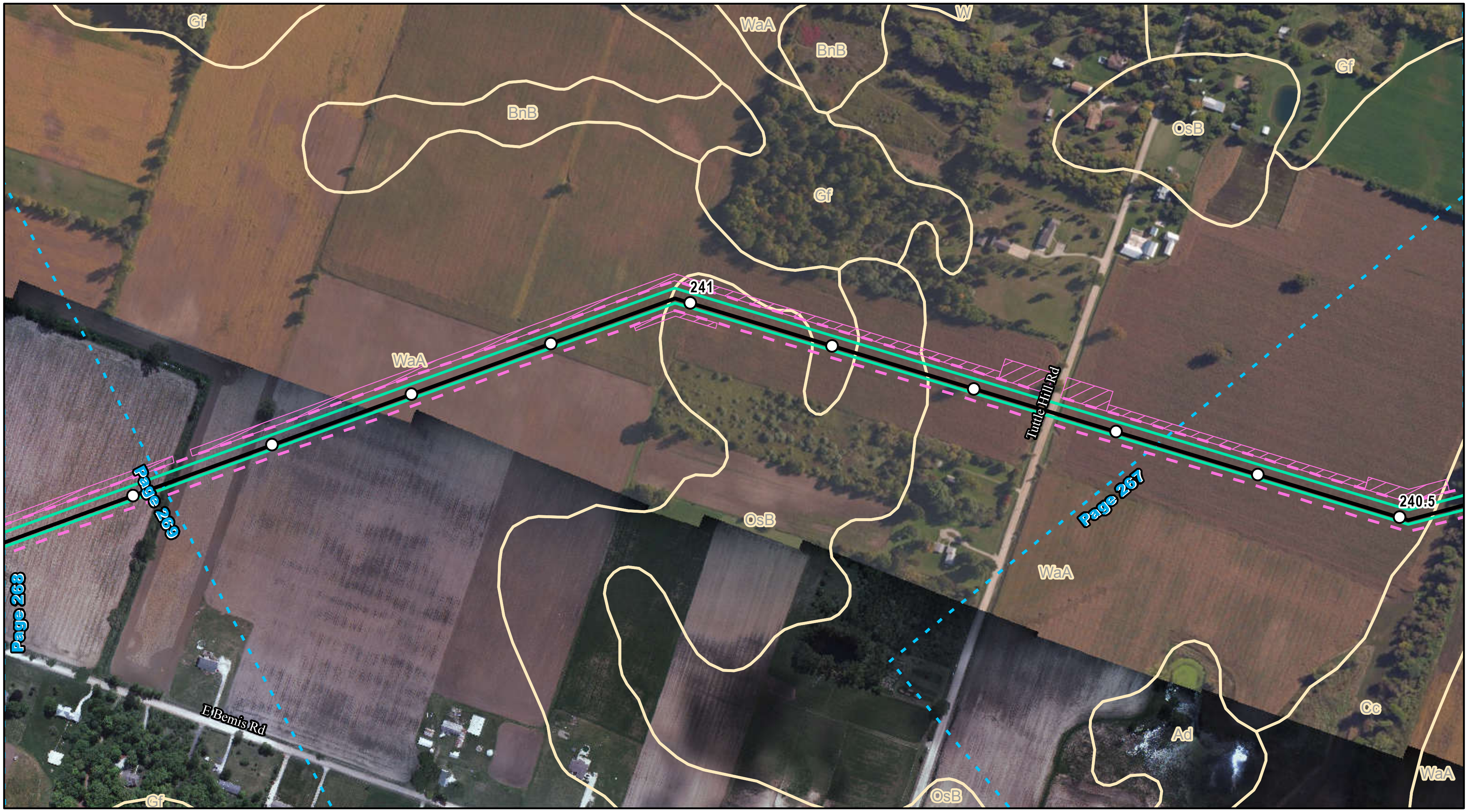

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N

0 250 500
Feet

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Appendix 7B

Soils Crossed by the NEXUS Project Pipeline Facilities

Washtenaw County

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Appendix 7B

Soils Crossed by the NEXUS Project Pipeline Facilities

Washtenaw County

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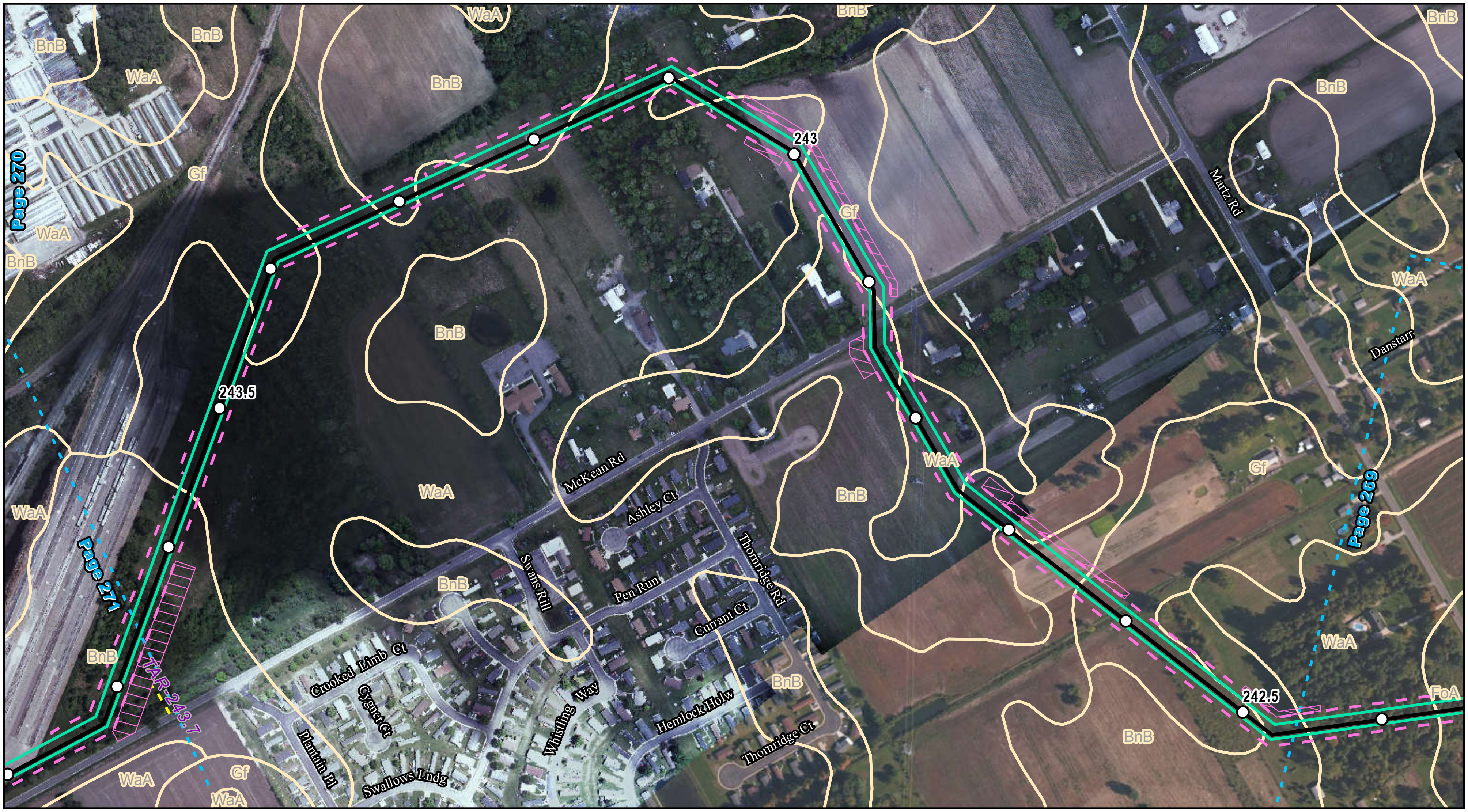

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Soils Crossed by the NEXUS Project Pipeline Facilities

Washtenaw County

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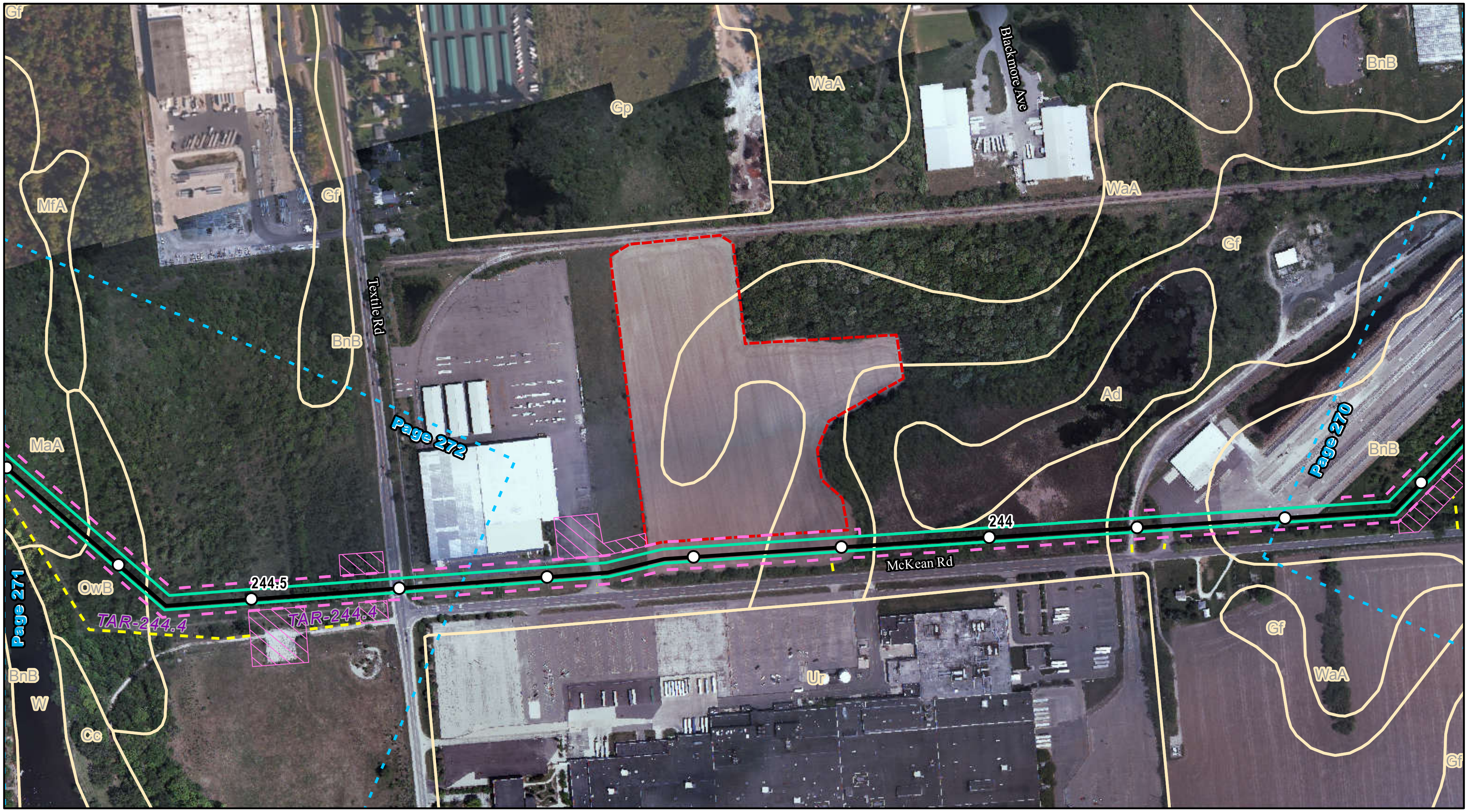

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Appendix 7B

Soils Crossed by the NEXUS Project Pipeline Facilities

Washtenaw County

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Appendix 7B

Soils Crossed by the NEXUS Project Pipeline Facilities

Washtenaw County

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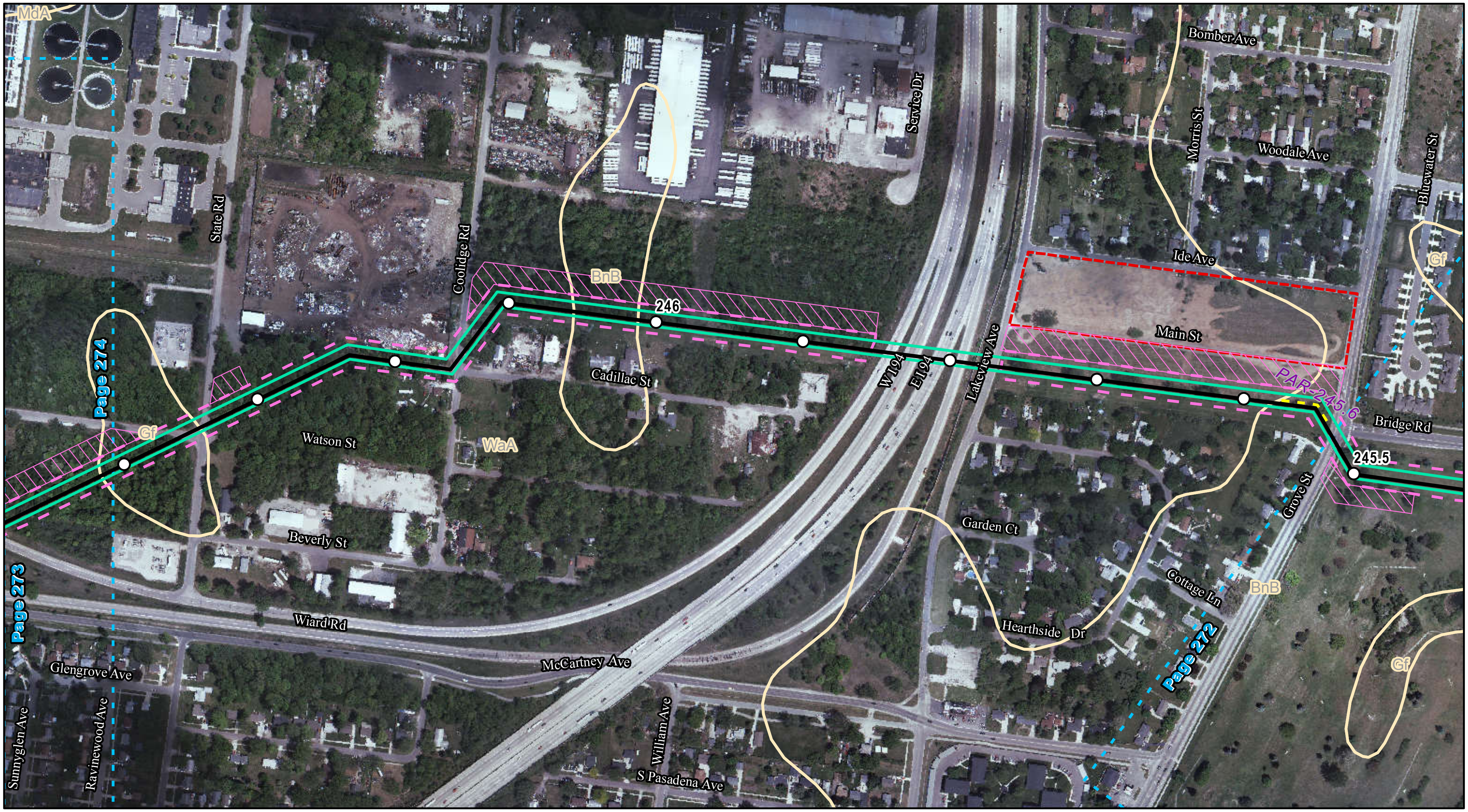

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Appendix 7B

Soils Crossed by the NEXUS Project Pipeline Facilities

Washtenaw County

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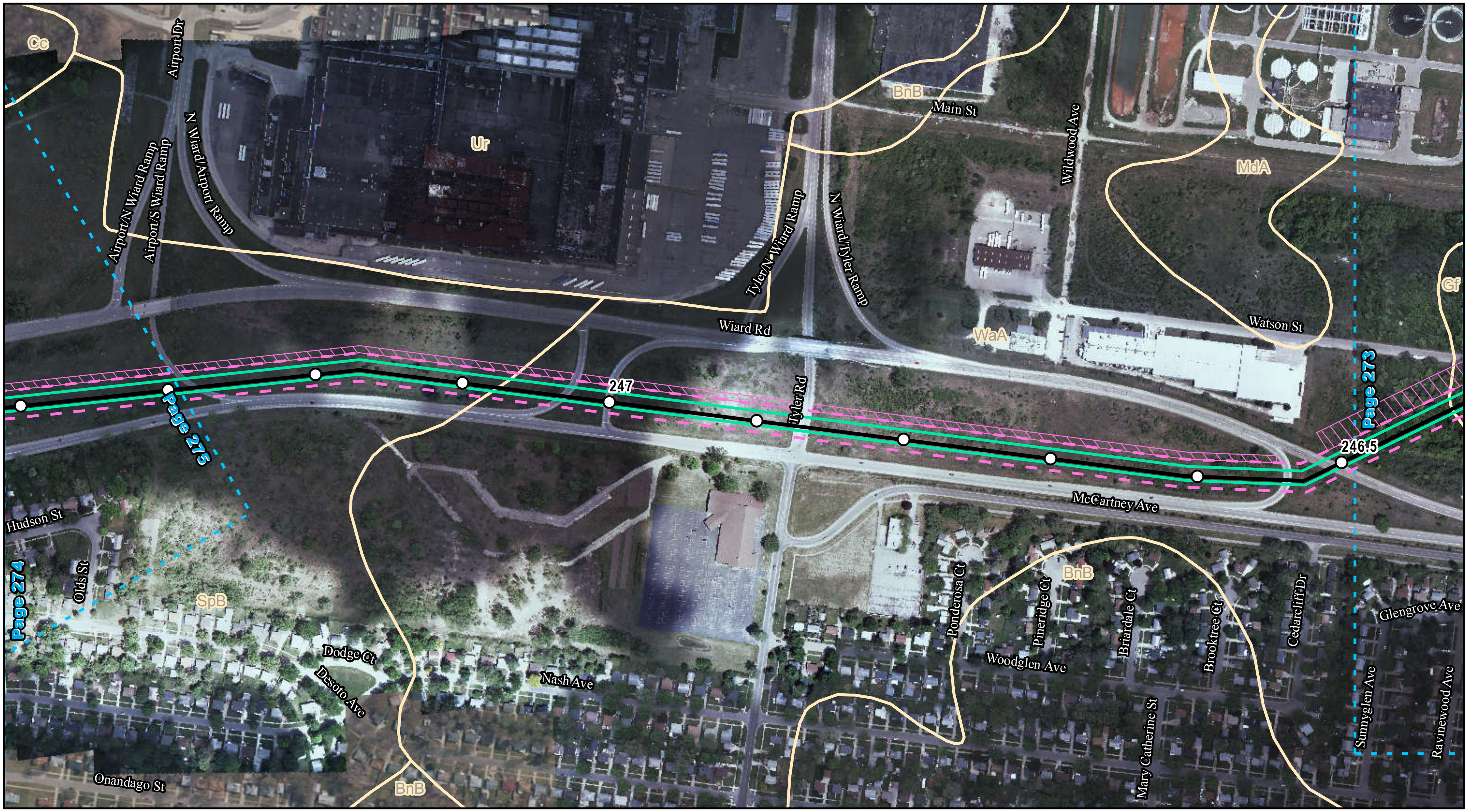

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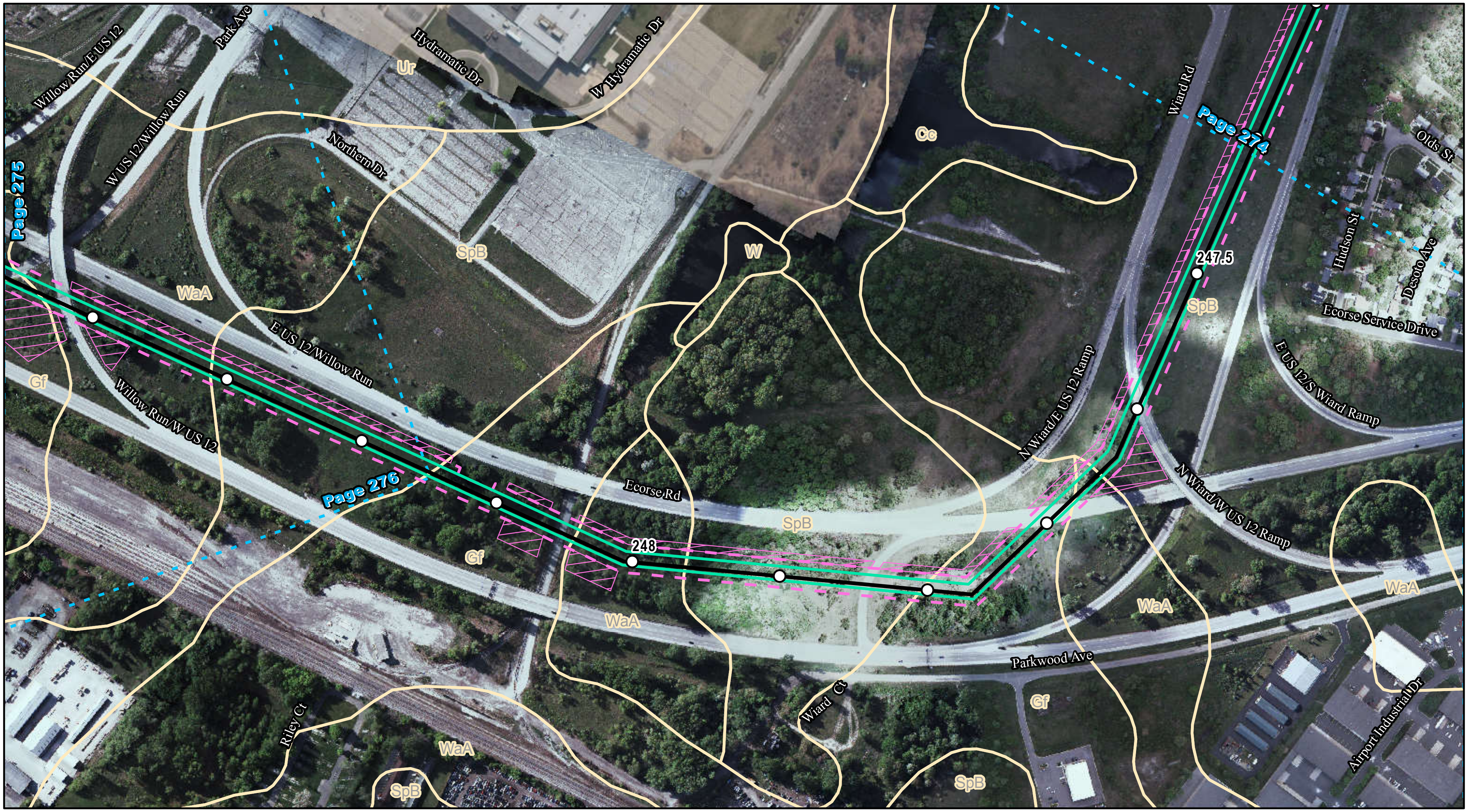
Appendix 7B

Soils Crossed by the NEXUS Project Pipeline Facilities

Washtenaw County

NEXUS GAS TRANSMISSION

Created: 6/1/2015



Legend

- Mileposts (0.1 mile)
- NEXUS Mainline Pipeline
- TGP Interconnect
- Access Roads
- Permanent Easement
- Temporary Workspace
- ATWS
- Proposed Compressor Station
- Proposed Contractor Yard
- NRCS Soils
- Project Counties
- Adjacent Page

0 250 500
Feet

Projection: NAD83, UTM Zone 17N US Survey Feet, Grid North. Sources: ESRI, SPECTRA, TRC, USDA NRCS

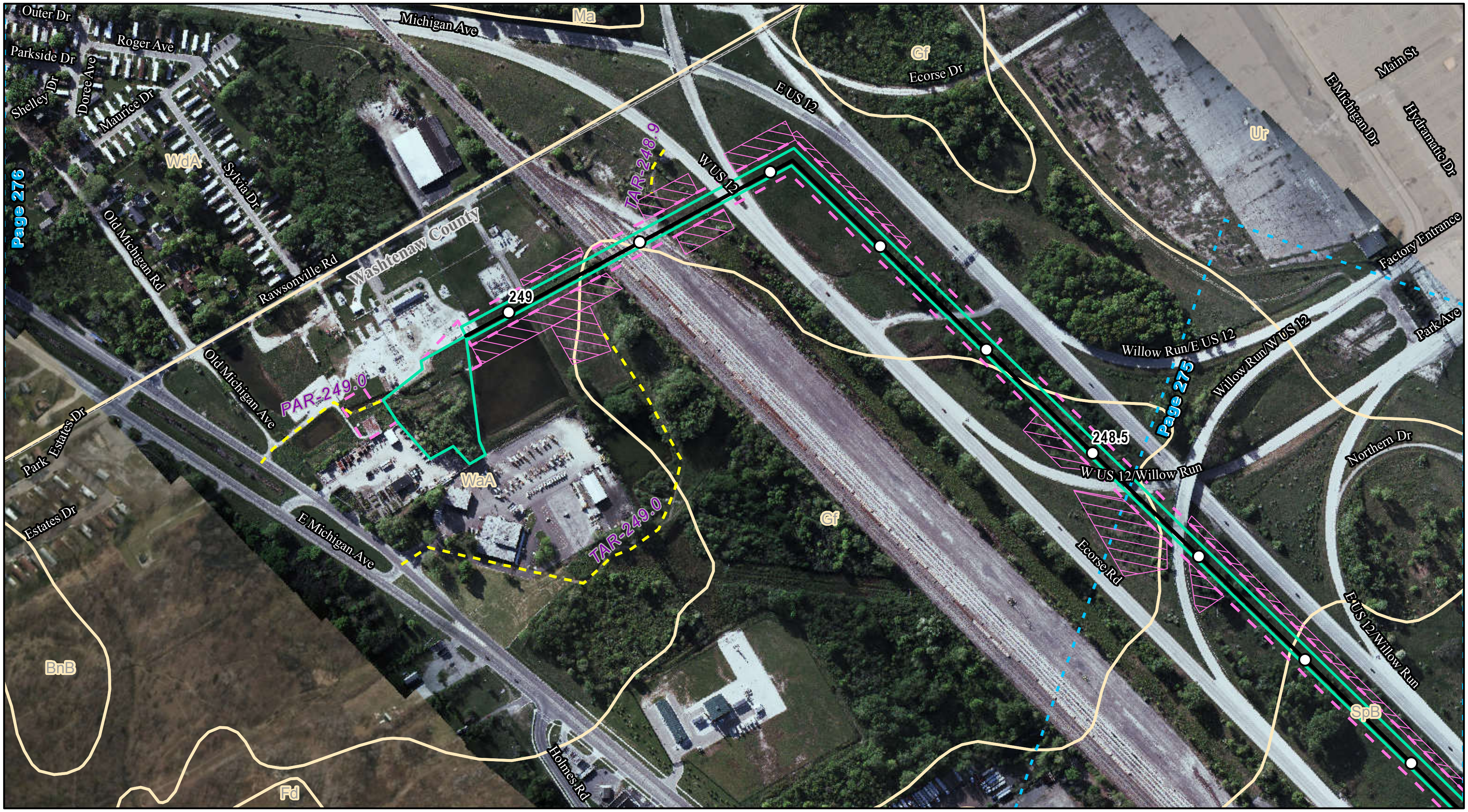
Appendix 7B

Soils Crossed by the NEXUS Project Pipeline Facilities

Washtenaw County

NEXUS GAS TRANSMISSION

Created: 6/1/2015



Legend

- Mileposts (0.1 mile)
- NEXUS Mainline Pipeline
- TGP Interconnect
- Access Roads
- Permanent Easement
- Temporary Workspace
- ATWS
- Proposed Compressor Station
- Proposed Contractor Yard
- NRCS Soils
- Project Counties
- Adjacent Page

N

0 250 500
Feet

Projection: NAD83, UTM Zone 17N US Survey Feet, Grid North. Sources: ESRI, SPECTRA, TRC, USDA NRCS

Appendix 7B

Soils Crossed by the NEXUS Project Pipeline Facilities

Washtenaw County

NEXUS GAS TRANSMISSION

Created: 6/1/2015

Legend

- Mileposts (0.1 mile)
- NEXUS Mainline Pipeline
- TGP Interconnect
- Access Roads
- Permanent Easement
- Temporary Workspace
- ATWS
- Proposed Compressor Station
- Proposed Contractor Yard
- NRCS Soils
- Project Counties
- Adjacent Page

N

0 250 500
Feet

Projection: NAD83, UTM Zone 17N US Survey Feet, Grid North. Sources: ESRI, SPECTRA, TRC, USDA NRCS

Appendix 7B

Soils Crossed by the NEXUS Project Pipeline Facilities

Erie County

NEXUS GAS TRANSMISSION

Created: 6/1/2015

Legend

- Mileposts (0.1 mile)
- NEXUS Mainline Pipeline
- TGP Interconnect
- Access Roads
- Permanent Easement
- Temporary Workspace
- ATWS
- Proposed Compressor Station
- Proposed Contractor Yard
- NRCS Soils
- Project Counties
- Adjacent Page

N

0 250 500

Feet

Projection: NAD83, UTM Zone 17N US Survey Feet, Grid North. Sources: ESRI, SPECTRA, TRC, USDA NRCS

Appendix 7B

Soils Crossed by the NEXUS Project Pipeline Facilities

Wood County

NEXUS GAS TRANSMISSION

Created: 6/1/2015

Legend

- Mileposts (0.1 mile)
- NEXUS Mainline Pipeline
- TGP Interconnect
- Access Roads
- Permanent Easement
- Temporary Workspace
- ATWS
- Proposed Compressor Station
- Proposed Contractor Yard
- NRCS Soils
- Project Counties
- Adjacent Page

0 250 500
Feet

Projection: NAD83, UTM Zone 17N US Survey Feet, Grid North. Sources: ESRI, SPECTRA, TRC, USDA NRCS

Appendix 7B

Soils Crossed by the NEXUS Project Pipeline Facilities

Lucas County

NEXUS GAS TRANSMISSION

Created: 6/1/2015

Legend

- Mileposts (0.1 mile)
- NEXUS Mainline Pipeline
- TGP Interconnect
- Access Roads
- Permanent Easement
- Temporary Workspace
- ATWS
- Proposed Compressor Station
- Proposed Contractor Yard
- NRCS Soils
- Project Counties
- Adjacent Page

N

0 250 500
Feet

Projection: NAD83, UTM Zone 17N US Survey Feet, Grid North. Sources: ESRI, SPECTRA, TRC, USDA NRCS

Appendix 7B

Soils Crossed by the NEXUS Project Pipeline Facilities

Lenawee County

NEXUS GAS TRANSMISSION

Created: 6/1/2015

APPENDIX 7C

Soils Affected by the NEXUS Project Compressor Stations

Legend

- Mileposts (0.1 mile)
- NEXUS Mainline Pipeline
- TGP Interconnect
- Access Roads
- Permanent Easement
- Temporary Workspace
- ATWS
- Proposed Compressor Station Sites
- Proposed Contractor Yard
- NRCS Soils
- Project Counties

N

0 250 500
Feet

Projection: NAD83, UTM Zone 17N US Survey Feet, Grid North. Sources: ESRI, SPECTRA, TRC, USDA NRCS

Appendix 7C

Soils affected by the NEXUS Project Compressor Stations

Hanoverton Compressor Station

NEXUS GAS TRANSMISSION

Created: 5/27/2015

Page 1 of 4

Legend

- Mileposts (0.1 mile)
- NEXUS Mainline Pipeline
- TGP Interconnect
- Access Roads
- Permanent Easement
- Temporary Workspace
- ATWS
- Proposed Compressor Station Sites
- Proposed Contractor Yard
- NRCS Soils
- Project Counties

N

0 250 500
Feet

Projection: NAD83, UTM Zone 17N US Survey Feet, Grid North. Sources: ESRI, SPECTRA, TRC, USDA NRCS

Appendix 7C

Soils affected by the NEXUS Project Compressor Stations

Wadsworth Compressor Station

NEXUS GAS TRANSMISSION

Created: 5/27/2015

Legend

- Mileposts (0.1 mile)
- NEXUS Mainline Pipeline
- TGP Interconnect
- Access Roads
- Permanent Easement
- Temporary Workspace
- ATWS
- Proposed Compressor Station Sites
- Proposed Contractor Yard
- NRCS Soils
- Project Counties

0 250 500
Feet

Projection: NAD83, UTM Zone 17N US Survey Feet, Grid North. Sources: ESRI, SPECTRA, TRC, USDA NRCS

Appendix 7C

Soils affected by the NEXUS Project Compressor Stations

Clyde Compressor Station

NEXUS GAS TRANSMISSION

Created: 5/27/2015

Legend

- Mileposts (0.1 mile)
- NEXUS Mainline Pipeline
- TGP Interconnect
- Access Roads
- Permanent Easement
- Temporary Workspace
- ATWS
- Proposed Compressor Station Sites
- Proposed Contractor Yard
- NRCS Soils
- Project Counties

0 250 500
Feet

Projection: NAD83, UTM Zone 17N US Survey Feet, Grid North. Sources: ESRI, SPECTRA, TRC, USDA NRCS

Appendix 7C

Soils affected by the NEXUS Project Compressor Stations

Waterville Compressor Station

Created: 5/27/2015